FUTURA LA SCUOLA PER L'ITALIA DI DOMANI

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Italiadomani

Comune di

MILAZZO (ME)

Città Metropolitana di Messina

NEXT GENERATION EU - DECRETO N. 79 DEL 30.04.2024 – MINISTERO DELL'ISTRUZIONE E DEL MERITO DI CONCERTO CON IL MINISTERO DELL'ECONOMIA E DELLE FINANZE – PNRR - MISSIONE 4- ISTRUZIONE E RICERCA-COMPONENTE 1- INVESTIMENTO 1.1 - PIANO PER ASILI NIDO E SCUOLE D'INFANZIA E SERVIZI DI EDUCAZIONE E CURA PER LA PRIMA INFANZIA FINANZIATO DALL'UNIONE EUROPEA. INTERVENTO DENOMINATO:

"RICONVERSIONE CON DEMOLIZIONE E RICOSTRUZIONE DELL'EDIFICIO SITO IN VIA MADONNA DELLE GRAZIE. "

CUP: H57G24000050006

PROGETTO ESECUTIVO (Art. 41 e alleg. i.7 del D.Lgs. 36 / 2023)

Contenuto: *R2 - PROGETTO*

- Fascicolo di Calcolo

Tav.

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Il Progettista e Coordinatore Sicurezza in fase di Progettazione
Ing. Giulio MAMBELLI

Il R.U.P.
Ing. Claudio CAPPADONA

Il Dirigente del 6° Settore
Dott. Domenico LOMBARDO

L'Assessore ai LL.PP.
Ing. Santi ROMAGNOLO

Il Sindaco
Dott. Giuseppe MIDILI

Modellazione

La struttura è costituita da diversi elementi distinti, in base alla loro funzione, in:

- Fondazione in c.a. costituita da: graticcio di travi
- Travi in c.a.
- Pilastri in c.a.
- Solaio per Scuola
- Solaio per Terrazzo
- Solaio per Scala

I livelli di sicurezza scelti dal Committente e dal Progettista in funzione del tipo e dell'uso della struttura, nonché in funzione delle conseguenze del danno, con riguardo a persone, beni, e possibile turbativa sociale, compreso il costo delle opere necessarie per la riduzione del rischio di danno o di collasso, hanno indirizzato al progetto di una struttura con i seguenti requisiti:

- sicurezza nei confronti degli Stati Limite Ultimi (SLU);
- sicurezza nei confronti degli Stati Limite di Esercizio (SLE).

La struttura è stata schematizzata attraverso un modello spaziale agli elementi finiti che tenga conto dell'effettivo stato deformativo e di sollecitazione, secondo l'effettiva realizzazione.
I vincoli esterni della struttura sono stati caratterizzati, a seconda della presenza degli elementi di fondazione, con: travi winkler, plinti diretti, plinti su pali, platee, ovvero con vincoli perfetti di incastro, appoggio, carrello, ecc.
I vincoli interni sono stati schematizzati secondo le sollecitazioni mutuamente scambiate tra gli elementi strutturali, inserendo, ove opportuno, il rilascio di alcune caratteristiche della sollecitazione per schematizzare il comportamento di vincoli interni non iperstatici (cerniere, carrelli, ecc.).
Il modello agli elementi finiti è stato calcolato tenendo conto dell'interazione tra strutture in fondazione e strutture in elevazione, consentendo un'accurata distribuzione delle azioni statiche e sismiche; il calcolo è stato eseguito considerando che la struttura abbia un comportamento elastico lineare.
I solai sono schematizzati come aree di carico, sulle quali vengono definiti i carichi permanenti (QP Solai), i carichi fissi (QFissi Solai) e i carichi variabili (QV solai); tali carichi sono assegnati alle aste in modo automatico in relazione all'influenza delle diverse aree di carico. Le masse corrispondenti ai carichi variabili sui solai nelle combinazioni sismiche sono state trattate in maniera automatica mediante un coefficiente moltiplicativo, definito in funzione della tipologia del solaio.
Il modello utilizzato è stato valutato alla luce dei diversi scenari di carico a cui la struttura è sottoposta durante la sua costruzione e la sua vita, al fine di garantire la sicurezza e la durabilità della stessa. Per la tipologia strutturale affrontata non è stato necessario definire scenari di contingenza; pertanto non si è tenuto conto delle fasi costruttive delle struttura e, inoltre, si ritiene che non ci siano variazioni del modello di calcolo e degli schemi di vincolo, durante la vita dell'opera. Per il dettaglio degli scenari di calcolo si faccia riferimento alla "Relazione di Calcolo".
Il progetto e la verifica degli elementi strutturali è stato effettuato seguendo la teoria degli Stati limite. I parametri relativi alle verifiche effettuate sono riportati nella Relazione di Calcolo.
Il solutore agli elementi finiti impiegato nell'analisi è SpaceSolver, per il calcolo di strutture piane e spaziali schematizzabili da un insieme di elementi finiti tipo:

- BEAM
- PLATE-SHELL
- WINK
- BOUNDARY

Questi elementi interagiscono tra loro attraverso i nodi, con la possibilità di tenere in conto tutti i possibili disassamenti, mediante l'introduzione di conci rigidi e traslazioni degli elementi bidimensionali. Il solutore lavora in campo elastico lineare, si basa sulle routines di Matlab ed è stato sviluppato in collaborazione con l'Università di Roma – Tor Vergata. Il solutore offre la possibilità di risolvere anche travi su suolo alla Winkler con molle spalmate sull'intera suola, anziché sul solo asse, plinti diretti e su pali, pali singoli, platee, piastre sottili e spesse, con controllo delle rotazioni attorno all'asse normale alla piastra (drilling). Inoltre, per gli elementi BEAM l'equilibrio è scritto rispetto alla linea dei centri di taglio anzichè rispetto alla linea dei baricentri. L'affidabilità del solutore è stata testata su una serie di esempi campioni calcolati con altri

procedimenti o con formule note, di cui si rende disponibile la documentazione.

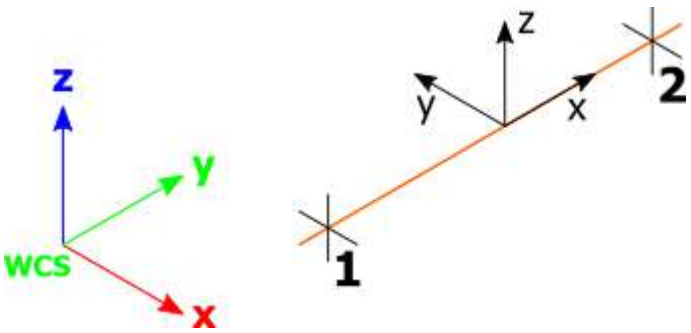
Affidabilità dei codici utilizzati

Il programma è dotato di una serie di filtri di auto diagnostica che segnalano i seguenti eventi:

- labilità della struttura;
- assenza di masse;
- nodi collegati ad aste nulle;
- mancanza di terreno sugli elementi in fondazione;
- controllo sull'assegnazione dei nodi all'impalcato;
- correttezza degli spettri di progetto;
- fattori di partecipazione modali;
- assegnazione dei criteri di verifica agli elementi;
- numerazione degli elementi strutturali;
- congruenza delle connessioni tra elementi shell;
- congruenza delle aree di carico;
- definizione delle caratteristiche d'inerzia delle sezioni;
- presenza del magrone sotto la travi tipo wink;
- elementi non verificati per semi progetto allo SLU, con inserimento automatico delle armature secondo i criteri di verifica;
- elementi non verificati allo SLU per armature già inserite nell'elemento strutturale;
- elementi non verificati allo SLE per armature già inserite nell'elemento strutturale.

Presentazione dei risultati

I disegni dello schema statico adottato sono riportati nel fascicolo allegato alla presente relazione. E' stato impiegato il Sistema Internazionale per le unità di misura, con riferimento al daN per le forze.



Il sistema di riferimento globale rispetto al quale è stata riferita l'intera struttura è una terna di assi cartesiani sinistrorsa OXYZ (X,Y, e Z sono disposti e orientati rispettivamente secondo il pollice, l'indice ed il medio della mano destra, una volta posizionati questi ultimi a 90° tra loro).
La terna di riferimento locale per un'asta è anch'essa una terna sinistrorsa O'xyz che ha l'asse x orientato dal nodo iniziale I dell'asta verso il nodo finale J e gli assi y e z diretti secondo gli assi geometrici della sezione, con l'asse y orizzontale e orientato in modo da portarsi a coincidere con l'asse x a mezzo di una rotazione oraria di 90° e l'asse z di conseguenza.

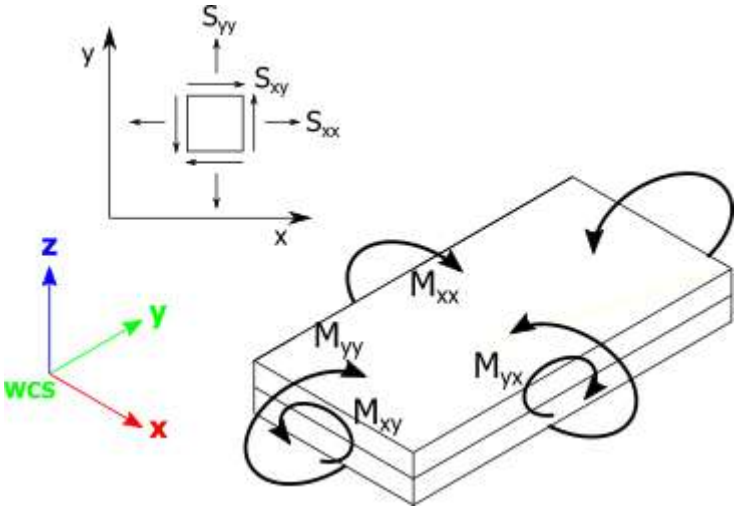
Per un'asta comunque disposta nello spazio la sua terna locale è orientata in modo tale da portarsi a coincidere con la terna globale a mezzo di rotazioni orarie degli assi locali inferiori a 180°.

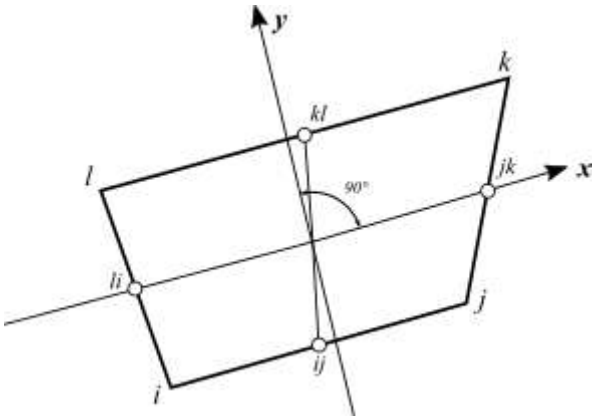
- Le forze, sia sulle aste che sulle pareti o lastre, sono positive se opposte agli assi locali.
- Le forze nodali sono positive se opposte agli assi globali.
- Le coppie sono positive se sinistrorse.

Le caratteristiche di sollecitazione sono positive se sulla faccia di normale positiva sono rappresentate da vettori equiversi agli assi di riferimento locali; in particolare il vettore momento positivo rappresenta una coppia che ruota come le dita della mano destra che si chiudono quando il pollice è equiverso all'asse locale.

- Le traslazioni sono positive se concordi con gli assi globali.
- Le rotazioni sono positive se sinistrorse.

Il sistema di riferimento locale per gli elementi bidimensionali è quello riportato nelle figure seguenti.





La terna locale per l'elemento shell è costituita dall'asse x locale che va dal nodo li al nodo jk, l'asse y è diretto secondo il piano dell'elemento e orientato verso il nodo i e l'asse z, di conseguenza, è orientato in modo da formare la solita terna sinistrorsa. L'asse z locale rappresenta la normale positiva all'elemento.
Le sollecitazioni dell'elemento sono:

- Sforzi membranali
  - $S_{xx} = \sigma_x$
  - $S_{yy} = \sigma_y$
  - $S_{xy} = \tau_{xy}$
- Sforzi flessionali (momenti)
  - M_{xx}, momento che genera σ_x (intorno ad y)
  - M_{yy}, momento che genera σ_y (intorno a x)
  - M_{xy}, momento torcente che genera τ_{xy}

Le sollecitazioni principali dell'elemento sono:

$$M_{1,2} = \frac{M_{xx} + M_{yy}}{2} \pm \sqrt{\left(\frac{M_{xx} - M_{yy}}{2}\right)^2 + M_{xy}^2}$$

$$S_{1,2} = \frac{S_{xx} + S_{yy}}{2} \pm \sqrt{\left(\frac{S_{xx} - S_{yy}}{2}\right)^2 + S_{xy}^2}$$

$$\tan 2\theta = \frac{M_{xy}}{M_{xx} - M_{yy}} \qquad \tan 2\psi = \frac{S_{xy}}{S_{xx} - S_{yy}}$$

dove θ è l'angolo formato dagli assi principali di M_1 e M_2 con quelli di riferimento e ψ è l'angolo formato dagli assi principali di S_1 e S_2 con quelli di riferimento. L'elemento shell usato come piastra fornisce i momenti flettenti e non i tagli in direzione ortogonale all'elemento, che possono ottenersi come derivazione dei momenti flettenti;

$\tau zx = Mxx,x + Mxy,y$

$\tau zy = Mxy,y + Myy,y$

Quando invece viene usato come lastra ci restituisce valori di σ e τ costanti, non adatti a rappresentare momenti flettenti, ma solo sforzi normali e tagli nel piano della lastra.

I tabulati di calcolo contengono due sezioni principali: la descrizione del modello di calcolo e la presentazione dei risultati.
La descrizione del modello di calcolo contiene:

- i dati generali (dimensioni);
- le coordinate nodali;
- i vincoli dei nodi e i vincoli interni delle aste, con le eventuali sconnessioni;
- le caratteristiche sezionali;
- le caratteristiche dei solai;
- le caratteristiche delle aste;
- i carichi sulle aste, sui nodi e sui muri (inclusa la distribuzione delle distorsioni impresse, e delle variazioni e dei gradienti di temperatura);
- configurazione di sistemi che introducono stati coattivi;
- le caratteristiche dei materiali;
- legami costitutivi e criteri di verifica;
- le condizioni di carico.

La stampa dei risultati contiene:

- le combinazioni dei carichi;
- le forze sismiche agenti sulla struttura;
- gli spostamenti d'impalcato, se l'impalcato è rigido;
- gli spostamenti nodali;
- le sollecitazioni sulle membrature per ogni combinazione di carico;
- la sollecitazione sul terreno sotto travi di fondazione o platee;
- deformate;
- diagrammi sollecitazioni.

Tabulati di input

Dati generali

Nome struttura	Struttura_01
Temperatura di riferimento [°C]	0
Fattore rigidezza assiale pilastri	1
Numero di frequenze	25
% Filtro masse libere	0.1
% Coefficiente di smorzamento viscoso	5
Spostamenti modali con segno	Si
Deformabilità a taglio delle aste	Si
Impalcati deformabili per carichi termici	No
Spostamento ammissibile impalcati	0.0050*h

Impalcati

N°	Quota	Rigido	Incr.Soll.Pil	Inc.Soll.Par.
	m	m		
0	0.00	No	1.000	1.000
1	4.39	Si	1.000	1.000
2	8.14	Si	1.000	1.000

Percentuali Spostamento masse impalcati

Posizione	% Spostamento direzione X	% Spostamento direzione Y
1	0	-5
2	5	0
3	0	5
4	-5	0

Combinazioni del Sisma in X e Y e Verticale

Comb.	Pos. SismaX	Pos. SismaY	Fx	Fy	Fz
1	1	2	1	0.3	0
2	1	2	0.3	1	0
3	1	4	1	0.3	0
4	1	4	0.3	1	0
5	3	2	1	0.3	0
6	3	2	0.3	1	0
7	3	4	1	0.3	0
8	3	4	0.3	1	0

Comb. Numero di combinazione dei sismi
Pos. SismaX Posizione in cui viene scelto il sisma in direzione X
Pos. SismaY Posizione in cui viene scelto il sisma in direzione Y
Fx Fattore con cui il sisma X partecipa
Fy Fattore con cui il sisma Y partecipa
Fz Fattore con cui il sisma Verticale partecipa (quando richiesto)

Ogni combinazione genera al massimo 8 sotto-combinazioni in base a tutte le combinazioni possibili dei segni di Fx ed Fy ed Fz.

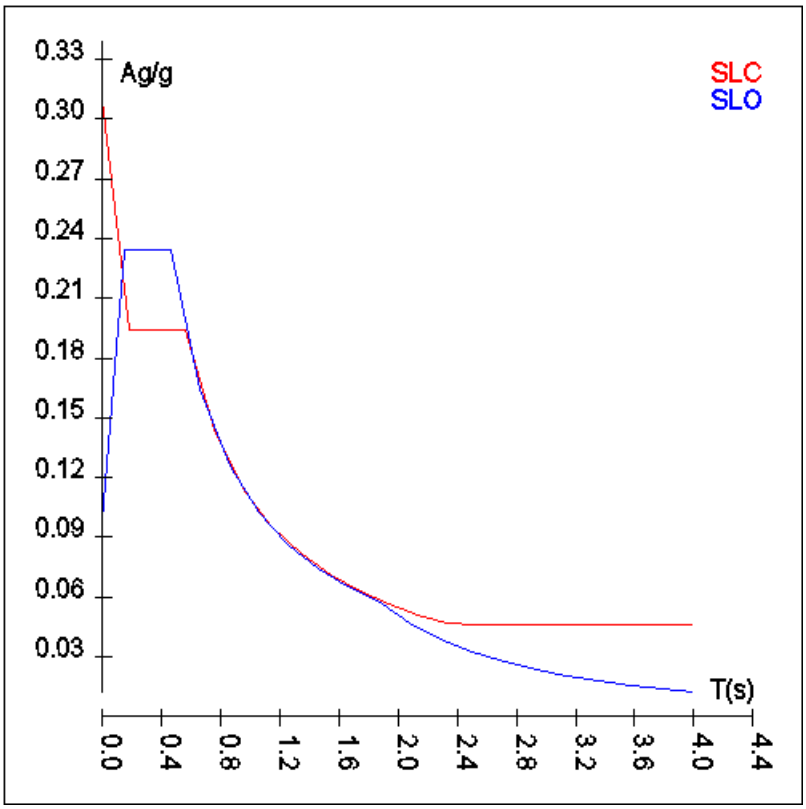
Spettri di risposta

Spettro: **Spettro NT2018 altre SL**
Il calcolo degli spettri e del fattore di comportamento sono stati calcolati per la seguente tipologia di terreno e struttura.

Vita della struttura	
Tipo	Opere infr. imp. normale (50-100)
Vita nominale VN [anni]	50.0
Classe d'uso	III
Coefficiente d'uso CU	1.500
Periodo di riferimento VR [anni]	75.000
Probabilità di superamento PVR allo Stato limite di esercizio - SLO	81.0%
Probabilità di superamento PVR allo Stato limite ultimo - SLC	5.0%
Periodo di ritorno TR SLO [anni]	45.2
Periodo di ritorno TR SLC [anni]	1462.2
Parametri del sito	
Comune	Milazzo (ME)
Longitudine	15.2427
Latitudine	38.2209
Id reticolo del sito	44761-44760-44983-44982

Valori di riferimento del sito	
Accelerazione orizzontale massima del sito Ag/g - SLO (TR=45.2)	0.0649
Fattore di amplificazione dello spettro Fo - SLO (TR=45.2)	2.4132
Periodo di riferimento di inizio del tratto a velocità costante T^*C [s] - SLO (TR=45.2)	0.294
Accelerazione orizzontale massima del sito Ag/g - SLC (TR=1462.2)	0.2312
Fattore di amplificazione dello spettro Fo - SLC (TR=1462.2)	2.5936
Periodo di riferimento di inizio del tratto a velocità costante T^*C [s] - SLC (TR=1462.2)	0.394
Coefficiente Amplificazione Topografica St	1.000
Categoria terreno	C
Stato limite SLC	
Coefficiente di amplificazione stratigrafica Ss	1.34
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.19
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.56
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	2.52
Stato limite SLO	
Coefficiente di amplificazione stratigrafica Ss	1.50
Periodo di inizio del tratto ad accelerazione costante dello spettro TB [s]	0.15
Periodo di inizio del tratto a velocità costante dello spettro TC [s]	0.46
Periodo di inizio del tratto a spostamento costante dello spettro TD [s]	1.86
Fattore di comportamento (SLC)	
Classe duttilità	A
Tipo struttura	Cemento armato
Fattore di riduzione per regolarità in altezza Kr- Struttura non regolare	0.800000
Fattore di riduzione per rottura pareti Kw	1.000
Regolare in pianta	NO (cfr.NTC7.3.1)
Coefficiente moltiplicativo Ce - struttura a telaio, a pareti accoppiate e miste	4.500
Au/A1 - Telaio + piani + campate	1.300
Fattore di comportamento q = Kw*Kr*q0=Kw*Kr*Ce*(1+Au/A1)/2	4.140
Fattore di comportamento SLO (spettro elastico)	
q	1.000

T SLC [s]	**Sd SLC**[a/g]	**T SLO** [s]	**Sd SLO**[a/g]
0.00000	0.30990	0.00000	0.09728
0.18757	0.19415	0.15428	0.23477
0.56271	0.19415	0.46285	0.23477
0.75894	0.14395	0.66236	0.16406
0.95517	0.11438	0.86187	0.12608
1.15139	0.09488	1.06138	0.10238
1.34762	0.08107	1.26089	0.08618
1.54385	0.07076	1.46040	0.07441
1.74008	0.06278	1.65991	0.06546
1.93631	0.05642	1.85943	0.05844
2.13253	0.05123	2.07348	0.04700
2.32876	0.04691	2.28754	0.03861
2.52499	0.04625	2.50160	0.03229
2.73571	0.04625	2.71566	0.02740
2.94642	0.04625	2.92971	0.02354
3.15714	0.04625	3.14377	0.02044
3.36785	0.04625	3.35783	0.01792
3.57857	0.04625	3.57189	0.01584
3.78928	0.04625	3.78594	0.01410
4.00000	0.04625	4.00000	0.01263



Caratteristiche del terreno

Strato n°	Spessore	γ	γSat	ϕ	Addensato	OCR	Coesione	Cu	E	ν
	m	kN/m^3	kN/m^3	°			MPa	MPa	MPa	
Terreno Milazzo: Cost.Winkler=2.10 DaN/cmc - Falda assente										
1	15.00	18.00	18.00	25.00	No	--	0.00	0.00	3.20E00	0.30

Materiali		
C25/30		
Peso specifico	kN/m^3	25.00
Modulo di Young E	MPa	3.12E04
Modulo di Poisson ν		0.13
Coefficiente di dilatazione termica λ	1/°C	1e-05

Nodi - Geometria e vincoli

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
	Coordinate [m]			Vincoli						
2	0.00	0.00	0.00	1	1	0	0	0	1	0
3	5.14	0.00	0.00	1	1	0	0	0	1	0
4	9.78	0.00	0.00	1	1	0	0	0	1	0
5	15.68	0.00	0.00	1	1	0	0	0	1	0
6	19.65	0.00	0.00	1	1	0	0	0	1	0
7	24.95	0.00	0.00	1	1	0	0	0	1	0
8	2.99	2.16	0.00	1	1	0	0	0	1	0
9	7.50	2.28	0.00	1	1	0	0	0	1	0
10	15.38	3.77	0.00	1	1	0	0	0	1	0
11	19.65	3.77	0.00	1	1	0	0	0	1	0
12	24.95	3.77	0.00	1	1	0	0	0	1	0
13	5.30	4.48	0.00	1	1	0	0	0	1	0

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
14	9.83	4.61	0.00	1	1	0	0	0	1	0
15	0.00	4.82	0.00	1	1	0	0	0	1	0
16	7.64	6.81	0.00	1	1	0	0	0	1	0
17	13.59	8.38	0.00	1	1	0	0	0	1	0
18	15.38	8.47	0.00	1	1	0	0	0	1	0
19	19.65	8.47	0.00	1	1	0	0	0	1	0
20	24.95	8.47	0.00	1	1	0	0	0	1	0
21	0.00	9.12	0.00	1	1	0	0	0	1	0
22	5.74	9.12	0.00	1	1	0	0	0	1	0
23	11.40	10.57	0.00	1	1	0	0	0	1	0
24	0.00	12.00	0.00	1	1	0	0	0	1	0
25	5.45	12.00	0.00	1	1	0	0	0	1	0
26	11.49	12.00	0.00	1	1	0	0	0	1	0
27	19.95	12.60	0.00	1	1	0	0	0	1	0
28	24.95	12.60	0.00	1	1	0	0	0	1	0
29	0.00	16.40	0.00	1	1	0	0	0	1	0
30	5.34	16.40	0.00	1	1	0	0	0	1	0
31	11.49	16.40	0.00	1	1	0	0	0	1	0
35	13.59	8.38	2.67	0	0	0	0	0	0	1
36	11.40	10.57	2.67	0	0	0	0	0	0	1
37	9.83	4.61	0.80	0	0	0	0	0	0	0
38	12.36	7.16	2.67	0	0	0	0	0	0	1
39	10.18	9.35	2.67	0	0	0	0	0	0	1
102	0.00	0.00	4.39	0	0	0	0	0	0	1
103	5.14	0.00	4.39	0	0	0	0	0	0	1
104	9.78	0.00	4.39	0	0	0	0	0	0	1
105	15.68	0.00	4.39	0	0	0	0	0	0	1
106	19.65	0.00	4.39	0	0	0	0	0	0	1
107	24.95	0.00	4.39	0	0	0	0	0	0	1
108	2.99	2.16	4.39	0	0	0	0	0	0	1
109	7.50	2.28	4.39	0	0	0	0	0	0	1
110	15.38	3.77	4.39	0	0	0	0	0	0	1
111	19.65	3.77	4.39	0	0	0	0	0	0	1
112	24.95	3.77	4.39	0	0	0	0	0	0	1
113	5.30	4.48	4.39	0	0	0	0	0	0	1
114	9.83	4.61	4.39	0	0	0	0	0	0	1
115	0.00	4.82	4.39	0	0	0	0	0	0	1
116	7.64	6.81	4.39	0	0	0	0	0	0	1
117	13.59	8.38	4.39	0	0	0	0	0	0	1
118	15.38	8.47	4.39	0	0	0	0	0	0	1
119	19.65	8.47	4.39	0	0	0	0	0	0	1
120	24.95	8.47	4.39	0	0	0	0	0	0	1
121	0.00	9.12	4.39	0	0	0	0	0	0	1
122	5.74	9.12	4.39	0	0	0	0	0	0	1
123	11.40	10.57	4.39	0	0	0	0	0	0	1
124	0.00	12.00	4.39	0	0	0	0	0	0	1
125	5.45	12.00	4.39	0	0	0	0	0	0	1
126	11.49	12.00	4.39	0	0	0	0	0	0	1
127	19.95	12.60	4.39	0	0	0	0	0	0	1
128	24.95	12.60	4.39	0	0	0	0	0	0	1
129	0.00	16.40	4.39	0	0	0	0	0	0	1
130	5.34	16.40	4.39	0	0	0	0	0	0	1
131	11.49	16.40	4.39	0	0	0	0	0	0	1
204	9.78	0.00	8.14	0	0	0	0	0	0	2
205	15.68	0.00	8.14	0	0	0	0	0	0	2
206	19.65	0.00	8.14	0	0	0	0	0	0	2
209	7.50	2.28	8.14	0	0	0	0	0	0	2
210	15.38	3.77	8.14	0	0	0	0	0	0	2
211	19.65	3.77	8.14	0	0	0	0	0	0	2
213	5.30	4.48	8.14	0	0	0	0	0	0	2
214	9.83	4.61	8.14	0	0	0	0	0	0	2
216	7.64	6.81	8.14	0	0	0	0	0	0	2
217	13.59	8.38	8.14	0	0	0	0	0	0	2
218	15.38	8.47	8.14	0	0	0	0	0	0	2

Nodo	X	Y	Z	Tx	Ty	Tz	Rx	Ry	Rz	Impalcato
219	19.65	8.47	8.14	0	0	0	0	0	0	2
222	5.74	9.12	8.14	0	0	0	0	0	0	2
223	11.40	10.57	8.14	0	0	0	0	0	0	2
225	5.45	12.00	8.14	0	0	0	0	0	0	2
226	11.49	12.00	8.14	0	0	0	0	0	0	2

Nodi - Carichi

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
			kN			kN*m			cm			°		°C
102	QP Solai	0.00	0.00	1.88	-0.27	-1.53	0.00							
102	QFissi Solai	0.00	0.00	0.00	0.00	-0.01	0.00							
102	QFissi Solai	0.00	0.00	1.69	-0.44	-1.12	0.00							
102	QV Solai	0.00	0.00	3.85	-1.00	-2.56	0.00							
102	QV Solai	0.00	0.00	0.02	0.00	-0.02	0.00							
102	QV SolaiPsi0	0.00	0.00	2.69	-0.70	-1.79	0.00							
102	QV SolaiPsi0	0.00	0.00	0.01	0.00	-0.02	0.00							
102	QV SolaiPsi1	0.00	0.00	2.69	-0.70	-1.79	0.00							
102	QV SolaiPsi1	0.00	0.00	0.01	0.00	-0.02	0.00							
102	QV SolaiPsi2	0.00	0.00	2.31	-0.60	-1.53	0.00							
102	QV SolaiPsi2	0.00	0.00	0.01	0.00	-0.01	0.00							
102	Neve	0.00	0.00	0.46	-0.12	-0.31	0.00							
103	QFissi Solai	0.00	0.00	0.01	0.00	0.00	0.00							
103	QFissi Solai	0.00	0.00	0.09	0.01	0.00	0.00							
103	QV Solai	0.00	0.00	0.02	0.00	0.00	0.00							
103	QV Solai	0.00	0.00	0.20	0.03	-0.01	0.00							
103	QV SolaiPsi0	0.00	0.00	0.02	0.00	0.00	0.00							
103	QV SolaiPsi0	0.00	0.00	0.14	0.02	0.00	0.00							
103	QV SolaiPsi1	0.00	0.00	0.14	0.02	0.00	0.00							
103	QV SolaiPsi1	0.00	0.00	0.02	0.00	0.00	0.00							
103	QV SolaiPsi2	0.00	0.00	0.12	0.02	0.00	0.00							
103	QV SolaiPsi2	0.00	0.00	0.01	0.00	0.00	0.00							
103	Neve	0.00	0.00	0.02	0.00	0.00	0.00							
104	QFissi Solai	0.00	0.00	0.25	0.04	-0.02	0.00							
104	QV Solai	0.00	0.00	0.57	0.09	-0.04	0.00							
104	QV SolaiPsi0	0.00	0.00	0.40	0.06	-0.03	0.00							
104	QV SolaiPsi1	0.00	0.00	0.40	0.06	-0.03	0.00							
104	QV SolaiPsi2	0.00	0.00	0.34	0.05	-0.03	0.00							
104	Neve	0.00	0.00	0.07	0.01	-0.01	0.00							
105	QFissi Solai	0.00	0.00	0.13	0.02	0.01	0.00							
105	QV Solai	0.00	0.00	0.16	0.02	0.01	0.00							
105	QV SolaiPsi0	0.00	0.00	0.11	0.02	0.01	0.00							
105	QV SolaiPsi1	0.00	0.00	0.11	0.02	0.01	0.00							
105	QV SolaiPsi2	0.00	0.00	0.09	0.01	0.01	0.00							
106	QFissi Solai	0.00	0.00	0.13	0.02	-0.01	0.00							
106	QV Solai	0.00	0.00	0.16	0.02	-0.01	0.00							
106	QV SolaiPsi0	0.00	0.00	0.11	0.02	-0.01	0.00							
106	QV SolaiPsi1	0.00	0.00	0.11	0.02	-0.01	0.00							
106	QV SolaiPsi2	0.00	0.00	0.09	0.01	-0.01	0.00							
108	QP Solai	0.00	0.00	0.07	-0.01	-0.01	0.00							
108	QP Solai	0.00	0.00	0.07	-0.01	-0.01	0.00							
108	QFissi Solai	0.00	0.00	0.04	0.00	0.00	0.00							
108	QFissi Solai	0.00	0.00	0.34	-0.02	-0.05	0.00							
108	QV Solai	0.00	0.00	0.10	-0.01	-0.01	0.00							
108	QV Solai	0.00	0.00	0.77	-0.05	-0.12	0.00							
108	QV SolaiPsi0	0.00	0.00	0.07	-0.01	-0.01	0.00							
108	QV SolaiPsi0	0.00	0.00	0.54	-0.03	-0.08	0.00							
108	QV SolaiPsi1	0.00	0.00	0.54	-0.03	-0.08	0.00							
108	QV SolaiPsi1	0.00	0.00	0.07	-0.01	-0.01	0.00							
108	QV SolaiPsi2	0.00	0.00	0.06	-0.01	0.00	0.00							
108	QV SolaiPsi2	0.00	0.00	0.46	-0.03	-0.07	0.00							
108	Neve	0.00	0.00	0.09	-0.01	-0.01	0.00							
109	QFissi Solai	0.00	0.00	0.59	0.12	0.00	0.00							
109	QV Solai	0.00	0.00	1.34	0.28	0.00	0.00							
109	QV SolaiPsi0	0.00	0.00	0.94	0.20	0.00	0.00							
109	QV SolaiPsi1	0.00	0.00	0.94	0.20	0.00	0.00							
109	QV SolaiPsi2	0.00	0.00	0.80	0.17	0.00	0.00							
109	Neve	0.00	0.00	0.16	0.03	0.00	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
110	QFissi Solai	0.00	0.00	0.63	-0.05	-0.09	0.00							
110	QV Solai	0.00	0.00	0.77	-0.06	-0.12	0.00							
110	QV SolaiPsi0	0.00	0.00	0.54	-0.04	-0.08	0.00							
110	QV SolaiPsi1	0.00	0.00	0.54	-0.04	-0.08	0.00							
110	QV SolaiPsi2	0.00	0.00	0.46	-0.03	-0.07	0.00							
111	QFissi Solai	0.00	0.00	0.13	-0.02	-0.01	0.00							
111	QFissi Solai	0.00	0.00	0.53	-0.04	-0.08	0.00							
111	QFissi Solai	0.00	0.00	0.80	-0.07	-0.11	0.00							
111	QV Solai	0.00	0.00	1.20	-0.09	-0.18	0.00							
111	QV Solai	0.00	0.00	0.16	-0.02	-0.01	0.00							
111	QV Solai	0.00	0.00	0.98	-0.09	-0.13	0.00							
111	QV SolaiPsi0	0.00	0.00	0.11	-0.02	-0.01	0.00							
111	QV SolaiPsi0	0.00	0.00	0.84	-0.06	-0.13	0.00							
111	QV SolaiPsi0	0.00	0.00	0.69	-0.06	-0.09	0.00							
111	QV SolaiPsi1	0.00	0.00	0.11	-0.02	-0.01	0.00							
111	QV SolaiPsi1	0.00	0.00	0.69	-0.06	-0.09	0.00							
111	QV SolaiPsi1	0.00	0.00	0.84	-0.06	-0.13	0.00							
111	QV SolaiPsi2	0.00	0.00	0.59	-0.05	-0.08	0.00							
111	QV SolaiPsi2	0.00	0.00	0.72	-0.05	-0.11	0.00							
111	QV SolaiPsi2	0.00	0.00	0.09	-0.01	-0.01	0.00							
111	Neve	0.00	0.00	0.14	-0.01	-0.02	0.00							
112	QFissi Solai	0.00	0.00	0.53	-0.04	0.08	0.00							
112	QV Solai	0.00	0.00	1.20	-0.09	0.18	0.00							
112	QV SolaiPsi0	0.00	0.00	0.84	-0.06	0.13	0.00							
112	QV SolaiPsi1	0.00	0.00	0.84	-0.06	0.13	0.00							
112	QV SolaiPsi2	0.00	0.00	0.72	-0.05	0.11	0.00							
112	Neve	0.00	0.00	0.14	-0.01	0.02	0.00							
113	QP Solai	0.00	0.00	0.22	-0.02	-0.03	0.00							
113	QFissi Solai	0.00	0.00	0.59	0.00	-0.13	0.00							
113	QFissi Solai	0.00	0.00	1.11	0.05	-0.28	0.00							
113	QV Solai	0.00	0.00	2.53	0.10	-0.63	0.00							
113	QV Solai	0.00	0.00	1.35	0.00	-0.29	0.00							
113	QV SolaiPsi0	0.00	0.00	1.77	0.07	-0.44	0.00							
113	QV SolaiPsi0	0.00	0.00	0.94	0.00	-0.20	0.00							
113	QV SolaiPsi1	0.00	0.00	0.94	0.00	-0.20	0.00							
113	QV SolaiPsi1	0.00	0.00	1.77	0.07	-0.44	0.00							
113	QV SolaiPsi2	0.00	0.00	1.52	0.06	-0.38	0.00							
113	QV SolaiPsi2	0.00	0.00	0.81	0.00	-0.17	0.00							
113	Neve	0.00	0.00	0.30	0.01	-0.08	0.00							
113	Neve	0.00	0.00	0.16	0.00	-0.03	0.00							
114	QFissi Solai	0.00	0.00	0.41	0.07	0.02	0.00							
114	QFissi Solai	0.00	0.00	0.04	0.01	0.00	0.00							
114	QV Solai	0.00	0.00	0.10	0.02	0.00	0.00							
114	QV Solai	0.00	0.00	0.50	0.08	0.03	0.00							
114	QV SolaiPsi0	0.00	0.00	0.35	0.06	0.02	0.00							
114	QV SolaiPsi0	0.00	0.00	0.07	0.01	0.00	0.00							
114	QV SolaiPsi1	0.00	0.00	0.07	0.01	0.00	0.00							
114	QV SolaiPsi1	0.00	0.00	0.35	0.06	0.02	0.00							
114	QV SolaiPsi2	0.00	0.00	0.06	0.01	0.00	0.00							
114	QV SolaiPsi2	0.00	0.00	0.30	0.05	0.02	0.00							
114	Neve	0.00	0.00	0.01	0.00	0.00	0.00							
115	QFissi Solai	0.00	0.00	0.14	-0.01	-0.02	0.00							
115	QV Solai	0.00	0.00	0.33	-0.02	-0.05	0.00							
115	QV SolaiPsi0	0.00	0.00	0.23	-0.02	-0.03	0.00							
115	QV SolaiPsi1	0.00	0.00	0.23	-0.02	-0.03	0.00							
115	QV SolaiPsi2	0.00	0.00	0.20	-0.01	-0.03	0.00							
115	Neve	0.00	0.00	0.04	0.00	-0.01	0.00							
116	QFissi Solai	0.00	0.00	0.41	-0.02	-0.07	0.00							
116	QV Solai	0.00	0.00	0.50	-0.03	-0.08	0.00							
116	QV SolaiPsi0	0.00	0.00	0.35	-0.02	-0.06	0.00							
116	QV SolaiPsi1	0.00	0.00	0.35	-0.02	-0.06	0.00							
116	QV SolaiPsi2	0.00	0.00	0.30	-0.02	-0.05	0.00							
117	QFissi Solai	0.00	0.00	0.11	-0.01	0.03	0.00							
117	QV Solai	0.00	0.00	0.13	-0.01	0.03	0.00							
117	QV SolaiPsi0	0.00	0.00	0.09	-0.01	0.02	0.00							
117	QV SolaiPsi1	0.00	0.00	0.09	-0.01	0.02	0.00							
117	QV SolaiPsi2	0.00	0.00	0.08	-0.01	0.02	0.00							
118	QFissi Solai	0.00	0.00	0.29	-0.04	-0.02	0.00							
118	QV Solai	0.00	0.00	0.35	-0.05	-0.03	0.00							
118	QV SolaiPsi0	0.00	0.00	0.24	-0.04	-0.02	0.00							
118	QV SolaiPsi1	0.00	0.00	0.24	-0.04	-0.02	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
118	QV SolaiPsi2	0.00	0.00	0.21	-0.03	-0.02	0.00							
119	QP Solai	0.00	0.00	0.06	0.00	-0.03	0.00							
119	QFissi Solai	0.00	0.00	0.17	-0.03	-0.01	0.00							
119	QFissi Solai	0.00	0.00	1.03	-0.15	-0.46	0.00							
119	QV Solai	0.00	0.00	2.34	-0.34	-1.05	0.00							
119	QV Solai	0.00	0.00	0.21	-0.03	-0.02	0.00							
119	QV SolaiPsi0	0.00	0.00	0.15	-0.02	-0.01	0.00							
119	QV SolaiPsi0	0.00	0.00	1.64	-0.24	-0.74	0.00							
119	QV SolaiPsi1	0.00	0.00	1.64	-0.24	-0.74	0.00							
119	QV SolaiPsi1	0.00	0.00	0.15	-0.02	-0.01	0.00							
119	QV SolaiPsi2	0.00	0.00	0.13	-0.02	-0.01	0.00							
119	QV SolaiPsi2	0.00	0.00	1.40	-0.20	-0.63	0.00							
119	Neve	0.00	0.00	0.28	-0.04	-0.13	0.00							
120	QFissi Solai	0.00	0.00	0.99	-0.15	0.15	0.00							
120	QV Solai	0.00	0.00	2.26	-0.34	0.34	0.00							
120	QV SolaiPsi0	0.00	0.00	1.58	-0.24	0.24	0.00							
120	QV SolaiPsi1	0.00	0.00	1.58	-0.24	0.24	0.00							
120	QV SolaiPsi2	0.00	0.00	1.35	-0.20	0.20	0.00							
120	Neve	0.00	0.00	0.27	-0.04	0.04	0.00							
121	QFissi Solai	0.00	0.00	0.14	-0.01	-0.02	0.00							
121	QV Solai	0.00	0.00	0.33	-0.02	-0.05	0.00							
121	QV SolaiPsi0	0.00	0.00	0.23	-0.02	-0.03	0.00							
121	QV SolaiPsi1	0.00	0.00	0.23	-0.02	-0.03	0.00							
121	QV SolaiPsi2	0.00	0.00	0.20	-0.01	-0.03	0.00							
121	Neve	0.00	0.00	0.04	0.00	-0.01	0.00							
122	QFissi Solai	0.00	0.00	0.13	-0.01	0.02	0.00							
122	QV Solai	0.00	0.00	0.29	-0.02	0.04	0.00							
122	QV SolaiPsi0	0.00	0.00	0.21	-0.02	0.03	0.00							
122	QV SolaiPsi1	0.00	0.00	0.21	-0.02	0.03	0.00							
122	QV SolaiPsi2	0.00	0.00	0.18	-0.01	0.03	0.00							
122	Neve	0.00	0.00	0.04	0.00	0.01	0.00							
123	QFissi Solai	0.00	0.00	0.30	-0.07	0.02	0.00							
123	QV Solai	0.00	0.00	0.37	-0.09	0.02	0.00							
123	QV SolaiPsi0	0.00	0.00	0.26	-0.06	0.02	0.00							
123	QV SolaiPsi1	0.00	0.00	0.26	-0.06	0.02	0.00							
123	QV SolaiPsi2	0.00	0.00	0.22	-0.05	0.01	0.00							
124	QFissi Solai	0.00	0.00	0.14	0.01	-0.02	0.00							
124	QV Solai	0.00	0.00	0.33	0.02	-0.05	0.00							
124	QV SolaiPsi0	0.00	0.00	0.23	0.02	-0.03	0.00							
124	QV SolaiPsi1	0.00	0.00	0.23	0.02	-0.03	0.00							
124	QV SolaiPsi2	0.00	0.00	0.20	0.01	-0.03	0.00							
124	Neve	0.00	0.00	0.04	0.00	-0.01	0.00							
125	QP Solai	0.00	0.00	2.15	0.31	-0.32	0.00							
125	QP Solai	0.00	0.00	0.03	0.00	0.00	0.00							
125	QFissi Solai	0.00	0.00	0.87	0.13	-0.13	0.00							
125	QFissi Solai	0.00	0.00	2.63	0.57	-0.40	0.00							
125	QFissi Solai	0.00	0.00	0.50	0.06	-0.05	0.00							
125	QV Solai	0.00	0.00	1.13	0.14	-0.11	0.00							
125	QV Solai	0.00	0.00	1.97	0.30	-0.29	0.00							
125	QV Solai	0.00	0.00	3.21	0.70	-0.48	0.00							
125	QV SolaiPsi0	0.00	0.00	1.38	0.21	-0.21	0.00							
125	QV SolaiPsi0	0.00	0.00	2.25	0.49	-0.34	0.00							
125	QV SolaiPsi0	0.00	0.00	0.79	0.10	-0.08	0.00							
125	QV SolaiPsi1	0.00	0.00	2.25	0.49	-0.34	0.00							
125	QV SolaiPsi1	0.00	0.00	1.38	0.21	-0.21	0.00							
125	QV SolaiPsi1	0.00	0.00	0.79	0.10	-0.08	0.00							
125	QV SolaiPsi2	0.00	0.00	1.18	0.18	-0.18	0.00							
125	QV SolaiPsi2	0.00	0.00	0.68	0.08	-0.07	0.00							
125	QV SolaiPsi2	0.00	0.00	1.93	0.42	-0.29	0.00							
125	Neve	0.00	0.00	0.14	0.01	-0.01	0.00							
125	Neve	0.00	0.00	0.24	0.04	-0.04	0.00							
126	QP Solai	0.00	0.00	1.98	0.31	0.30	0.00							
126	QFissi Solai	0.00	0.00	2.49	0.57	0.37	0.00							
126	QV Solai	0.00	0.00	3.04	0.70	0.45	0.00							
126	QV SolaiPsi0	0.00	0.00	2.13	0.49	0.32	0.00							
126	QV SolaiPsi1	0.00	0.00	2.13	0.49	0.32	0.00							
126	QV SolaiPsi2	0.00	0.00	1.82	0.42	0.27	0.00							
130	QP Solai	0.00	0.00	0.48	-0.07	-0.02	0.00							
130	QFissi Solai	0.00	0.00	1.15	-0.17	-0.23	0.00							
130	QV Solai	0.00	0.00	2.62	-0.39	-0.52	0.00							
130	QV SolaiPsi0	0.00	0.00	1.84	-0.28	-0.37	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
130	QV SolaiPsi1	0.00	0.00	1.84	-0.28	-0.37	0.00							
130	QV SolaiPsi2	0.00	0.00	1.57	-0.24	-0.31	0.00							
130	Neve	0.00	0.00	0.31	-0.05	-0.06	0.00							
204	QFissi Solai	0.00	0.00	0.04	0.00	0.00	0.00							
204	QV Solai	0.00	0.00	0.09	0.01	-0.01	0.00							
204	QV SolaiPsi0	0.00	0.00	0.06	0.01	-0.01	0.00							
204	QV SolaiPsi1	0.00	0.00	0.06	0.01	-0.01	0.00							
204	QV SolaiPsi2	0.00	0.00	0.05	0.00	-0.01	0.00							
204	Neve	0.00	0.00	0.01	0.00	0.00	0.00							
205	QFissi Solai	0.00	0.00	0.09	0.01	0.01	0.00							
205	QV Solai	0.00	0.00	0.21	0.03	0.02	0.00							
205	QV SolaiPsi0	0.00	0.00	0.15	0.02	0.01	0.00							
205	QV SolaiPsi1	0.00	0.00	0.15	0.02	0.01	0.00							
205	QV SolaiPsi2	0.00	0.00	0.12	0.02	0.01	0.00							
205	Neve	0.00	0.00	0.02	0.00	0.00	0.00							
206	QP Solai	0.00	0.00	0.30	0.04	-0.04	0.00							
206	QFissi Solai	0.00	0.00	0.76	0.15	-0.28	0.00							
206	QV Solai	0.00	0.00	1.72	0.34	-0.63	0.00							
206	QV SolaiPsi0	0.00	0.00	1.20	0.24	-0.44	0.00							
206	QV SolaiPsi1	0.00	0.00	1.20	0.24	-0.44	0.00							
206	QV SolaiPsi2	0.00	0.00	1.03	0.20	-0.38	0.00							
206	Neve	0.00	0.00	0.21	0.04	-0.08	0.00							
209	QFissi Solai	0.00	0.00	0.18	0.03	-0.01	0.00							
209	QV Solai	0.00	0.00	0.41	0.07	-0.02	0.00							
209	QV SolaiPsi0	0.00	0.00	0.29	0.05	-0.02	0.00							
209	QV SolaiPsi1	0.00	0.00	0.29	0.05	-0.02	0.00							
209	QV SolaiPsi2	0.00	0.00	0.24	0.04	-0.01	0.00							
209	Neve	0.00	0.00	0.05	0.01	0.00	0.00							
210	QFissi Solai	0.00	0.00	0.48	-0.04	-0.07	0.00							
210	QV Solai	0.00	0.00	1.10	-0.08	-0.16	0.00							
210	QV SolaiPsi0	0.00	0.00	0.77	-0.06	-0.12	0.00							
210	QV SolaiPsi1	0.00	0.00	0.77	-0.06	-0.12	0.00							
210	QV SolaiPsi2	0.00	0.00	0.66	-0.05	-0.10	0.00							
210	Neve	0.00	0.00	0.13	-0.01	-0.02	0.00							
211	QP Solai	0.00	0.00	0.41	-0.06	-0.06	0.00							
211	QP Solai	0.00	0.00	0.30	-0.04	-0.04	0.00							
211	QFissi Solai	0.00	0.00	0.27	-0.04	-0.06	0.00							
211	QFissi Solai	0.00	0.00	0.85	-0.09	-0.30	0.00							
211	QV Solai	0.00	0.00	1.94	-0.21	-0.68	0.00							
211	QV Solai	0.00	0.00	0.62	-0.09	-0.14	0.00							
211	QV SolaiPsi0	0.00	0.00	1.36	-0.15	-0.48	0.00							
211	QV SolaiPsi0	0.00	0.00	0.44	-0.07	-0.10	0.00							
211	QV SolaiPsi1	0.00	0.00	1.36	-0.15	-0.48	0.00							
211	QV SolaiPsi1	0.00	0.00	0.44	-0.07	-0.10	0.00							
211	QV SolaiPsi2	0.00	0.00	1.17	-0.13	-0.41	0.00							
211	QV SolaiPsi2	0.00	0.00	0.37	-0.06	-0.08	0.00							
211	Neve	0.00	0.00	0.23	-0.03	-0.08	0.00							
211	Neve	0.00	0.00	0.07	-0.01	-0.02	0.00							
214	QFissi Solai	0.00	0.00	0.21	0.04	0.00	0.00							
214	QFissi Solai	0.00	0.00	0.59	0.13	0.00	0.00							
214	QV Solai	0.00	0.00	1.34	0.29	0.00	0.00							
214	QV Solai	0.00	0.00	0.48	0.11	0.00	0.00							
214	QV SolaiPsi0	0.00	0.00	0.94	0.20	0.00	0.00							
214	QV SolaiPsi0	0.00	0.00	0.34	0.07	0.00	0.00							
214	QV SolaiPsi1	0.00	0.00	0.94	0.20	0.00	0.00							
214	QV SolaiPsi1	0.00	0.00	0.34	0.07	0.00	0.00							
214	QV SolaiPsi2	0.00	0.00	0.29	0.06	0.00	0.00							
214	QV SolaiPsi2	0.00	0.00	0.81	0.17	0.00	0.00							
214	Neve	0.00	0.00	0.05	0.01	0.00	0.00							
214	Neve	0.00	0.00	0.16	0.03	0.00	0.00							
216	QFissi Solai	0.00	0.00	0.59	0.00	-0.13	0.00							
216	QV Solai	0.00	0.00	1.35	0.00	-0.29	0.00							
216	QV SolaiPsi0	0.00	0.00	0.94	0.00	-0.20	0.00							
216	QV SolaiPsi1	0.00	0.00	0.94	0.00	-0.20	0.00							
216	QV SolaiPsi2	0.00	0.00	0.81	0.00	-0.17	0.00							
216	Neve	0.00	0.00	0.16	0.00	-0.03	0.00							
217	QP Solai	0.00	0.00	0.84	-0.13	0.13	0.00							
217	QFissi Solai	0.00	0.00	0.58	-0.09	0.11	0.00							
217	QV Solai	0.00	0.00	1.32	-0.21	0.25	0.00							
217	QV SolaiPsi0	0.00	0.00	0.92	-0.15	0.17	0.00							
217	QV SolaiPsi1	0.00	0.00	0.92	-0.15	0.17	0.00							

N°	Cond.	Fx	Fy	Fz	Mx	My	Mz	Tx	Ty	Tz	Rx	Ry	Rz	Δt
217	QV SolaiPsi2	0.00	0.00	0.79	-0.13	0.15	0.00							
217	Neve	0.00	0.00	0.15	-0.02	0.03	0.00							
218	QFissi Solai	0.00	0.00	0.21	-0.03	-0.02	0.00							
218	QV Solai	0.00	0.00	0.47	-0.07	-0.04	0.00							
218	QV SolaiPsi0	0.00	0.00	0.33	-0.05	-0.03	0.00							
218	QV SolaiPsi1	0.00	0.00	0.33	-0.05	-0.03	0.00							
218	QV SolaiPsi2	0.00	0.00	0.28	-0.04	-0.02	0.00							
218	Neve	0.00	0.00	0.06	-0.01	0.00	0.00							
219	QP Solai	0.00	0.00	0.41	-0.06	-0.06	0.00							
219	QFissi Solai	0.00	0.00	0.37	-0.06	-0.08	0.00							
219	QV Solai	0.00	0.00	0.85	-0.13	-0.19	0.00							
219	QV SolaiPsi0	0.00	0.00	0.59	-0.09	-0.13	0.00							
219	QV SolaiPsi1	0.00	0.00	0.59	-0.09	-0.13	0.00							
219	QV SolaiPsi2	0.00	0.00	0.51	-0.08	-0.11	0.00							
219	Neve	0.00	0.00	0.10	-0.02	-0.02	0.00							
222	QP Solai	0.00	0.00	0.14	-0.05	0.01	0.00							
222	QFissi Solai	0.00	0.00	1.83	-0.52	0.13	0.00							
222	QV Solai	0.00	0.00	4.15	-1.19	0.31	0.00							
222	QV SolaiPsi0	0.00	0.00	2.91	-0.83	0.21	0.00							
222	QV SolaiPsi1	0.00	0.00	2.91	-0.83	0.21	0.00							
222	QV SolaiPsi2	0.00	0.00	2.49	-0.71	0.18	0.00							
222	Neve	0.00	0.00	0.50	-0.14	0.03	0.00							
223	QFissi Solai	0.00	0.00	0.22	-0.05	0.01	0.00							
223	QV Solai	0.00	0.00	0.49	-0.12	0.03	0.00							
223	QV SolaiPsi0	0.00	0.00	0.34	-0.08	0.02	0.00							
223	QV SolaiPsi1	0.00	0.00	0.34	-0.08	0.02	0.00							
223	QV SolaiPsi2	0.00	0.00	0.29	-0.07	0.02	0.00							
223	Neve	0.00	0.00	0.06	-0.01	0.00	0.00							
225	QP Solai	0.00	0.00	1.94	0.31	-0.29	0.00							
225	QFissi Solai	0.00	0.00	1.76	0.41	-0.26	0.00							
225	QV Solai	0.00	0.00	3.99	0.93	-0.60	0.00							
225	QV SolaiPsi0	0.00	0.00	2.80	0.65	-0.42	0.00							
225	QV SolaiPsi1	0.00	0.00	2.80	0.65	-0.42	0.00							
225	QV SolaiPsi2	0.00	0.00	2.40	0.56	-0.36	0.00							
225	Neve	0.00	0.00	0.48	0.11	-0.07	0.00							
226	QP Solai	0.00	0.00	1.98	0.31	0.30	0.00							
226	QFissi Solai	0.00	0.00	1.78	0.41	0.27	0.00							
226	QV Solai	0.00	0.00	4.05	0.93	0.61	0.00							
226	QV SolaiPsi0	0.00	0.00	2.84	0.65	0.42	0.00							
226	QV SolaiPsi1	0.00	0.00	2.84	0.65	0.42	0.00							
226	QV SolaiPsi2	0.00	0.00	2.43	0.56	0.36	0.00							
226	Neve	0.00	0.00	0.49	0.11	0.07	0.00							

Input - Aste - Tabella sezioni tipo

Tipo	Nome	Base	Altezza	Larg.mag.
R		m	m	m
	60x25	0.60	0.25	0.00
	30x60	0.30	0.60	0.00
	60x30	0.60	0.30	0.00
	F50x100	0.50	1.00	0.90
	80x30	0.80	0.30	0.00
	125x30	1.25	0.30	0.00
	30x70	0.30	0.70	0.00
	30x50	0.30	0.50	0.00

Aste - Geometria e vincoli

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
							°		m							m	
2	2	102	I-I	125x30	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
3	3	103	I-I	80x30	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
4	4	104	I-I	80x30	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
4	104	204	I-I	80x30	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
5	5	105	I-I	60x30	C25/30	Pilastri	0.00	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
5	105	205	I-I	60x30	C25/30	Pilastri	0.00	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
6	6	106	I-I	60x30	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
6	106	206	I-I	60x30	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	-0.00	0.00	Pila.	3.75	3.75
7	7	107	I-I	80x30	C25/30	Pilastri	0.00	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
8	8	108	I-I	60x30	C25/30	Pilastri	-45.	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
9	9	109	I-I	30x70	C25/30	Pilastri	-45.	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
9	109	209	I-I	30x70	C25/30	Pilastri	-45.	3030	0.00	0.00	0.00	0.00	0.00	-0.00	Pila.	3.75	3.75
10	10	110	I-I	30x60	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
10	110	210	I-I	30x60	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
11	11	111	I-I	60x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
11	111	211	I-I	60x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	-0.00	0.00	Pila.	3.75	3.75
12	12	112	I-I	30x60	C25/30	Pilastri	0.00	6060	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
13	13	113	I-I	30x70	C25/30	Pilastri	-45.	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
13	113	213	I-I	30x70	C25/30	Pilastri	-45.	1010	0.00	0.00	0.00	0.00	-0.00	0.00	Pila.	3.75	3.75
14	14	37	I-I	30x60	C25/30	Pilastri tozzi	-45.	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	0.80	0.80
14	37	114	I-I	30x60	C25/30	Pilastri	-45.	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.59	3.59
14	114	214	I-I	30x60	C25/30	Pilastri	-45.	3030	0.00	0.00	0.00	0.00	-0.00	-0.00	Pila.	3.75	3.75
15	15	115	I-I	30x60	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
16	16	116	I-I	30x60	C25/30	Pilastri	-45.	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
16	116	216	I-I	30x60	C25/30	Pilastri	-45.	1010	0.00	0.00	0.00	0.00	-0.00	0.00	Pila.	3.75	3.75
17	17	35	I-I	30x70	C25/30	Pilastri	45.0	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	2.67	2.67
17	35	117	I-I	30x70	C25/30	Pilastri	45.0	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	1.72	1.72
17	117	217	I-I	30x70	C25/30	Pilastri	45.0	3030	0.00	0.00	0.00	0.00	-0.00	0.00	Pila.	3.75	3.75
18	18	118	I-I	60x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
18	118	218	I-I	60x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
19	19	119	I-I	60x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
19	119	219	I-I	60x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	-0.00	0.00	Pila.	3.75	3.75
20	20	120	I-I	30x60	C25/30	Pilastri	0.00	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
21	21	121	I-I	30x60	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
22	22	122	I-I	30x60	C25/30	Pilastri	0.00	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
22	122	222	I-I	30x60	C25/30	Pilastri	0.00	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
23	23	36	I-I	30x70	C25/30	Pilastri	45.0	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	2.67	2.67
23	36	123	I-I	30x70	C25/30	Pilastri	45.0	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	1.72	1.72
23	123	223	I-I	30x70	C25/30	Pilastri	45.0	9090	0.00	0.00	0.00	0.00	0.00	-0.00	Pila.	3.75	3.75
24	24	124	I-I	30x60	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
25	25	125	I-I	30x60	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
25	125	225	I-I	30x60	C25/30	Pilastri	0.00	1010	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
26	26	126	I-I	30x60	C25/30	Pilastri	0.00	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
26	126	226	I-I	30x60	C25/30	Pilastri	0.00	3030	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	3.75	3.75
27	27	127	I-I	80x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
28	28	128	I-I	80x30	C25/30	Pilastri	0.00	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
29	29	129	I-I	80x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
30	30	130	I-I	80x30	C25/30	Pilastri	0.00	7070	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
31	31	131	I-I	80x30	C25/30	Pilastri	0.00	9090	0.00	0.00	0.00	0.00	0.00	0.00	Pila.	4.39	4.39
101	129	130	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.34	5.34
101	130	131	I-I	30x50	C25/30	Travi alte	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Trave	6.14	6.14
102	124	125	I-I	30x50	C25/30	Travi alte	0.00	7171	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.45	5.45
102	125	126	I-I	30x50	C25/30	Travi alte	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Trave	6.04	6.04
103	121	122	I-I	30x50	C25/30	Travi alte	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.74	5.74
104	115	113	I-I	30x50	C25/30	Travi alte	0.00	9776	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.31	5.31
105	102	108	I-I	30x50	C25/30	Travi alte	0.00	9991	0.00	0.10	0.00	0.00	0.00	0.00	Trave	3.68	3.68
105	108	113	I-I	30x50	C25/30	Travi alte	0.00	9191	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.28	3.28
105	113	116	I-I	30x50	C25/30	Travi alte	0.00	9191	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.30	3.30
105	116	123	I-I	30x50	C25/30	Travi alte	0.00	9199	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.33	5.33
106	103	109	I-I	30x50	C25/30	Travi alte	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.28	3.28
106	109	114	I-I	30x50	C25/30	Travi alte	0.00	7373	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.30	3.30
106	114	117	I-I	30x50	C25/30	Travi alte	0.00	7373	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.33	5.33
107	102	103	I-I	30x50	C25/30	Travi alte	0.00	7171	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.14	5.14
107	103	104	I-I	30x50	C25/30	Travi alte	0.00	7171	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.63	4.63
107	104	105	I-I	30x50	C25/30	Travi alte	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.90	5.90
107	105	106	I-I	30x50	C25/30	Travi alte	0.00	7371	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.97	3.97
107	106	107	I-I	30x50	C25/30	Travi alte	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.30	5.30
108	107	112	I-I	30x50	C25/30	Travi alte	0.00	7376	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.77	3.77
108	112	120	I-I	30x50	C25/30	Travi alte	0.00	7679	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.70	4.70
108	120	128	I-I	30x50	C25/30	Travi alte	0.00	7979	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.13	4.13
109	106	111	I-I	30x50	C25/30	Travi alte	0.00	9197	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.77	3.77
109	111	119	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.70	4.70
110	119	127	I-I	30x50	C25/30	Travi alte	0.00	7997	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.14	4.14
111	102	115	I-I	30x50	C25/30	Travi alte	0.00	9197	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.82	4.82
111	115	121	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.31	4.31
111	121	124	I-I	30x50	C25/30	Travi alte	0.00	9791	0.00	0.00	0.00	0.00	0.00	0.00	Trave	2.88	2.88
111	124	129	I-I	30x50	C25/30	Travi alte	0.00	9197	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.40	4.40
112	113	122	I-I	30x50	C25/30	Travi alte	0.00	7679	0.00	-0.03	0.00	0.00	0.00	0.00	Trave	4.67	4.67
112	122	125	I-I	30x50	C25/30	Travi alte	0.00	7973	0.00	0.00	0.00	0.00	0.00	0.00	Trave	2.89	2.89
112	125	130	I-I	60x25	C25/30	Travi spessore	0.00	9197	0.00	0.00	0.00	0.00	-0.10	0.00	Trave	4.40	4.40
113	123	126	I-I	30x50	C25/30	Travi tozze	0.00	9773	0.00	0.00	0.00	0.00	0.00	0.00	Trave	1.43	1.43
113	126	131	I-I	30x50	C25/30	Travi alte	0.00	7379	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.40	4.40
114	116	114	I-I	30x50	C25/30	Travi alte	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.10	3.10

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
115	113	109	I-I	60x25	C25/30	Travi spessore	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.11	3.11
116	108	103	I-I	30x50	C25/30	Travi alte	0.00	7171	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.05	3.05
117	117	118	I-I	30x50	C25/30	Travi alte	0.00	7197	0.00	0.00	0.00	0.00	0.00	0.00	Trave	1.79	1.79
117	118	119	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.27	4.27
117	119	120	I-I	60x25	C25/30	Travi spessore	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.30	5.30
118	127	128	I-I	30x50	C25/30	Travi alte	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.00	5.00
119	110	111	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.27	4.27
119	111	112	I-I	30x50	C25/30	Travi alte	0.00	9796	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.30	5.30
120	105	110	I-I	30x50	C25/30	Travi alte	0.00	7397	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.78	3.78
120	110	118	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.70	4.70
121	104	114	I-I	30x50	C25/30	Travi alte	0.00	9194	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.62	4.62
122	36	35	I-I	30x50	C25/30	Travi alte	0.00	9993	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.10	3.10
123	39	116	I-C	30x50	C25/30	Travi alte	0.00	7777	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.99	3.99
123	36	39	C-I	30x50	C25/30	Travi alte	0.00	7770	0.00	0.00	0.00	0.00	0.00	0.00	Trave	1.73	1.73
201	225	226	I-I	30x50	C25/30	Travi alte	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Trave	6.04	6.04
202	213	216	I-I	30x50	C25/30	Travi alte	0.00	9191	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.30	3.30
202	216	223	I-I	30x50	C25/30	Travi alte	0.00	9199	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.33	5.33
203	213	222	I-I	30x50	C25/30	Travi alte	0.00	7679	0.00	-0.03	0.00	0.00	0.00	0.00	Trave	4.67	4.67
203	222	225	I-I	30x50	C25/30	Travi alte	0.00	9191	0.00	0.00	0.00	0.00	0.00	0.00	Trave	2.89	2.89
204	223	226	I-I	30x50	C25/30	Travi alte	0.00	9773	0.00	0.00	0.00	0.00	0.00	0.00	Trave	1.43	1.43
205	223	217	I-I	30x50	C25/30	Travi alte	0.00	9993	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.10	3.10
206	217	218	I-I	30x50	C25/30	Travi alte	0.00	9397	0.00	0.00	0.00	0.00	0.00	0.00	Trave	1.79	1.79
206	218	219	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.27	4.27
207	204	205	I-I	30x50	C25/30	Travi alte	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.90	5.90
207	205	206	I-I	30x50	C25/30	Travi alte	0.00	7371	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.97	3.97
208	209	214	I-I	30x50	C25/30	Travi alte	0.00	7373	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.30	3.30
208	214	217	I-I	30x50	C25/30	Travi alte	0.00	7373	0.00	0.00	0.00	0.00	0.00	0.00	Trave	5.33	5.33
209	204	209	I-I	30x50	C25/30	Travi alte	0.00	9193	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.23	3.23
209	209	213	I-I	30x50	C25/30	Travi alte	0.00	9391	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.11	3.11
210	214	216	I-I	60x25	C25/30	Travi spessore	0.00	9391	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.10	3.10
211	204	214	I-I	30x50	C25/30	Travi alte	0.00	9194	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.62	4.62
212	205	210	I-I	30x50	C25/30	Travi alte	0.00	7397	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.78	3.78
212	210	218	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.70	4.70
213	206	211	I-I	30x50	C25/30	Travi alte	0.00	7979	0.00	0.00	0.00	0.00	0.00	0.00	Trave	3.77	3.77
213	211	219	I-I	30x50	C25/30	Travi alte	0.00	7979	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.70	4.70
214	210	211	I-I	30x50	C25/30	Travi alte	0.00	9797	0.00	-0.00	0.00	0.00	-0.00	0.00	Trave	4.27	4.27
8000	37	38	C-I	30x50	C25/30	Travi alte	0.00	7373	0.00	0.00	0.00	0.00	0.00	0.00	Trave	4.05	4.05
8000	38	35	I-C	30x50	C25/30	Travi alte	0.00	7073	0.00	0.00	0.00	0.00	0.00	0.00	Trave	1.73	1.73
9001	2	3	I-I	F50x100	C25/30	Fond	0.00	7171	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	5.14	5.14
9001	3	4	I-I	F50x100	C25/30	Fond	0.00	7171	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	4.63	4.63
9001	4	5	I-I	F50x100	C25/30	Fond	0.00	7173	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	5.90	5.90
9001	5	6	I-I	F50x100	C25/30	Fond	0.00	7371	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	3.97	3.97
9001	6	7	I-I	F50x100	C25/30	Fond	0.00	7173	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	5.30	5.30
9002	10	11	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	4.27	4.27
9002	11	12	I-I	F50x100	C25/30	Fond	0.00	9796	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	5.30	5.30
9003	17	18	I-I	F50x100	C25/30	Fond	0.00	9397	0.00	0.10	0.00	0.00	0.00	0.00	Fond.	1.79	1.79
9003	18	19	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	4.27	4.27
9003	19	20	I-I	F50x100	C25/30	Fond	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	5.30	5.30
9004	27	28	I-I	F50x100	C25/30	Fond	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	5.00	5.00
9005	15	13	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	0.00	0.00	0.00	-0.15	0.00	Fond.	5.31	5.31
9006	21	22	I-I	F50x100	C25/30	Fond	0.00	9799	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	5.74	5.74
9007	24	25	I-I	F50x100	C25/30	Fond	0.00	7171	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	5.45	5.45
9007	25	26	I-I	F50x100	C25/30	Fond	0.00	7173	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	6.04	6.04
9008	29	30	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	5.34	5.34
9008	30	31	I-I	F50x100	C25/30	Fond	0.00	9799	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	6.14	6.14
9009	2	15	I-I	F50x100	C25/30	Fond	0.00	9197	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	4.82	4.82
9009	15	21	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	4.31	4.31
9009	21	24	I-I	F50x100	C25/30	Fond	0.00	9791	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	2.88	2.88
9009	24	29	I-I	F50x100	C25/30	Fond	0.00	9197	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	4.40	4.40
9010	13	22	I-I	F50x100	C25/30	Fond	0.00	7679	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	4.67	4.67
9010	22	25	I-I	F50x100	C25/30	Fond	0.00	7973	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	2.89	2.89
9010	25	30	I-I	F50x100	C25/30	Fond	0.00	9197	0.00	0.10	0.00	0.00	0.00	0.00	Fond.	4.40	4.40
9011	23	26	I-I	F50x100	C25/30	Fond	0.00	7473	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	1.43	1.43
9011	26	31	I-I	F50x100	C25/30	Fond	0.00	7379	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	4.40	4.40
9012	2	8	I-I	F50x100	C25/30	Fond	0.00	9991	0.00	0.20	0.00	0.00	0.10	0.00	Fond.	3.68	3.68
9012	8	13	I-I	F50x100	C25/30	Fond	0.00	9191	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	3.28	3.28
9012	13	16	I-I	F50x100	C25/30	Fond	0.00	9191	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	3.30	3.30
9012	16	23	I-I	F50x100	C25/30	Fond	0.00	9199	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	5.33	5.33
9013	3	9	I-I	F50x100	C25/30	Fond	0.00	7173	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	3.28	3.28
9013	9	14	I-I	F50x100	C25/30	Fond	0.00	7373	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	3.30	3.30
9013	14	17	I-I	F50x100	C25/30	Fond	0.00	7373	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	5.33	5.33
9014	17	23	I-I	F50x100	C25/30	Fond	0.00	7379	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	3.10	3.10
9015	14	16	I-I	F50x100	C25/30	Fond	0.00	9391	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	3.10	3.10
9016	9	13	I-I	F50x100	C25/30	Fond	0.00	9391	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	3.11	3.11
9017	3	8	I-I	F50x100	C25/30	Fond	0.00	9191	0.00	0.00	0.00	0.00	0.00	0.00	Fond.	3.05	3.05
9018	4	14	I-I	F50x100	C25/30	Fond	0.00	9192	0.00	0.10	0.00	0.00	0.00	0.00	Fond.	4.62	4.62
9019	5	10	I-I	F50x100	C25/30	Fond	0.00	9297	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	3.78	3.78
9019	10	18	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	4.70	4.70

	Ni	Nf	Vinc.	Sez.	Mat.	Crit.pr.	Rot.	f.f.	xi	yi	zi	xf	yf	zf	Tipo	L2	L3
9020	6	11	I-I	F50x100	C25/30	Fond	0.00	9197	0.00	-0.20	0.00	0.00	-0.20	0.00	Fond.	3.77	3.77
9020	11	19	I-I	F50x100	C25/30	Fond	0.00	9797	0.00	-0.20	0.00	0.00	-0.20	0.00	Fond.	4.70	4.70
9020	19	27	I-I	F50x100	C25/30	Fond	0.00	9897	0.00	0.10	0.00	0.00	0.10	0.00	Fond.	4.14	4.14
9021	7	12	I-I	F50x100	C25/30	Fond	0.00	7376	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	3.77	3.77
9021	12	20	I-I	F50x100	C25/30	Fond	0.00	7679	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	4.70	4.70
9021	20	28	I-I	F50x100	C25/30	Fond	0.00	7979	0.00	-0.10	0.00	0.00	-0.10	0.00	Fond.	4.13	4.13

Aste - Carichi

Tabella degli elementi di carico sbalzo: lo sbalzo genera sull'asta a cui è collegato tutte le tipologie di carico generate dal solaio ad esso assegnato; nella tabella dei carichi delle aste il carico generato dallo sbalzo è indicato con (Sb.NN) con NN indice dello sbalzo.

Asta Asta a cui è collegato lo sbalzo
L Lunghezza dell'asta
N1, N2 nodi dell'asta
Xi Distanza dal nodo iniziale dell'asta del punto iniziale dello sbalzo
Bi Larghezza iniziale dello sbalzo
Xf Distanza dal nodo iniziale dell'asta del punto fiale dello sbalzo
Bf Larghezza finale dello sbalzo
Stipo Solaio tipo assegnato allo sbalzo

N° Sb.	Asta	L	N1	N2	Xi	Bi	Xf	Bf	STipo
		cm			m	m	m	m	
1	8000	4.05	37	38	0.00	1.50	4.05	1.50	Scala
2	8000	1.73	38	35	0.00	1.50	1.73	1.50	Scala
3	123	1.43	36	39	0.00	1.50	1.43	1.50	Scala
4	123	3.45	39	116	0.00	1.50	3.45	1.50	Scala
5	122	3.10	36	35	0.00	1.73	3.10	1.73	Scala
5	101	5.34	129	130	0.00	0.80	5.34	0.80	Terrazzo
6	111	4.40	124	129	0.00	0.80	4.40	0.80	Terrazzo
7	111	2.88	121	124	0.00	0.80	2.88	0.80	Terrazzo
8	111	4.31	115	121	0.00	0.80	4.31	0.80	Terrazzo
9	111	4.82	102	115	0.00	0.80	4.82	0.80	Terrazzo
10	107	5.14	102	103	0.00	0.80	5.14	0.80	Terrazzo
11	107	4.63	103	104	0.00	0.80	4.63	0.80	Terrazzo
12	107	5.90	104	105	0.00	0.80	5.90	0.80	Terrazzo
13	107	3.97	105	106	0.00	0.80	3.97	0.80	Terrazzo
14	107	5.30	106	107	0.00	0.80	5.30	0.80	Terrazzo
15	108	3.77	107	112	0.00	0.80	3.77	0.80	Terrazzo
16	108	4.70	112	120	0.00	0.80	4.70	0.80	Terrazzo
17	108	4.13	120	128	0.00	0.80	4.13	0.80	Terrazzo
18	118	5.00	127	128	0.00	0.80	5.00	0.80	Terrazzo
19	110	4.11	119	127	0.00	0.80	4.11	0.80	Terrazzo
20	117	4.27	118	119	0.00	0.80	4.27	0.80	Terrazzo
21	117	2.01	117	118	0.00	0.80	2.01	0.80	Terrazzo
22	113	1.66	123	126	0.00	0.80	1.66	0.80	Terrazzo
23	113	4.40	126	131	0.00	0.80	4.40	0.80	Terrazzo
24	101	6.14	130	131	0.00	0.80	6.14	0.80	Terrazzo
25	207	5.90	204	205	0.00	0.80	5.90	0.80	Terrazzo
26	207	3.97	205	206	0.00	0.80	3.97	0.80	Terrazzo
27	213	3.47	206	211	0.00	0.80	3.47	0.80	Terrazzo
28	213	4.70	211	219	0.00	0.80	4.70	0.80	Terrazzo
29	206	4.27	218	219	0.00	0.80	4.27	0.80	Terrazzo
30	206	1.79	217	218	0.00	0.80	1.79	0.80	Terrazzo
31	205	3.10	223	217	0.00	0.80	3.10	0.80	Terrazzo
32	204	1.66	223	226	0.00	0.80	1.66	0.80	Terrazzo
33	201	6.04	225	226	0.00	0.80	6.04	0.80	Terrazzo
34	203	3.48	222	225	0.00	0.80	3.48	0.80	Terrazzo
35	203	4.61	213	222	0.00	0.80	4.61	0.80	Terrazzo
36	209	3.11	209	213	0.00	0.80	3.11	0.80	Terrazzo
37	209	3.23	204	209	0.00	0.80	3.23	0.80	Terrazzo

Descrizione carichi aste

UnifG	Uniforme globale
UnifL	Uniforme locale
VarG	Variabile lineare globale
VarL	Variabile lineare locale
PolG	Poligonale globale
Termico	Distorsione termica
Torcente	Carico torcente
Precomp.	Carico da precompressione
PolL	Poligonale locale

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					m	car. dist. kN/m coppie torc. kN			m	car. dist. kN/m coppie torc. kN		
Pilastro 2												
125x30	2	102	Peso Proprio	UnifG	0.00	0.00	0.00	9.38	4.39	0.00	0.00	9.38
125x30	2	102	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 3												
80x30	3	103	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	3	103	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 4												
80x30	4	104	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	4	104	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
80x30	104	204	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	3.75	0.00	0.00	6.00
80x30	104	204	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 5												
60x30	5	105	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
60x30	5	105	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
60x30	105	205	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
60x30	105	205	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 6												
60x30	6	106	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
60x30	6	106	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
60x30	106	206	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
60x30	106	206	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 7												
80x30	7	107	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	7	107	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 8												
60x30	8	108	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
60x30	8	108	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 9												
30x70	9	109	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	4.39	0.00	0.00	5.25
30x70	9	109	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x70	109	209	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	3.75	0.00	0.00	5.25
30x70	109	209	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 10												
30x60	10	110	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	10	110	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	110	210	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
30x60	110	210	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 11												
60x30	11	111	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
60x30	11	111	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
60x30	111	211	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
60x30	111	211	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 12												
30x60	12	112	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	12	112	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 13												
30x70	13	113	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	4.39	0.00	0.00	5.25
30x70	13	113	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x70	113	213	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	3.75	0.00	0.00	5.25

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x70	113	213	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 14												
30x60	14	37	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	0.80	0.00	0.00	4.50
30x60	14	37	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	37	114	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.59	0.00	0.00	4.50
30x60	37	114	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	114	214	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
30x60	114	214	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 15												
30x60	15	115	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	15	115	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 16												
30x60	16	116	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	16	116	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	116	216	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
30x60	116	216	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 17												
30x70	17	35	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	2.67	0.00	0.00	5.25
30x70	17	35	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x70	35	117	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	1.72	0.00	0.00	5.25
30x70	35	117	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x70	117	217	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	3.75	0.00	0.00	5.25
30x70	117	217	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 18												
60x30	18	118	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
60x30	18	118	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
60x30	118	218	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
60x30	118	218	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 19												
60x30	19	119	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
60x30	19	119	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
60x30	119	219	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
60x30	119	219	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 20												
30x60	20	120	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	20	120	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 21												
30x60	21	121	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	21	121	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 22												
30x60	22	122	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	22	122	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	122	222	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
30x60	122	222	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 23												
30x70	23	36	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	2.67	0.00	0.00	5.25
30x70	23	36	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x70	36	123	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	1.72	0.00	0.00	5.25
30x70	36	123	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x70	123	223	Peso Proprio	UnifG	0.00	0.00	0.00	5.25	3.75	0.00	0.00	5.25
30x70	123	223	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 24												
30x60	24	124	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	24	124	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 25												
30x60	25	125	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	25	125	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	125	225	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50
30x60	125	225	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 26												
30x60	26	126	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	4.39	0.00	0.00	4.50
30x60	26	126	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x60	126	226	Peso Proprio	UnifG	0.00	0.00	0.00	4.50	3.75	0.00	0.00	4.50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x60	126	226	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 27												
80x30	27	127	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	27	127	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 28												
80x30	28	128	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	28	128	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 29												
80x30	29	129	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	29	129	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 30												
80x30	30	130	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	30	130	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Pilastro 31												
80x30	31	131	Peso Proprio	UnifG	0.00	0.00	0.00	6.00	4.39	0.00	0.00	6.00
80x30	31	131	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 101												
30x50	129	130	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.34	0.00	0.00	3.75
30x50	129	130	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	7.26	5.34	0.00	0.00	7.26
30x50	129	130	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	4.29	5.34	0.00	0.00	4.29
30x50	129	130	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	9.76	5.34	0.00	0.00	9.76
30x50	129	130	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	6.83	5.34	0.00	0.00	6.83
30x50	129	130	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	6.83	5.34	0.00	0.00	6.83
30x50	129	130	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	5.86	5.34	0.00	0.00	5.86
30x50	129	130	Neve(Sb.5)	PolG	0.00	0.00	0.00	0.38	5.34	0.00	0.00	0.38
30x50	129	130	Neve	PolG	0.15	0.00	0.00	0.79	5.34	0.00	0.00	0.79
30x50	129	130	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	130	131	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.14	0.00	0.00	3.75
30x50	130	131	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.70	0.00	0.00	2.50
					0.70	0.00	0.00	6.88	5.84	0.00	0.00	6.88
					5.84	0.00	0.00	2.50	6.14	0.00	0.00	2.50
30x50	130	131	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.40	0.00	0.00	1.41
					0.40	0.00	0.00	4.08	5.99	0.00	0.00	4.08
					5.99	0.00	0.00	1.41	6.14	0.00	0.00	1.41
30x50	130	131	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.40	0.00	0.00	3.20
					0.40	0.00	0.00	9.28	5.99	0.00	0.00	9.28
					5.99	0.00	0.00	3.20	6.14	0.00	0.00	3.20
30x50	130	131	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.40	0.00	0.00	2.24
					0.40	0.00	0.00	6.49	5.99	0.00	0.00	6.49
					5.99	0.00	0.00	2.24	6.14	0.00	0.00	2.24
30x50	130	131	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.40	0.00	0.00	2.24
					0.40	0.00	0.00	6.49	5.99	0.00	0.00	6.49
					5.99	0.00	0.00	2.24	6.14	0.00	0.00	2.24
30x50	130	131	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.40	0.00	0.00	1.92
					0.40	0.00	0.00	5.57	5.99	0.00	0.00	5.57
					5.99	0.00	0.00	1.92	6.14	0.00	0.00	1.92
30x50	130	131	Neve(Sb.24)	PolG	0.00	0.00	0.00	0.38	6.14	0.00	0.00	0.38
30x50	130	131	Neve	PolG	0.40	0.00	0.00	0.73	5.99	0.00	0.00	0.73
30x50	130	131	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 102												
30x50	124	125	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.45	0.00	0.00	3.75
30x50	124	125	QP Solai	PolG	0.30	0.00	0.00	8.36	5.45	0.00	0.00	8.36
30x50	124	125	QFissi Solai	PolG	0.15	0.00	0.00	5.12	5.45	0.00	0.00	5.12
30x50	124	125	QV Solai	PolG	0.15	0.00	0.00	11.64	5.45	0.00	0.00	11.64
30x50	124	125	QV SolaiPsi0	PolG	0.15	0.00	0.00	8.15	5.45	0.00	0.00	8.15
30x50	124	125	QV SolaiPsi1	PolG	0.15	0.00	0.00	8.15	5.45	0.00	0.00	8.15
30x50	124	125	QV SolaiPsi2	PolG	0.15	0.00	0.00	6.98	5.45	0.00	0.00	6.98

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	124	125	Neve	PolG	0.15	0.00	0.00	0.61	5.45	0.00	0.00	0.61
30x50	124	125	Neve	PolG	0.15	0.00	0.00	0.79	5.45	0.00	0.00	0.79
30x50	124	125	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	125	126	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.04	0.00	0.00	3.75
30x50	125	126	QP Solai	PolG	0.34	0.00	0.00	2.30	0.60	0.00	0.00	2.22
					0.60	0.00	0.00	6.60	2.19	0.00	0.00	6.10
					2.19	0.00	0.00	6.10	5.74	0.00	0.00	4.99
30x50	125	126	QFissi Solai	PolG	0.15	0.00	0.00	1.93	0.30	0.00	0.00	1.89
					0.30	0.00	0.00	4.57	2.30	0.00	0.00	4.09
					2.30	0.00	0.00	4.09	5.90	0.00	0.00	3.20
30x50	125	126	QV Solai	PolG	0.15	0.00	0.00	2.35	0.30	0.00	0.00	2.31
					0.30	0.00	0.00	8.39	2.30	0.00	0.00	7.80
					2.30	0.00	0.00	7.80	5.90	0.00	0.00	6.72
30x50	125	126	QV SolaiPsi0	PolG	0.15	0.00	0.00	1.65	0.30	0.00	0.00	1.62
					0.30	0.00	0.00	5.87	2.30	0.00	0.00	5.46
					2.30	0.00	0.00	5.46	5.90	0.00	0.00	4.71
30x50	125	126	QV SolaiPsi1	PolG	0.15	0.00	0.00	1.65	0.30	0.00	0.00	1.62
					0.30	0.00	0.00	5.87	2.30	0.00	0.00	5.46
					2.30	0.00	0.00	5.46	5.90	0.00	0.00	4.71
30x50	125	126	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.41	0.30	0.00	0.00	1.39
					0.30	0.00	0.00	5.03	2.30	0.00	0.00	4.68
					2.30	0.00	0.00	4.68	5.90	0.00	0.00	4.03
30x50	125	126	Neve	PolG	0.30	0.00	0.00	0.73	5.89	0.00	0.00	0.73
30x50	125	126	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	125	126	Tamponamento	PolG	0.00	0.00	0.00	7.80	6.04	0.00	0.00	7.80
Trave 103												
30x50	121	122	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.74	0.00	0.00	3.75
30x50	121	122	QP Solai	PolG	0.30	0.00	0.00	8.62	5.45	0.00	0.00	8.62
30x50	121	122	QFissi Solai	PolG	0.15	0.00	0.00	5.27	5.60	0.00	0.00	5.27
30x50	121	122	QV Solai	PolG	0.15	0.00	0.00	11.97	5.60	0.00	0.00	11.98
30x50	121	122	QV SolaiPsi0	PolG	0.15	0.00	0.00	8.38	5.60	0.00	0.00	8.38
30x50	121	122	QV SolaiPsi1	PolG	0.15	0.00	0.00	8.38	5.60	0.00	0.00	8.38
30x50	121	122	QV SolaiPsi2	PolG	0.15	0.00	0.00	7.18	5.60	0.00	0.00	7.19
30x50	121	122	Neve	PolG	0.15	0.00	0.00	0.61	5.60	0.00	0.00	0.61
30x50	121	122	Neve	PolG	0.15	0.00	0.00	0.83	5.60	0.00	0.00	0.83
30x50	121	122	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 104												
30x50	115	113	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.78	0.00	0.00	3.75
30x50	115	113	QP Solai	PolG	0.31	0.00	0.00	6.59	2.98	0.00	0.00	5.76
					2.98	0.00	0.00	5.76	5.34	0.00	0.00	5.02
					5.34	0.00	0.00	5.02	5.46	0.00	0.00	5.02
					5.46	0.00	0.00	0.00	5.50	0.00	0.00	0.00
30x50	115	113	QFissi Solai	PolG	0.16	0.00	0.00	4.00	3.08	0.00	0.00	3.50
					3.08	0.00	0.00	3.50	5.65	0.00	0.00	3.05
					5.65	0.00	0.00	0.01	5.71	0.00	0.00	0.00
30x50	115	113	QV Solai	PolG	0.16	0.00	0.00	9.10	3.08	0.00	0.00	7.95
					3.08	0.00	0.00	7.95	5.65	0.00	0.00	6.92
					5.65	0.00	0.00	0.03	5.71	0.00	0.00	0.00
30x50	115	113	QV SolaiPsi0	PolG	0.16	0.00	0.00	6.37	3.08	0.00	0.00	5.56
					3.08	0.00	0.00	5.56	5.65	0.00	0.00	4.84
					5.65	0.00	0.00	0.02	5.71	0.00	0.00	0.00
30x50	115	113	QV SolaiPsi1	PolG	0.16	0.00	0.00	6.37	3.08	0.00	0.00	5.56
					3.08	0.00	0.00	5.56	5.65	0.00	0.00	4.84
					5.65	0.00	0.00	0.02	5.71	0.00	0.00	0.00
30x50	115	113	QV SolaiPsi2	PolG	0.16	0.00	0.00	5.46	3.08	0.00	0.00	4.77
					3.08	0.00	0.00	4.77	5.65	0.00	0.00	4.15
					5.65	0.00	0.00	0.02	5.71	0.00	0.00	0.00
30x50	115	113	Neve	PolG	0.16	0.00	0.00	0.00	5.71	0.00	0.00	0.00
30x50	115	113	Neve	PolG	0.16	0.00	0.00	0.83	5.65	0.00	0.00	0.83
30x50	115	113	Neve	PolG	0.16	0.00	0.00	0.00	5.65	0.00	0.00	0.00
30x50	115	113	Neve	PolG	0.16	0.00	0.00	0.27	3.08	0.00	0.00	0.13
					3.08	0.00	0.00	0.13	5.71	0.00	0.00	0.00
30x50	115	113	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 105												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	102	108	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	2.52	0.00	0.00	3.75
30x50	102	108	QP Solai	PolG	0.00	0.00	0.00	1.69	0.21	0.00	0.00	1.79
					0.21	0.00	0.00	1.79	2.52	0.00	0.00	5.76
30x50	102	108	QFissi Solai	PolG	0.00	0.00	0.00	1.22	2.52	0.00	0.00	3.66
30x50	102	108	QV Solai	PolG	0.00	0.00	0.00	2.77	2.52	0.00	0.00	8.31
30x50	102	108	QV SolaiPsi0	PolG	0.00	0.00	0.00	1.94	2.52	0.00	0.00	5.82
30x50	102	108	QV SolaiPsi1	PolG	0.00	0.00	0.00	1.94	2.52	0.00	0.00	5.82
30x50	102	108	QV SolaiPsi2	PolG	0.00	0.00	0.00	1.66	2.52	0.00	0.00	4.99
30x50	102	108	Neve	PolG	0.00	0.00	0.00	0.15	2.52	0.00	0.00	0.39
30x50	102	108	Neve	PolG	0.00	0.00	0.00	0.15	2.52	0.00	0.00	0.09
30x50	102	108	Neve	PolG	0.00	0.00	0.00	0.03	2.52	0.00	0.00	0.51
30x50	102	108	Neve	PolG	0.00	0.00	0.00	0.00	2.52	0.00	0.00	0.00
30x50	102	108	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	108	113	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.28	0.00	0.00	3.75
30x50	108	113	QP Solai	PolG	0.00	0.00	0.00	2.90	0.30	0.00	0.00	3.05
					0.30	0.00	0.00	6.12	3.28	0.00	0.00	7.58
30x50	108	113	QFissi Solai	PolG	0.00	0.00	0.00	1.79	0.15	0.00	0.00	1.83
					0.15	0.00	0.00	3.77	3.28	0.00	0.00	4.63
30x50	108	113	QV Solai	PolG	0.00	0.00	0.00	4.07	0.15	0.00	0.00	4.16
					0.15	0.00	0.00	8.57	3.28	0.00	0.00	10.53
30x50	108	113	QV SolaiPsi0	PolG	0.00	0.00	0.00	2.85	0.15	0.00	0.00	2.91
					0.15	0.00	0.00	6.00	3.28	0.00	0.00	7.37
30x50	108	113	QV SolaiPsi1	PolG	0.00	0.00	0.00	2.85	0.15	0.00	0.00	2.91
					0.15	0.00	0.00	6.00	3.28	0.00	0.00	7.37
30x50	108	113	QV SolaiPsi2	PolG	0.00	0.00	0.00	2.44	0.15	0.00	0.00	2.50
					0.15	0.00	0.00	5.14	3.28	0.00	0.00	6.32
30x50	108	113	Neve	PolG	0.15	0.00	0.00	0.53	3.28	0.00	0.00	0.54
30x50	108	113	Neve	PolG	0.00	0.00	0.00	0.40	3.28	0.00	0.00	0.71
30x50	108	113	Neve	PolG	0.00	0.00	0.00	0.09	3.28	0.00	0.00	0.01
30x50	108	113	Neve	PolG	0.15	0.00	0.00	0.00	3.28	0.00	0.00	0.00
30x50	108	113	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	113	116	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.30	0.00	0.00	3.75
30x50	113	116	QP Solai	PolG	0.60	0.00	0.00	3.14	0.69	0.00	0.00	3.14
					0.69	0.00	0.00	4.76	3.30	0.00	0.00	6.00
30x50	113	116	QFissi Solai	PolG	0.30	0.00	0.00	2.76	0.33	0.00	0.00	2.76
					0.33	0.00	0.00	4.13	3.30	0.00	0.00	5.23
30x50	113	116	QV Solai	PolG	0.30	0.00	0.00	3.37	0.33	0.00	0.00	3.37
					0.33	0.00	0.00	5.03	3.30	0.00	0.00	6.38
30x50	113	116	QV SolaiPsi0	PolG	0.30	0.00	0.00	2.36	0.33	0.00	0.00	2.36
					0.33	0.00	0.00	3.52	3.30	0.00	0.00	4.47
30x50	113	116	QV SolaiPsi1	PolG	0.30	0.00	0.00	2.36	0.33	0.00	0.00	2.36
					0.33	0.00	0.00	3.52	3.30	0.00	0.00	4.47
30x50	113	116	QV SolaiPsi2	PolG	0.30	0.00	0.00	2.02	0.33	0.00	0.00	2.02
					0.33	0.00	0.00	3.02	3.30	0.00	0.00	3.83
30x50	113	116	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	116	123	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.33	0.00	0.00	3.75
30x50	116	123	QP Solai	PolG	0.00	0.00	0.00	2.87	3.25	0.00	0.00	4.42
					3.25	0.00	0.00	0.71	3.30	0.00	0.00	0.70
					3.30	0.00	0.00	4.44	5.02	0.00	0.00	5.25
30x50	116	123	QFissi Solai	PolG	0.00	0.00	0.00	2.48	3.40	0.00	0.00	3.75
					3.40	0.00	0.00	3.75	5.09	0.00	0.00	4.37
30x50	116	123	QV Solai	PolG	0.00	0.00	0.00	3.02	3.40	0.00	0.00	4.57
					3.40	0.00	0.00	4.57	5.09	0.00	0.00	5.33
30x50	116	123	QV SolaiPsi0	PolG	0.00	0.00	0.00	2.12	3.40	0.00	0.00	3.20
					3.40	0.00	0.00	3.20	5.09	0.00	0.00	3.73
30x50	116	123	QV SolaiPsi1	PolG	0.00	0.00	0.00	2.12	3.40	0.00	0.00	3.20
					3.40	0.00	0.00	3.20	5.09	0.00	0.00	3.73
30x50	116	123	QV SolaiPsi2	PolG	0.00	0.00	0.00	1.81	3.40	0.00	0.00	2.74
					3.40	0.00	0.00	2.74	5.09	0.00	0.00	3.20
30x50	116	123	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	116	123	Tamponamento	PolG	0.00	0.00	0.00	7.80	5.33	0.00	0.00	7.80
Trave 106												
30x50	103	109	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.28	0.00	0.00	3.75
30x50	103	109	QP Solai	PolG	0.30	0.00	0.00	3.09	0.43	0.00	0.00	3.09

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					0.43	0.00	0.00	3.09	3.28	0.00	0.00	6.66
30x50	103	109	QFissi Solai	PolG	0.06	0.00	0.00	0.00	0.15	0.00	0.00	0.06
					0.15	0.00	0.00	2.01	3.28	0.00	0.00	4.21
30x50	103	109	QV Solai	PolG	0.06	0.00	0.00	0.00	0.15	0.00	0.00	0.14
					0.15	0.00	0.00	4.56	3.28	0.00	0.00	9.58
30x50	103	109	QV SolaiPsi0	PolG	0.06	0.00	0.00	0.00	0.15	0.00	0.00	0.10
					0.15	0.00	0.00	3.19	3.28	0.00	0.00	6.71
30x50	103	109	QV SolaiPsi1	PolG	0.06	0.00	0.00	0.00	0.15	0.00	0.00	0.10
					0.15	0.00	0.00	3.19	3.28	0.00	0.00	6.71
30x50	103	109	QV SolaiPsi2	PolG	0.06	0.00	0.00	0.00	0.15	0.00	0.00	0.08
					0.15	0.00	0.00	2.74	3.28	0.00	0.00	5.75
30x50	103	109	Neve	PolG	0.06	0.00	0.00	0.00	3.28	0.00	0.00	0.61
30x50	103	109	Neve	PolG	0.15	0.00	0.00	0.53	3.28	0.00	0.00	0.54
30x50	103	109	Neve	PolG	0.15	0.00	0.00	0.00	3.28	0.00	0.00	0.00
30x50	103	109	Neve	PolG	0.06	0.00	0.00	0.00	3.28	0.00	0.00	0.00
30x50	103	109	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	109	114	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.30	0.00	0.00	3.75
30x50	109	114	QP Solai	PolG	0.00	0.00	0.00	3.51	0.21	0.00	0.00	3.78
					0.21	0.00	0.00	3.78	0.60	0.00	0.00	3.31
					0.60	0.00	0.00	6.44	3.30	0.00	0.00	3.13
30x50	109	114	QFissi Solai	PolG	0.00	0.00	0.00	2.23	0.21	0.00	0.00	2.38
					0.21	0.00	0.00	2.38	0.30	0.00	0.00	2.32
					0.30	0.00	0.00	5.08	3.30	0.00	0.00	3.00
30x50	109	114	QV Solai	PolG	0.00	0.00	0.00	5.07	0.21	0.00	0.00	5.41
					0.21	0.00	0.00	5.41	0.30	0.00	0.00	5.27
					0.30	0.00	0.00	8.64	3.30	0.00	0.00	3.93
30x50	109	114	QV SolaiPsi0	PolG	0.00	0.00	0.00	3.55	0.21	0.00	0.00	3.78
					0.21	0.00	0.00	3.78	0.30	0.00	0.00	3.69
					0.30	0.00	0.00	6.04	3.30	0.00	0.00	2.75
30x50	109	114	QV SolaiPsi1	PolG	0.00	0.00	0.00	3.55	0.21	0.00	0.00	3.78
					0.21	0.00	0.00	3.78	0.30	0.00	0.00	3.69
					0.30	0.00	0.00	6.04	3.30	0.00	0.00	2.75
30x50	109	114	QV SolaiPsi2	PolG	0.00	0.00	0.00	3.04	0.21	0.00	0.00	3.24
					0.21	0.00	0.00	3.24	0.30	0.00	0.00	3.16
					0.30	0.00	0.00	5.18	3.30	0.00	0.00	2.36
30x50	109	114	Neve	PolG	0.00	0.00	0.00	0.61	0.21	0.00	0.00	0.65
					0.21	0.00	0.00	0.65	3.30	0.00	0.00	0.07
30x50	109	114	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	114	117	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.33	0.00	0.00	3.75
30x50	114	117	QP Solai	PolG	0.42	0.00	0.00	5.67	5.03	0.00	0.00	3.51
30x50	114	117	QFissi Solai	PolG	0.36	0.00	0.00	4.70	5.09	0.00	0.00	2.96
30x50	114	117	QV Solai	PolG	0.36	0.00	0.00	5.74	5.09	0.00	0.00	3.61
30x50	114	117	QV SolaiPsi0	PolG	0.36	0.00	0.00	4.02	5.09	0.00	0.00	2.53
30x50	114	117	QV SolaiPsi1	PolG	0.36	0.00	0.00	4.02	5.09	0.00	0.00	2.53
30x50	114	117	QV SolaiPsi2	PolG	0.36	0.00	0.00	3.44	5.09	0.00	0.00	2.17
30x50	114	117	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	114	117	Tamponamento	PolG	-0.00	0.00	0.00	7.80	5.33	0.00	0.00	7.80
Trave 107												
30x50	102	103	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.14	0.00	0.00	3.75
30x50	102	103	QP Solai(Sb.10)	PolG	-0.00	0.00	0.00	2.50	1.53	0.00	0.00	2.50
					1.53	0.00	0.00	2.50	1.55	0.00	0.00	2.51
					1.55	0.00	0.00	3.03	4.84	0.00	0.00	4.56
					4.84	0.00	0.00	2.50	5.14	0.00	0.00	2.50
30x50	102	103	QFissi Solai(Sb.10)	PolG	-0.00	0.00	0.00	1.41	1.17	0.00	0.00	1.41
					1.17	0.00	0.00	1.76	5.14	0.00	0.00	2.81
30x50	102	103	QV Solai(Sb.10)	PolG	-0.00	0.00	0.00	3.20	1.17	0.00	0.00	3.20
					1.17	0.00	0.00	4.00	5.14	0.00	0.00	6.38
30x50	102	103	QV SolaiPsi0(Sb.10)	PolG	-0.00	0.00	0.00	2.24	1.17	0.00	0.00	2.24
					1.17	0.00	0.00	2.80	5.14	0.00	0.00	4.46
30x50	102	103	QV SolaiPsi1(Sb.10)	PolG	-0.00	0.00	0.00	2.24	1.17	0.00	0.00	2.24
					1.17	0.00	0.00	2.80	5.14	0.00	0.00	4.46
30x50	102	103	QV SolaiPsi2(Sb.10)	PolG	-0.00	0.00	0.00	1.92	1.17	0.00	0.00	1.92
					1.17	0.00	0.00	2.40	5.14	0.00	0.00	3.83
30x50	102	103	Neve	PolG	1.17	0.00	0.00	0.10	5.14	0.00	0.00	0.00

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	102	103	Neve	PolG	1.17	0.00	0.00	0.00	5.14	0.00	0.00	0.38
30x50	102	103	Neve(Sb.10)	PolG	0.00	0.00	0.00	0.38	5.14	0.00	0.00	0.38
30x50	102	103	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	103	104	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.63	0.00	0.00	3.75
30x50	103	104	QP Solai(Sb.11)	PolG	-0.00	0.00	0.00	2.50	0.31	0.00	0.00	2.50
					0.31	0.00	0.00	2.50	0.37	0.00	0.00	3.16
					0.37	0.00	0.00	3.89	4.34	0.00	0.00	5.08
					4.34	0.00	0.00	5.08	4.63	0.00	0.00	5.17
30x50	103	104	QFissi Solai(Sb.11)	PolG	-0.00	0.00	0.00	2.28	4.49	0.00	0.00	3.04
					4.49	0.00	0.00	3.04	4.63	0.00	0.00	3.06
30x50	103	104	QV Solai(Sb.11)	PolG	-0.00	0.00	0.00	5.18	4.49	0.00	0.00	6.91
					4.49	0.00	0.00	6.91	4.63	0.00	0.00	6.96
30x50	103	104	QV SolaiPsi0(Sb.11)	PolG	-0.00	0.00	0.00	3.62	4.49	0.00	0.00	4.83
					4.49	0.00	0.00	4.83	4.63	0.00	0.00	4.87
30x50	103	104	QV SolaiPsi1(Sb.11)	PolG	-0.00	0.00	0.00	3.62	4.49	0.00	0.00	4.83
					4.49	0.00	0.00	4.83	4.63	0.00	0.00	4.87
30x50	103	104	QV SolaiPsi2(Sb.11)	PolG	-0.00	0.00	0.00	3.11	4.49	0.00	0.00	4.14
					4.49	0.00	0.00	4.14	4.63	0.00	0.00	4.18
30x50	103	104	Neve	PolG	0.00	0.00	0.00	0.01	4.49	0.00	0.00	0.43
					4.49	0.00	0.00	0.43	4.63	0.00	0.00	0.44
30x50	103	104	Neve	PolG	0.00	0.00	0.00	0.23	4.63	0.00	0.00	0.01
30x50	103	104	Neve(Sb.11)	PolG	0.00	0.00	0.00	0.38	4.63	0.00	0.00	0.38
30x50	103	104	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	104	105	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.90	0.00	0.00	3.75
30x50	104	105	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.35	0.00	0.00	2.50
					0.35	0.00	0.00	3.95	3.60	0.00	0.00	4.97
					3.60	0.00	0.00	4.97	5.60	0.00	0.00	4.97
					5.60	0.00	0.00	2.50	5.90	0.00	0.00	2.50
30x50	104	105	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.60	3.54	0.00	0.00	3.42
					3.54	0.00	0.00	3.42	5.75	0.00	0.00	3.42
					5.75	0.00	0.00	1.41	5.90	0.00	0.00	1.41
30x50	104	105	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	4.65	3.54	0.00	0.00	5.65
					3.54	0.00	0.00	5.65	5.75	0.00	0.00	5.65
					5.75	0.00	0.00	3.20	5.90	0.00	0.00	3.20
30x50	104	105	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.25	3.54	0.00	0.00	3.96
					3.54	0.00	0.00	3.96	5.75	0.00	0.00	3.96
					5.75	0.00	0.00	2.24	5.90	0.00	0.00	2.24
30x50	104	105	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.25	3.54	0.00	0.00	3.96
					3.54	0.00	0.00	3.96	5.75	0.00	0.00	3.96
					5.75	0.00	0.00	2.24	5.90	0.00	0.00	2.24
30x50	104	105	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	2.79	3.54	0.00	0.00	3.39
					3.54	0.00	0.00	3.39	5.75	0.00	0.00	3.39
					5.75	0.00	0.00	1.92	5.90	0.00	0.00	1.92
30x50	104	105	Neve(Sb.12)	PolG	0.00	0.00	0.00	0.38	5.90	0.00	0.00	0.38
30x50	104	105	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	104	105	Tamponamento	PolG	0.00	0.00	0.00	7.80	5.90	0.00	0.00	7.80
30x50	105	106	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.97	0.00	0.00	3.75
30x50	105	106	QP Solai	PolG	0.00	0.00	0.00	3.50	3.97	0.00	0.00	3.50
30x50	105	106	QFissi Solai	PolG	0.00	0.00	0.00	2.26	3.97	0.00	0.00	2.26
30x50	105	106	QV Solai	PolG	0.00	0.00	0.00	4.24	3.97	0.00	0.00	4.24
30x50	105	106	QV SolaiPsi0	PolG	0.00	0.00	0.00	2.97	3.97	0.00	0.00	2.97
30x50	105	106	QV SolaiPsi1	PolG	0.00	0.00	0.00	2.97	3.97	0.00	0.00	2.97
30x50	105	106	QV SolaiPsi2	PolG	0.00	0.00	0.00	2.54	3.97	0.00	0.00	2.54
30x50	105	106	Neve(Sb.13)	PolG	0.00	0.00	0.00	0.38	3.97	0.00	0.00	0.38
30x50	105	106	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	105	106	Tamponamento	PolG	0.00	0.00	0.00	7.80	3.97	0.00	0.00	7.80
30x50	106	107	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.30	0.00	0.00	3.75
30x50	106	107	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	3.50	5.00	0.00	0.00	3.50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					5.00	0.00	0.00	2.50	5.30	0.00	0.00	2.50
30x50	106	107	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.02	5.15	0.00	0.00	2.02
					5.15	0.00	0.00	1.41	5.30	0.00	0.00	1.41
30x50	106	107	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	4.59	5.15	0.00	0.00	4.59
					5.15	0.00	0.00	3.20	5.30	0.00	0.00	3.20
30x50	106	107	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.21	5.15	0.00	0.00	3.21
					5.15	0.00	0.00	2.24	5.30	0.00	0.00	2.24
30x50	106	107	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.21	5.15	0.00	0.00	3.21
					5.15	0.00	0.00	2.24	5.30	0.00	0.00	2.24
30x50	106	107	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	2.75	5.15	0.00	0.00	2.75
					5.15	0.00	0.00	1.92	5.30	0.00	0.00	1.92
30x50	106	107	Neve	PolG	0.15	0.00	0.00	0.17	5.15	0.00	0.00	0.17
30x50	106	107	Neve(Sb.14)	PolG	0.00	0.00	0.00	0.38	5.30	0.00	0.00	0.38
30x50	106	107	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 108												
30x50	107	112	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.77	0.00	0.00	3.75
30x50	107	112	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	8.39	3.47	0.00	0.00	8.39
					3.47	0.00	0.00	2.50	3.77	0.00	0.00	2.50
30x50	107	112	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	4.93	3.62	0.00	0.00	4.93
					3.62	0.00	0.00	1.41	3.77	0.00	0.00	1.41
30x50	107	112	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	11.20	3.62	0.00	0.00	11.20
					3.62	0.00	0.00	3.20	3.77	0.00	0.00	3.20
30x50	107	112	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	7.84	3.62	0.00	0.00	7.84
					3.62	0.00	0.00	2.24	3.77	0.00	0.00	2.24
30x50	107	112	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	7.84	3.62	0.00	0.00	7.84
					3.62	0.00	0.00	2.24	3.77	0.00	0.00	2.24
30x50	107	112	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	6.72	3.62	0.00	0.00	6.72
					3.62	0.00	0.00	1.92	3.77	0.00	0.00	1.92
30x50	107	112	Neve(Sb.15)	PolG	0.00	0.00	0.00	0.38	3.77	0.00	0.00	0.38
30x50	107	112	Neve	PolG	0.15	0.00	0.00	0.96	3.62	0.00	0.00	0.96
30x50	107	112	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	112	120	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.70	0.00	0.00	3.75
30x50	112	120	QP Solai	PolG	0.00	0.00	0.00	8.39	4.10	0.00	0.00	8.39
					4.10	0.00	0.00	2.50	4.70	0.00	0.00	2.50
30x50	112	120	QFissi Solai	PolG	0.00	0.00	0.00	4.93	4.40	0.00	0.00	4.93
					4.40	0.00	0.00	1.41	4.70	0.00	0.00	1.41
30x50	112	120	QV Solai	PolG	0.00	0.00	0.00	11.20	4.40	0.00	0.00	11.20
					4.40	0.00	0.00	3.20	4.70	0.00	0.00	3.20
30x50	112	120	QV SolaiPsi0	PolG	0.00	0.00	0.00	7.84	4.40	0.00	0.00	7.84
					4.40	0.00	0.00	2.24	4.70	0.00	0.00	2.24
30x50	112	120	QV SolaiPsi1	PolG	0.00	0.00	0.00	7.84	4.40	0.00	0.00	7.84
					4.40	0.00	0.00	2.24	4.70	0.00	0.00	2.24
30x50	112	120	QV SolaiPsi2	PolG	0.00	0.00	0.00	6.72	4.40	0.00	0.00	6.72
					4.40	0.00	0.00	1.92	4.70	0.00	0.00	1.92
30x50	112	120	Neve	PolG	0.00	0.00	0.00	0.96	4.40	0.00	0.00	0.96
30x50	112	120	Neve(Sb.16)	PolG	0.00	0.00	0.00	0.38	4.70	0.00	0.00	0.38
30x50	112	120	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	120	128	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.13	0.00	0.00	3.75
30x50	120	128	QP Solai	PolG	0.00	0.00	0.00	8.01	3.83	0.00	0.00	8.01
					3.83	0.00	0.00	2.50	4.13	0.00	0.00	2.50
30x50	120	128	QFissi Solai	PolG	0.00	0.00	0.00	4.72	3.98	0.00	0.00	4.72
					3.98	0.00	0.00	1.41	4.13	0.00	0.00	1.41
30x50	120	128	QV Solai	PolG	0.00	0.00	0.00	10.72	3.98	0.00	0.00	10.72

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					3.98	0.00	0.00	3.20	4.13	0.00	0.00	3.20
30x50	120	128	QV SolaiPsi0	PolG	0.00	0.00	0.00	7.50	3.98	0.00	0.00	7.50
					3.98	0.00	0.00	2.24	4.13	0.00	0.00	2.24
30x50	120	128	QV SolaiPsi1	PolG	0.00	0.00	0.00	7.50	3.98	0.00	0.00	7.50
					3.98	0.00	0.00	2.24	4.13	0.00	0.00	2.24
30x50	120	128	QV SolaiPsi2	PolG	0.00	0.00	0.00	6.43	3.98	0.00	0.00	6.43
					3.98	0.00	0.00	1.92	4.13	0.00	0.00	1.92
30x50	120	128	Neve	PolG	0.00	0.00	0.00	0.90	3.98	0.00	0.00	0.90
30x50	120	128	Neve(Sb.17)	PolG	0.00	0.00	0.00	0.38	4.13	0.00	0.00	0.38
30x50	120	128	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 109												
30x50	106	111	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.77	0.00	0.00	3.75
30x50	106	111	QP Solai	PolG	0.30	0.00	0.00	10.85	3.47	0.00	0.00	10.86
30x50	106	111	QFissi Solai	PolG	0.15	0.00	0.00	7.72	3.62	0.00	0.00	7.72
30x50	106	111	QV Solai	PolG	0.15	0.00	0.00	13.12	3.62	0.00	0.00	13.12
30x50	106	111	QV SolaiPsi0	PolG	0.15	0.00	0.00	9.19	3.62	0.00	0.00	9.19
30x50	106	111	QV SolaiPsi1	PolG	0.15	0.00	0.00	9.19	3.62	0.00	0.00	9.19
30x50	106	111	QV SolaiPsi2	PolG	0.15	0.00	0.00	7.87	3.62	0.00	0.00	7.87
30x50	106	111	Neve	PolG	0.15	0.00	0.00	0.96	3.62	0.00	0.00	0.96
30x50	106	111	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	106	111	Tamponamento	PolG	0.00	0.00	0.00	7.80	3.77	0.00	0.00	7.80
30x50	111	119	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.70	0.00	0.00	3.75
30x50	111	119	QP Solai	PolG	0.00	0.00	0.00	10.85	4.10	0.00	0.00	10.85
					4.10	0.00	0.00	4.97	4.40	0.00	0.00	4.97
30x50	111	119	QFissi Solai	PolG	0.00	0.00	0.00	7.72	4.40	0.00	0.00	7.72
					4.40	0.00	0.00	4.20	4.55	0.00	0.00	4.20
30x50	111	119	QV Solai	PolG	0.00	0.00	0.00	13.12	4.40	0.00	0.00	13.12
					4.40	0.00	0.00	5.12	4.55	0.00	0.00	5.12
30x50	111	119	QV SolaiPsi0	PolG	0.00	0.00	0.00	9.19	4.40	0.00	0.00	9.19
					4.40	0.00	0.00	3.59	4.55	0.00	0.00	3.59
30x50	111	119	QV SolaiPsi1	PolG	0.00	0.00	0.00	9.19	4.40	0.00	0.00	9.19
					4.40	0.00	0.00	3.59	4.55	0.00	0.00	3.59
30x50	111	119	QV SolaiPsi2	PolG	0.00	0.00	0.00	7.87	4.40	0.00	0.00	7.87
					4.40	0.00	0.00	3.07	4.55	0.00	0.00	3.07
30x50	111	119	Neve	PolG	0.00	0.00	0.00	0.96	4.40	0.00	0.00	0.96
30x50	111	119	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	111	119	Tamponamento	PolG	0.00	0.00	0.00	7.80	4.70	0.00	0.00	7.80
Trave 110												
30x50	119	127	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.11	0.00	0.00	3.75
30x50	119	127	QP Solai	PolG	0.00	0.00	0.00	8.01	3.82	0.00	0.00	8.01
					3.82	0.00	0.00	2.50	4.14	0.00	0.00	2.50
30x50	119	127	QFissi Solai	PolG	0.00	0.00	0.00	4.72	3.97	0.00	0.00	4.72
					3.97	0.00	0.00	1.41	4.14	0.00	0.00	1.41
30x50	119	127	QV Solai	PolG	0.00	0.00	0.00	10.72	3.97	0.00	0.00	10.72
					3.97	0.00	0.00	3.20	4.14	0.00	0.00	3.20
30x50	119	127	QV SolaiPsi0	PolG	0.00	0.00	0.00	7.50	3.97	0.00	0.00	7.50
					3.97	0.00	0.00	2.24	4.14	0.00	0.00	2.24
30x50	119	127	QV SolaiPsi1	PolG	0.00	0.00	0.00	7.50	3.97	0.00	0.00	7.50
					3.97	0.00	0.00	2.24	4.14	0.00	0.00	2.24
30x50	119	127	QV SolaiPsi2	PolG	0.00	0.00	0.00	6.43	3.97	0.00	0.00	6.43
					3.97	0.00	0.00	1.92	4.14	0.00	0.00	1.92
30x50	119	127	Neve(Sb.19)	PolG	0.00	0.00	0.00	0.38	4.14	0.00	0.00	0.38
30x50	119	127	Neve	PolG	0.00	0.00	0.00	0.90	3.97	0.00	0.00	0.90
30x50	119	127	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 111												
30x50	102	115	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.82	0.00	0.00	3.75
30x50	102	115	QP Solai	PolG	0.00	0.00	0.00	3.13	2.14	0.00	0.00	5.84
					2.14	0.00	0.00	5.85	4.51	0.00	0.00	8.81
					4.51	0.00	0.00	2.50	4.82	0.00	0.00	2.50
30x50	102	115	QFissi Solai	PolG	0.00	0.00	0.00	2.02	2.03	0.00	0.00	3.47
					2.03	0.00	0.00	3.47	4.67	0.00	0.00	5.31
					4.67	0.00	0.00	1.41	4.82	0.00	0.00	1.41
30x50	102	115	QV Solai	PolG	0.00	0.00	0.00	4.59	2.03	0.00	0.00	7.88
					2.03	0.00	0.00	7.88	4.67	0.00	0.00	12.07

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					4.67	0.00	0.00	3.20	4.82	0.00	0.00	3.20
30x50	102	115	QV SolaiPsi0	PolG	0.00	0.00	0.00	3.21	2.03	0.00	0.00	5.51
					2.03	0.00	0.00	5.52	4.67	0.00	0.00	8.45
					4.67	0.00	0.00	2.24	4.82	0.00	0.00	2.24
30x50	102	115	QV SolaiPsi1	PolG	0.00	0.00	0.00	3.21	2.03	0.00	0.00	5.51
					2.03	0.00	0.00	5.52	4.67	0.00	0.00	8.45
					4.67	0.00	0.00	2.24	4.82	0.00	0.00	2.24
30x50	102	115	QV SolaiPsi2	PolG	0.00	0.00	0.00	2.75	2.03	0.00	0.00	4.73
					2.03	0.00	0.00	4.73	4.67	0.00	0.00	7.24
					4.67	0.00	0.00	1.92	4.82	0.00	0.00	1.92
30x50	102	115	Neve	PolG	0.00	0.00	0.00	0.17	2.03	0.00	0.00	0.56
					2.03	0.00	0.00	0.56	4.67	0.00	0.00	1.06
30x50	102	115	Neve(Sb.9)	PolG	0.00	0.00	0.00	0.38	4.82	0.00	0.00	0.38
30x50	102	115	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	115	121	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.31	0.00	0.00	3.75
30x50	115	121	QP Solai	PolG	0.00	0.00	0.00	4.13	4.01	0.00	0.00	4.12
					4.01	0.00	0.00	2.50	4.31	0.00	0.00	2.50
30x50	115	121	QFissi Solai	PolG	0.00	0.00	0.00	2.37	4.16	0.00	0.00	2.37
					4.16	0.00	0.00	1.41	4.31	0.00	0.00	1.41
30x50	115	121	QV Solai	PolG	0.00	0.00	0.00	5.39	4.16	0.00	0.00	5.38
					4.16	0.00	0.00	3.20	4.31	0.00	0.00	3.20
30x50	115	121	QV SolaiPsi0	PolG	0.00	0.00	0.00	3.78	4.16	0.00	0.00	3.77
					4.16	0.00	0.00	2.24	4.31	0.00	0.00	2.24
30x50	115	121	QV SolaiPsi1	PolG	0.00	0.00	0.00	3.78	4.16	0.00	0.00	3.77
					4.16	0.00	0.00	2.24	4.31	0.00	0.00	2.24
30x50	115	121	QV SolaiPsi2	PolG	0.00	0.00	0.00	3.24	4.16	0.00	0.00	3.23
					4.16	0.00	0.00	1.92	4.31	0.00	0.00	1.92
30x50	115	121	Neve(Sb.8)	PolG	0.00	0.00	0.00	0.38	4.31	0.00	0.00	0.38
30x50	115	121	Neve	PolG	0.00	0.00	0.00	0.26	4.16	0.00	0.00	0.26
30x50	115	121	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	121	124	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	2.88	0.00	0.00	3.75
30x50	121	124	QP Solai	PolG	0.00	0.00	0.00	4.11	2.88	0.00	0.00	4.11
30x50	121	124	QFissi Solai	PolG	0.00	0.00	0.00	2.37	2.88	0.00	0.00	2.37
30x50	121	124	QV Solai	PolG	0.00	0.00	0.00	5.38	2.88	0.00	0.00	5.38
30x50	121	124	QV SolaiPsi0	PolG	0.00	0.00	0.00	3.76	2.88	0.00	0.00	3.76
30x50	121	124	QV SolaiPsi1	PolG	0.00	0.00	0.00	3.76	2.88	0.00	0.00	3.76
30x50	121	124	QV SolaiPsi2	PolG	0.00	0.00	0.00	3.23	2.88	0.00	0.00	3.23
30x50	121	124	Neve	PolG	0.00	0.00	0.00	0.26	2.88	0.00	0.00	0.26
30x50	121	124	Neve(Sb.7)	PolG	0.00	0.00	0.00	0.38	2.88	0.00	0.00	0.38
30x50	121	124	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	124	129	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.40	0.00	0.00	3.75
30x50	124	129	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	4.11	4.10	0.00	0.00	4.11
					4.10	0.00	0.00	2.50	4.40	0.00	0.00	2.50
30x50	124	129	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.39	4.25	0.00	0.00	2.39
					4.25	0.00	0.00	1.41	4.40	0.00	0.00	1.41
30x50	124	129	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	5.44	4.25	0.00	0.00	5.44
					4.25	0.00	0.00	3.20	4.40	0.00	0.00	3.20
30x50	124	129	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.81	4.25	0.00	0.00	3.81
					4.25	0.00	0.00	2.24	4.40	0.00	0.00	2.24
30x50	124	129	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.81	4.25	0.00	0.00	3.81
					4.25	0.00	0.00	2.24	4.40	0.00	0.00	2.24
30x50	124	129	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	3.26	4.25	0.00	0.00	3.26
					4.25	0.00	0.00	1.92	4.40	0.00	0.00	1.92
30x50	124	129	Neve(Sb.6)	PolG	0.00	0.00	0.00	0.38	4.40	0.00	0.00	0.38
30x50	124	129	Neve	PolG	0.15	0.00	0.00	0.27	4.25	0.00	0.00	0.27
30x50	124	129	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 112												
30x50	113	122	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.61	0.00	0.00	3.75

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	113	122	QP Solai	PolG	0.29	0.00	0.00	1.62	0.44	0.00	0.00	1.62
					0.44	0.00	0.00	1.65	2.28	0.00	0.00	4.00
					2.28	0.00	0.00	4.00	4.30	0.00	0.00	6.56
					4.30	0.00	0.00	4.90	4.58	0.00	0.00	5.26
30x50	113	122	QFissi Solai	PolG	0.08	0.00	0.00	0.02	0.14	0.00	0.00	0.08
					0.14	0.00	0.00	1.04	2.18	0.00	0.00	3.08
					2.18	0.00	0.00	3.08	4.45	0.00	0.00	5.34
					4.45	0.00	0.00	4.35	4.58	0.00	0.00	4.49
30x50	113	122	QV Solai	PolG	0.08	0.00	0.00	0.02	0.14	0.00	0.00	0.09
					0.14	0.00	0.00	2.29	2.18	0.00	0.00	4.78
					2.18	0.00	0.00	4.78	4.45	0.00	0.00	7.56
					4.45	0.00	0.00	5.31	4.58	0.00	0.00	5.47
30x50	113	122	QV SolaiPsi0	PolG	0.08	0.00	0.00	0.02	0.14	0.00	0.00	0.07
					0.14	0.00	0.00	1.60	2.18	0.00	0.00	3.35
					2.18	0.00	0.00	3.35	4.45	0.00	0.00	5.29
					4.45	0.00	0.00	3.72	4.58	0.00	0.00	3.83
30x50	113	122	QV SolaiPsi1	PolG	0.08	0.00	0.00	0.02	0.14	0.00	0.00	0.07
					0.14	0.00	0.00	1.60	2.18	0.00	0.00	3.35
					2.18	0.00	0.00	3.35	4.45	0.00	0.00	5.29
					4.45	0.00	0.00	3.72	4.58	0.00	0.00	3.83
30x50	113	122	QV SolaiPsi2	PolG	0.08	0.00	0.00	0.01	0.14	0.00	0.00	0.06
					0.14	0.00	0.00	1.37	2.18	0.00	0.00	2.87
					2.18	0.00	0.00	2.87	4.45	0.00	0.00	4.53
					4.45	0.00	0.00	3.19	4.58	0.00	0.00	3.28
30x50	113	122	Neve	PolG	0.14	0.00	0.00	0.00	4.45	0.00	0.00	0.01
30x50	113	122	Neve	PolG	0.14	0.00	0.00	0.26	4.45	0.00	0.00	0.26
30x50	113	122	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	113	122	Tamponamento	PolG	0.08	0.00	0.00	7.80	4.69	0.00	0.00	7.80
30x50	122	125	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	2.88	0.00	0.00	3.75
30x50	122	125	QP Solai	PolG	0.00	0.00	0.00	5.29	0.02	0.00	0.00	5.31
					0.02	0.00	0.00	6.92	1.25	0.00	0.00	8.43
					1.25	0.00	0.00	8.43	2.88	0.00	0.00	8.43
30x50	122	125	QFissi Solai	PolG	0.00	0.00	0.00	5.44	1.19	0.00	0.00	6.61
					1.19	0.00	0.00	6.61	2.88	0.00	0.00	6.61
30x50	122	125	QV Solai	PolG	0.00	0.00	0.00	7.64	1.19	0.00	0.00	9.07
					1.19	0.00	0.00	9.07	2.88	0.00	0.00	9.07
30x50	122	125	QV SolaiPsi0	PolG	0.00	0.00	0.00	5.35	1.19	0.00	0.00	6.35
					1.19	0.00	0.00	6.35	2.88	0.00	0.00	6.35
30x50	122	125	QV SolaiPsi1	PolG	0.00	0.00	0.00	5.35	1.19	0.00	0.00	6.35
					1.19	0.00	0.00	6.35	2.88	0.00	0.00	6.35
30x50	122	125	QV SolaiPsi2	PolG	0.00	0.00	0.00	4.59	1.19	0.00	0.00	5.44
					1.19	0.00	0.00	5.44	2.88	0.00	0.00	5.44
30x50	122	125	Neve	PolG	0.00	0.00	0.00	0.26	2.88	0.00	0.00	0.26
30x50	122	125	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	122	125	Tamponamento	PolG	-0.00	0.00	0.00	7.80	2.88	0.00	0.00	7.80
60x25	125	130	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.40	0.00	0.00	3.75
60x25	125	130	QP Solai	PolG	0.29	0.00	0.00	1.61	0.59	0.00	0.00	1.61
					0.59	0.00	0.00	3.22	4.09	0.00	0.00	3.22
60x25	125	130	QFissi Solai	PolG	0.14	0.00	0.00	0.98	0.44	0.00	0.00	0.98
					0.44	0.00	0.00	1.97	4.24	0.00	0.00	1.97
60x25	125	130	QV Solai	PolG	0.14	0.00	0.00	2.24	0.44	0.00	0.00	2.24
					0.44	0.00	0.00	4.48	4.24	0.00	0.00	4.48
60x25	125	130	QV SolaiPsi0	PolG	0.14	0.00	0.00	1.57	0.44	0.00	0.00	1.57
					0.44	0.00	0.00	3.13	4.24	0.00	0.00	3.13
60x25	125	130	QV SolaiPsi1	PolG	0.14	0.00	0.00	1.57	0.44	0.00	0.00	1.57
					0.44	0.00	0.00	3.13	4.24	0.00	0.00	3.13
60x25	125	130	QV SolaiPsi2	PolG	0.14	0.00	0.00	1.34	0.44	0.00	0.00	1.34
					0.44	0.00	0.00	2.69	4.24	0.00	0.00	2.69
60x25	125	130	Neve	PolG	0.14	0.00	0.00	0.27	4.24	0.00	0.00	0.27
60x25	125	130	Neve	PolG	0.44	0.00	0.00	0.27	4.24	0.00	0.00	0.27
60x25	125	130	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 113												
30x50	123	126	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	1.66	0.00	0.00	3.75
30x50	123	126	QP Solai	PolG	0.00	0.00	0.00	9.32	1.43	0.00	0.00	9.32

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					1.43	0.00	0.00	6.82	1.66	0.00	0.00	6.82
30x50	123	126	QFissi Solai	PolG	0.00	0.00	0.00	7.06	1.43	0.00	0.00	7.06
					1.43	0.00	0.00	5.65	1.66	0.00	0.00	5.65
30x50	123	126	QV Solai	PolG	0.00	0.00	0.00	10.09	1.43	0.00	0.00	10.09
					1.43	0.00	0.00	6.89	1.66	0.00	0.00	6.89
30x50	123	126	QV SolaiPsi0	PolG	0.00	0.00	0.00	7.06	1.43	0.00	0.00	7.07
					1.43	0.00	0.00	4.83	1.66	0.00	0.00	4.83
30x50	123	126	QV SolaiPsi1	PolG	0.00	0.00	0.00	7.06	1.43	0.00	0.00	7.07
					1.43	0.00	0.00	4.83	1.66	0.00	0.00	4.83
30x50	123	126	QV SolaiPsi2	PolG	0.00	0.00	0.00	6.06	1.43	0.00	0.00	6.06
					1.43	0.00	0.00	4.14	1.66	0.00	0.00	4.14
30x50	123	126	Neve(Sb.22)	PolG	0.00	0.00	0.00	0.38	1.43	0.00	0.00	0.38
30x50	123	126	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	123	126	Tamponamento	PolG	0.00	0.00	0.00	7.80	1.43	0.00	0.00	7.80
30x50	126	131	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.40	0.00	0.00	3.75
30x50	126	131	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.60	0.00	0.00	2.50
					0.60	0.00	0.00	4.11	4.10	0.00	0.00	4.11
					4.10	0.00	0.00	2.50	4.40	0.00	0.00	2.50
30x50	126	131	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.45	0.00	0.00	1.41
					0.45	0.00	0.00	2.39	4.25	0.00	0.00	2.39
					4.25	0.00	0.00	1.41	4.40	0.00	0.00	1.41
30x50	126	131	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.45	0.00	0.00	3.20
					0.45	0.00	0.00	5.44	4.25	0.00	0.00	5.44
					4.25	0.00	0.00	3.20	4.40	0.00	0.00	3.20
30x50	126	131	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.45	0.00	0.00	2.24
					0.45	0.00	0.00	3.81	4.25	0.00	0.00	3.81
					4.25	0.00	0.00	2.24	4.40	0.00	0.00	2.24
30x50	126	131	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.45	0.00	0.00	2.24
					0.45	0.00	0.00	3.81	4.25	0.00	0.00	3.81
					4.25	0.00	0.00	2.24	4.40	0.00	0.00	2.24
30x50	126	131	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.45	0.00	0.00	1.92
					0.45	0.00	0.00	3.26	4.25	0.00	0.00	3.26
					4.25	0.00	0.00	1.92	4.40	0.00	0.00	1.92
30x50	126	131	Neve(Sb.23)	PolG	0.00	0.00	0.00	0.38	4.40	0.00	0.00	0.38
30x50	126	131	Neve	PolG	0.45	0.00	0.00	0.27	4.25	0.00	0.00	0.27
30x50	126	131	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 114												
30x50	116	114	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.10	0.00	0.00	3.75
30x50	116	114	QP Solai	PolG	0.30	0.00	0.00	0.84	2.80	0.00	0.00	0.84
30x50	116	114	QFissi Solai	PolG	0.15	0.00	0.00	0.77	2.95	0.00	0.00	0.77
30x50	116	114	QV Solai	PolG	0.15	0.00	0.00	0.94	2.95	0.00	0.00	0.94
30x50	116	114	QV SolaiPsi0	PolG	0.15	0.00	0.00	0.66	2.95	0.00	0.00	0.66
30x50	116	114	QV SolaiPsi1	PolG	0.15	0.00	0.00	0.66	2.95	0.00	0.00	0.66
30x50	116	114	QV SolaiPsi2	PolG	0.15	0.00	0.00	0.57	2.95	0.00	0.00	0.57
30x50	116	114	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 115												
60x25	113	109	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.11	0.00	0.00	3.75
60x25	113	109	QP Solai	PolG	0.31	0.00	0.00	1.78	2.76	0.00	0.00	1.78
					2.76	0.00	0.00	1.78	2.81	0.00	0.00	0.84
60x25	113	109	QFissi Solai	PolG	0.15	0.00	0.00	1.38	2.91	0.00	0.00	1.38
					2.91	0.00	0.00	1.38	2.96	0.00	0.00	0.77
60x25	113	109	QV Solai	PolG	0.15	0.00	0.00	2.32	2.91	0.00	0.00	2.32
					2.91	0.00	0.00	2.32	2.96	0.00	0.00	0.94
60x25	113	109	QV SolaiPsi0	PolG	0.15	0.00	0.00	1.62	2.91	0.00	0.00	1.62
					2.91	0.00	0.00	1.62	2.96	0.00	0.00	0.66
60x25	113	109	QV SolaiPsi1	PolG	0.15	0.00	0.00	1.62	2.91	0.00	0.00	1.62
					2.91	0.00	0.00	1.62	2.96	0.00	0.00	0.66
60x25	113	109	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.39	2.91	0.00	0.00	1.39
					2.91	0.00	0.00	1.39	2.96	0.00	0.00	0.57
60x25	113	109	Neve	PolG	0.15	0.00	0.00	0.16	2.91	0.00	0.00	0.16
					2.91	0.00	0.00	0.16	2.96	0.00	0.00	0.00
60x25	113	109	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
60x25	113	109	Tamponamento	PolG	-0.00	0.00	0.00	7.80	3.11	0.00	0.00	7.80
Trave 116												

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	108	103	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.05	0.00	0.00	3.75
30x50	108	103	QP Solai	PolG	0.30	0.00	0.00	1.66	2.63	0.00	0.00	0.93
					2.63	0.00	0.00	0.93	2.75	0.00	0.00	0.93
30x50	108	103	QFissi Solai	PolG	0.15	0.00	0.00	1.10	2.90	0.00	0.00	0.62
					2.90	0.00	0.00	0.02	2.99	0.00	0.00	0.00
30x50	108	103	QV Solai	PolG	0.15	0.00	0.00	2.51	2.90	0.00	0.00	1.41
					2.90	0.00	0.00	0.03	2.99	0.00	0.00	0.00
30x50	108	103	QV SolaiPsi0	PolG	0.15	0.00	0.00	1.75	2.90	0.00	0.00	0.98
					2.90	0.00	0.00	0.02	2.99	0.00	0.00	0.00
30x50	108	103	QV SolaiPsi1	PolG	0.15	0.00	0.00	1.75	2.90	0.00	0.00	0.98
					2.90	0.00	0.00	0.02	2.99	0.00	0.00	0.00
30x50	108	103	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.50	2.90	0.00	0.00	0.84
					2.90	0.00	0.00	0.02	2.99	0.00	0.00	0.00
30x50	108	103	Neve	PolG	0.15	0.00	0.00	0.16	2.90	0.00	0.00	0.16
30x50	108	103	Neve	PolG	0.15	0.00	0.00	0.14	2.99	0.00	0.00	0.00
30x50	108	103	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 117												
30x50	117	118	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	2.01	0.00	0.00	3.75
30x50	117	118	QP Solai	PolG	0.00	0.00	0.00	4.97	1.79	0.00	0.00	4.97
					1.79	0.00	0.00	2.46	2.01	0.00	0.00	2.46
30x50	117	118	QFissi Solai	PolG	0.00	0.00	0.00	3.42	1.79	0.00	0.00	3.42
					1.79	0.00	0.00	2.01	2.01	0.00	0.00	2.01
30x50	117	118	QV Solai	PolG	0.00	0.00	0.00	5.65	1.79	0.00	0.00	5.65
					1.79	0.00	0.00	2.45	2.01	0.00	0.00	2.45
30x50	117	118	QV SolaiPsi0	PolG	0.00	0.00	0.00	3.96	1.79	0.00	0.00	3.96
					1.79	0.00	0.00	1.72	2.01	0.00	0.00	1.72
30x50	117	118	QV SolaiPsi1	PolG	0.00	0.00	0.00	3.96	1.79	0.00	0.00	3.96
					1.79	0.00	0.00	1.72	2.01	0.00	0.00	1.72
30x50	117	118	QV SolaiPsi2	PolG	0.00	0.00	0.00	3.39	1.79	0.00	0.00	3.39
					1.79	0.00	0.00	1.47	2.01	0.00	0.00	1.47
30x50	117	118	Neve(Sb.21)	PolG	0.00	0.00	0.00	0.38	1.79	0.00	0.00	0.38
30x50	117	118	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	117	118	Tamponamento	PolG	0.00	0.00	0.00	7.80	1.79	0.00	0.00	7.80
30x50	118	119	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.27	0.00	0.00	3.75
30x50	118	119	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	3.88	4.27	0.00	0.00	3.88
30x50	118	119	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.56	4.27	0.00	0.00	2.56
30x50	118	119	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	4.61	4.27	0.00	0.00	4.61
30x50	118	119	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.23	4.27	0.00	0.00	3.23
30x50	118	119	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.23	4.27	0.00	0.00	3.23
30x50	118	119	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	2.77	4.27	0.00	0.00	2.77
30x50	118	119	Neve(Sb.20)	PolG	0.00	0.00	0.00	0.38	4.27	0.00	0.00	0.38
30x50	118	119	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	118	119	Tamponamento	PolG	0.00	0.00	0.00	7.80	4.27	0.00	0.00	7.80
60x25	119	120	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.30	0.00	0.00	3.75
60x25	119	120	QP Solai	PolG	0.30	0.00	0.00	1.28	0.60	0.00	0.00	1.28
					0.60	0.00	0.00	2.48	5.00	0.00	0.00	2.48
60x25	119	120	QFissi Solai	PolG	0.15	0.00	0.00	0.80	0.45	0.00	0.00	0.80
					0.45	0.00	0.00	1.55	5.15	0.00	0.00	1.55
60x25	119	120	QV Solai	PolG	0.15	0.00	0.00	1.82	0.45	0.00	0.00	1.82
					0.45	0.00	0.00	3.53	5.15	0.00	0.00	3.53
60x25	119	120	QV SolaiPsi0	PolG	0.15	0.00	0.00	1.27	0.45	0.00	0.00	1.27
					0.45	0.00	0.00	2.47	5.15	0.00	0.00	2.47
60x25	119	120	QV SolaiPsi1	PolG	0.15	0.00	0.00	1.27	0.45	0.00	0.00	1.27
					0.45	0.00	0.00	2.47	5.15	0.00	0.00	2.47
60x25	119	120	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.09	0.45	0.00	0.00	1.09
					0.45	0.00	0.00	2.12	5.15	0.00	0.00	2.12
60x25	119	120	Neve	PolG	0.45	0.00	0.00	0.21	5.15	0.00	0.00	0.21
60x25	119	120	Neve	PolG	0.15	0.00	0.00	0.22	5.15	0.00	0.00	0.22

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
60x25	119	120	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 118												
30x50	127	128	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.00	0.00	0.00	3.75
30x50	127	128	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	3.70	4.70	0.00	0.00	3.70
					4.70	0.00	0.00	2.50	5.00	0.00	0.00	2.50
30x50	127	128	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.16	4.85	0.00	0.00	2.16
					4.85	0.00	0.00	1.41	5.00	0.00	0.00	1.41
30x50	127	128	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	4.91	4.85	0.00	0.00	4.91
					4.85	0.00	0.00	3.20	5.00	0.00	0.00	3.20
30x50	127	128	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.44	4.85	0.00	0.00	3.44
					4.85	0.00	0.00	2.24	5.00	0.00	0.00	2.24
30x50	127	128	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.44	4.85	0.00	0.00	3.44
					4.85	0.00	0.00	2.24	5.00	0.00	0.00	2.24
30x50	127	128	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	2.95	4.85	0.00	0.00	2.95
					4.85	0.00	0.00	1.92	5.00	0.00	0.00	1.92
30x50	127	128	Neve(Sb.18)	PolG	0.00	0.00	0.00	0.38	5.00	0.00	0.00	0.38
30x50	127	128	Neve	PolG	0.15	0.00	0.00	0.21	4.85	0.00	0.00	0.21
30x50	127	128	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 119												
30x50	110	111	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.27	0.00	0.00	3.75
30x50	110	111	QP Solai	PolG	0.30	0.00	0.00	2.37	4.27	0.00	0.00	2.37
30x50	110	111	QFissi Solai	PolG	0.15	0.00	0.00	2.01	4.27	0.00	0.00	2.01
30x50	110	111	QV Solai	PolG	0.15	0.00	0.00	2.45	4.27	0.00	0.00	2.45
30x50	110	111	QV SolaiPsi0	PolG	0.15	0.00	0.00	1.72	4.27	0.00	0.00	1.72
30x50	110	111	QV SolaiPsi1	PolG	0.15	0.00	0.00	1.72	4.27	0.00	0.00	1.72
30x50	110	111	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.47	4.27	0.00	0.00	1.47
30x50	110	111	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	111	112	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.30	0.00	0.00	3.75
30x50	111	112	QP Solai	PolG	0.30	0.00	0.00	2.28	5.00	0.00	0.00	2.28
30x50	111	112	QFissi Solai	PolG	0.15	0.00	0.00	1.41	5.15	0.00	0.00	1.41
30x50	111	112	QV Solai	PolG	0.15	0.00	0.00	3.21	5.15	0.00	0.00	3.21
30x50	111	112	QV SolaiPsi0	PolG	0.15	0.00	0.00	2.25	5.15	0.00	0.00	2.25
30x50	111	112	QV SolaiPsi1	PolG	0.15	0.00	0.00	2.25	5.15	0.00	0.00	2.25
30x50	111	112	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.92	5.15	0.00	0.00	1.92
30x50	111	112	Neve	PolG	0.15	0.00	0.00	0.17	5.15	0.00	0.00	0.17
30x50	111	112	Neve	PolG	0.15	0.00	0.00	0.22	5.15	0.00	0.00	0.22
30x50	111	112	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 120												
30x50	105	110	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.79	0.00	0.00	3.75
30x50	105	110	QP Solai	PolG	0.31	0.00	0.00	11.61	3.48	0.00	0.00	11.57
					3.48	0.00	0.00	6.60	3.78	0.00	0.00	6.59
30x50	105	110	QFissi Solai	PolG	0.16	0.00	0.00	9.71	3.63	0.00	0.00	9.68
					3.63	0.00	0.00	5.48	3.78	0.00	0.00	5.48
30x50	105	110	QV Solai	PolG	0.16	0.00	0.00	11.85	3.63	0.00	0.00	11.80
					3.63	0.00	0.00	6.68	3.78	0.00	0.00	6.68
30x50	105	110	QV SolaiPsi0	PolG	0.16	0.00	0.00	8.29	3.63	0.00	0.00	8.26
					3.63	0.00	0.00	4.68	3.78	0.00	0.00	4.67
30x50	105	110	QV SolaiPsi1	PolG	0.16	0.00	0.00	8.29	3.63	0.00	0.00	8.26
					3.63	0.00	0.00	4.68	3.78	0.00	0.00	4.67
30x50	105	110	QV SolaiPsi2	PolG	0.16	0.00	0.00	7.11	3.63	0.00	0.00	7.08
					3.63	0.00	0.00	4.01	3.78	0.00	0.00	4.01
30x50	105	110	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	110	118	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.70	0.00	0.00	3.75
30x50	110	118	QP Solai	PolG	0.00	0.00	0.00	11.56	1.14	0.00	0.00	11.55
					1.14	0.00	0.00	11.55	4.40	0.00	0.00	7.47
30x50	110	118	QFissi Solai	PolG	0.00	0.00	0.00	9.68	1.21	0.00	0.00	9.67
					1.21	0.00	0.00	9.67	4.55	0.00	0.00	6.38
30x50	110	118	QV Solai	PolG	0.00	0.00	0.00	11.80	1.21	0.00	0.00	11.79

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					1.21	0.00	0.00	11.79	4.55	0.00	0.00	7.78
30x50	110	118	QV SolaiPsi0	PolG	0.00	0.00	0.00	8.26	1.21	0.00	0.00	8.25
					1.21	0.00	0.00	8.25	4.55	0.00	0.00	5.45
30x50	110	118	QV SolaiPsi1	PolG	0.00	0.00	0.00	8.26	1.21	0.00	0.00	8.25
					1.21	0.00	0.00	8.25	4.55	0.00	0.00	5.45
30x50	110	118	QV SolaiPsi2	PolG	0.00	0.00	0.00	7.08	1.21	0.00	0.00	7.07
					1.21	0.00	0.00	7.07	4.55	0.00	0.00	4.67
30x50	110	118	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 121												
30x50	104	114	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.04	0.00	0.00	3.75
30x50	104	114	QP Solai	PolG	0.30	0.00	0.00	9.33	3.77	0.00	0.00	8.20
					3.77	0.00	0.00	8.20	4.61	0.00	0.00	7.93
					4.61	0.00	0.00	6.60	4.92	0.00	0.00	6.59
30x50	104	114	QFissi Solai	PolG	0.15	0.00	0.00	7.21	3.77	0.00	0.00	6.54
					3.77	0.00	0.00	6.54	4.98	0.00	0.00	6.32
30x50	104	114	QV Solai	PolG	0.15	0.00	0.00	10.58	3.77	0.00	0.00	9.09
					3.77	0.00	0.00	9.09	4.98	0.00	0.00	8.59
30x50	104	114	QV SolaiPsi0	PolG	0.15	0.00	0.00	7.41	3.77	0.00	0.00	6.36
					3.77	0.00	0.00	6.36	4.98	0.00	0.00	6.01
30x50	104	114	QV SolaiPsi1	PolG	0.15	0.00	0.00	7.41	3.77	0.00	0.00	6.36
					3.77	0.00	0.00	6.36	4.98	0.00	0.00	6.01
30x50	104	114	QV SolaiPsi2	PolG	0.15	0.00	0.00	6.35	3.77	0.00	0.00	5.45
					3.77	0.00	0.00	5.45	4.98	0.00	0.00	5.15
30x50	104	114	Neve	PolG	0.15	0.00	0.00	0.46	4.98	0.00	0.00	0.00
30x50	104	114	Neve	PolG	0.15	0.00	0.00	0.00	4.98	0.00	0.00	0.23
30x50	104	114	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 122												
30x50	36	35	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.10	0.00	0.00	3.75
30x50	36	35	QP Solai(Sb.5)	PolG	-0.00	0.00	0.00	2.60	3.10	0.00	0.00	2.60
30x50	36	35	QFissi Solai(Sb.5)	PolG	-0.00	0.00	0.00	4.50	3.10	0.00	0.00	4.50
30x50	36	35	QV Solai(Sb.5)	PolG	-0.00	0.00	0.00	6.92	3.10	0.00	0.00	6.92
30x50	36	35	QV SolaiPsi0(Sb.5)	PolG	-0.00	0.00	0.00	4.84	3.10	0.00	0.00	4.84
30x50	36	35	QV SolaiPsi1(Sb.5)	PolG	-0.00	0.00	0.00	4.84	3.10	0.00	0.00	4.84
30x50	36	35	QV SolaiPsi2(Sb.5)	PolG	-0.00	0.00	0.00	4.15	3.10	0.00	0.00	4.15
30x50	36	35	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	36	35	Tamponamento	PolG	0.00	0.00	0.00	7.20	3.10	0.00	0.00	7.20
Trave 123												
30x50	36	39	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	1.43	0.00	0.00	3.75
30x50	36	39	QP Solai(Sb.3)	PolG	-0.00	0.00	0.00	2.25	1.73	0.00	0.00	2.25
30x50	36	39	QFissi Solai(Sb.3)	PolG	-0.00	0.00	0.00	3.90	1.73	0.00	0.00	3.90
30x50	36	39	QV Solai(Sb.3)	PolG	-0.00	0.00	0.00	6.00	1.73	0.00	0.00	6.00
30x50	36	39	QV SolaiPsi0(Sb.3)	PolG	-0.00	0.00	0.00	4.20	1.73	0.00	0.00	4.20
30x50	36	39	QV SolaiPsi1(Sb.3)	PolG	-0.00	0.00	0.00	4.20	1.73	0.00	0.00	4.20
30x50	36	39	QV SolaiPsi2(Sb.3)	PolG	-0.00	0.00	0.00	3.60	1.73	0.00	0.00	3.60
30x50	36	39	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	39	116	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.45	0.00	0.00	3.75
30x50	39	116	QP Solai(Sb.4)	PolG	-0.00	-0.00	-0.00	2.25	3.99	-0.00	-0.00	2.25
30x50	39	116	QFissi Solai(Sb.4)	PolG	-0.00	-0.00	-0.00	3.90	3.99	-0.00	-0.00	3.90
30x50	39	116	QV Solai(Sb.4)	PolG	-0.00	-0.00	-0.00	6.00	3.99	-0.00	-0.00	6.00
30x50	39	116	QV SolaiPsi0(Sb.4)	PolG	-0.00	-0.00	-0.00	4.20	3.99	-0.00	-0.00	4.20
30x50	39	116	QV SolaiPsi1(Sb.4)	PolG	-0.00	-0.00	-0.00	4.20	3.99	-0.00	-0.00	4.20
30x50	39	116	QV SolaiPsi2(Sb.4)	PolG	-0.00	-0.00	-0.00	3.60	3.99	-0.00	-0.00	3.60
30x50	39	116	Neve(Sb.4)	PolG	0.00	-0.00	-0.00	0.72	3.99	-0.00	-0.00	0.72
30x50	39	116	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 201												
30x50	225	226	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	6.04	0.00	0.00	3.75
30x50	225	226	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.34	0.00	0.00	2.50
					0.34	0.00	0.00	4.80	2.19	0.00	0.00	4.22
					2.19	0.00	0.00	4.22	5.74	0.00	0.00	3.11
					5.74	0.00	0.00	2.50	6.04	0.00	0.00	2.50
30x50	225	226	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	1.99	0.30	0.00	0.00	1.99
					0.30	0.00	0.00	2.77	2.30	0.00	0.00	2.42
					2.30	0.00	0.00	2.42	5.90	0.00	0.00	1.79

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					5.90	0.00	0.00	1.41	6.04	0.00	0.00	1.41
30x50	225	226	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	4.53	0.30	0.00	0.00	4.53
					0.30	0.00	0.00	6.30	2.30	0.00	0.00	5.50
					2.30	0.00	0.00	5.50	5.90	0.00	0.00	4.06
					5.90	0.00	0.00	3.20	6.04	0.00	0.00	3.20
30x50	225	226	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.17	0.30	0.00	0.00	3.17
					0.30	0.00	0.00	4.41	2.30	0.00	0.00	3.85
					2.30	0.00	0.00	3.85	5.90	0.00	0.00	2.84
					5.90	0.00	0.00	2.24	6.04	0.00	0.00	2.24
30x50	225	226	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.17	0.30	0.00	0.00	3.17
					0.30	0.00	0.00	4.41	2.30	0.00	0.00	3.85
					2.30	0.00	0.00	3.85	5.90	0.00	0.00	2.84
					5.90	0.00	0.00	2.24	6.04	0.00	0.00	2.24
30x50	225	226	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	2.72	0.30	0.00	0.00	2.72
					0.30	0.00	0.00	3.78	2.30	0.00	0.00	3.30
					2.30	0.00	0.00	3.30	5.90	0.00	0.00	2.44
					5.90	0.00	0.00	1.92	6.04	0.00	0.00	1.92
30x50	225	226	Neve(Sb.33)	PolG	0.00	0.00	0.00	0.38	6.04	0.00	0.00	0.38
30x50	225	226	Neve	PolG	0.15	0.00	0.00	0.16	0.30	0.00	0.00	0.16
					0.30	0.00	0.00	0.37	2.30	0.00	0.00	0.28
					2.30	0.00	0.00	0.28	5.90	0.00	0.00	0.10
30x50	225	226	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	225	226	Tamponamento	PolG	0.00	0.00	0.00	2.40	6.04	0.00	0.00	2.40
Trave 202												
30x50	213	216	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.30	0.00	0.00	3.75
30x50	213	216	QP Solai	PolG	0.30	0.00	0.00	3.14	0.69	0.00	0.00	3.14
					0.69	0.00	0.00	4.76	3.30	0.00	0.00	6.00
30x50	213	216	QFissi Solai	PolG	0.15	0.00	0.00	1.97	0.33	0.00	0.00	1.97
					0.33	0.00	0.00	2.49	0.48	0.00	0.00	2.58
					0.48	0.00	0.00	2.99	3.30	0.00	0.00	3.74
30x50	213	216	QV Solai	PolG	0.15	0.00	0.00	4.49	0.33	0.00	0.00	4.49
					0.33	0.00	0.00	5.65	0.48	0.00	0.00	5.86
					0.48	0.00	0.00	6.80	3.30	0.00	0.00	8.51
30x50	213	216	QV SolaiPsi0	PolG	0.15	0.00	0.00	3.14	0.33	0.00	0.00	3.14
					0.33	0.00	0.00	3.96	0.48	0.00	0.00	4.10
					0.48	0.00	0.00	4.76	3.30	0.00	0.00	5.96
30x50	213	216	QV SolaiPsi1	PolG	0.15	0.00	0.00	3.14	0.33	0.00	0.00	3.14
					0.33	0.00	0.00	3.96	0.48	0.00	0.00	4.10
					0.48	0.00	0.00	4.76	3.30	0.00	0.00	5.96
30x50	213	216	QV SolaiPsi2	PolG	0.15	0.00	0.00	2.69	0.33	0.00	0.00	2.69
					0.33	0.00	0.00	3.39	0.48	0.00	0.00	3.52
					0.48	0.00	0.00	4.08	3.30	0.00	0.00	5.11
30x50	213	216	Neve	PolG	0.15	0.00	0.00	0.00	3.30	0.00	0.00	0.00
30x50	213	216	Neve	PolG	0.33	0.00	0.00	0.14	0.48	0.00	0.00	0.15
					0.48	0.00	0.00	0.26	3.30	0.00	0.00	0.20
30x50	213	216	Neve	PolG	0.33	0.00	0.00	0.00	3.30	0.00	0.00	0.29
30x50	213	216	Neve	PolG	0.15	0.00	0.00	0.54	3.30	0.00	0.00	0.54
30x50	213	216	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	216	223	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.33	0.00	0.00	3.75
30x50	216	223	QP Solai	PolG	0.00	0.00	0.00	2.87	0.60	0.00	0.00	3.16
					0.60	0.00	0.00	6.29	2.45	0.00	0.00	7.16
					2.45	0.00	0.00	7.16	2.50	0.00	0.00	7.19
					2.50	0.00	0.00	7.19	4.10	0.00	0.00	7.95
					4.10	0.00	0.00	7.95	5.03	0.00	0.00	8.38
30x50	216	223	QFissi Solai	PolG	0.00	0.00	0.00	1.77	0.30	0.00	0.00	1.85
					0.30	0.00	0.00	3.82	2.60	0.00	0.00	4.44
					2.60	0.00	0.00	4.44	3.42	0.00	0.00	4.59
					3.42	0.00	0.00	2.39	3.45	0.00	0.00	2.38
					3.45	0.00	0.00	4.67	5.09	0.00	0.00	5.10
					5.09	0.00	0.00	1.97	5.18	0.00	0.00	1.97

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	216	223	QV Solai	PolG	0.00	0.00	0.00	4.03	0.30	0.00	0.00	4.21
					0.30	0.00	0.00	8.69	2.60	0.00	0.00	10.09
					2.60	0.00	0.00	10.10	3.42	0.00	0.00	10.42
					3.42	0.00	0.00	5.42	3.45	0.00	0.00	5.42
					3.45	0.00	0.00	10.60	5.09	0.00	0.00	11.59
					5.09	0.00	0.00	4.48	5.18	0.00	0.00	4.48
30x50	216	223	QV SolaiPsi0	PolG	0.00	0.00	0.00	2.82	0.30	0.00	0.00	2.95
					0.30	0.00	0.00	6.08	2.60	0.00	0.00	7.06
					2.60	0.00	0.00	7.07	3.42	0.00	0.00	7.30
					3.42	0.00	0.00	3.79	3.45	0.00	0.00	3.79
					3.45	0.00	0.00	7.42	5.09	0.00	0.00	8.11
					5.09	0.00	0.00	3.14	5.18	0.00	0.00	3.14
30x50	216	223	QV SolaiPsi1	PolG	0.00	0.00	0.00	2.82	0.30	0.00	0.00	2.95
					0.30	0.00	0.00	6.08	2.60	0.00	0.00	7.06
					2.60	0.00	0.00	7.07	3.42	0.00	0.00	7.30
					3.42	0.00	0.00	3.79	3.45	0.00	0.00	3.79
					3.45	0.00	0.00	7.42	5.09	0.00	0.00	8.11
					5.09	0.00	0.00	3.14	5.18	0.00	0.00	3.14
30x50	216	223	QV SolaiPsi2	PolG	0.00	0.00	0.00	2.42	0.30	0.00	0.00	2.53
					0.30	0.00	0.00	5.21	2.60	0.00	0.00	6.05
					2.60	0.00	0.00	6.06	3.42	0.00	0.00	6.25
					3.42	0.00	0.00	3.25	3.45	0.00	0.00	3.25
					3.45	0.00	0.00	6.36	5.09	0.00	0.00	6.95
					5.09	0.00	0.00	2.69	5.18	0.00	0.00	2.69
30x50	216	223	Neve	PolG	0.00	0.00	0.00	0.29	2.60	0.00	0.00	0.54
					2.60	0.00	0.00	0.54	3.42	0.00	0.00	0.60
					3.42	0.00	0.00	0.00	3.45	0.00	0.00	0.00
					3.45	0.00	0.00	0.62	5.09	0.00	0.00	0.78
30x50	216	223	Neve	PolG	0.30	0.00	0.00	0.54	5.18	0.00	0.00	0.54
30x50	216	223	Neve	PolG	0.00	0.00	0.00	0.20	5.09	0.00	0.00	0.07
30x50	216	223	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 203												
30x50	213	222	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.61	0.00	0.00	3.75
30x50	213	222	QP Solai(Sb.35)	PolG	-0.00	0.00	0.00	2.50	0.44	0.00	0.00	2.50
					0.44	0.00	0.00	2.53	2.28	0.00	0.00	4.86
					2.28	0.00	0.00	4.86	4.01	0.00	0.00	7.04
					4.01	0.00	0.00	2.51	4.05	0.00	0.00	2.51
					4.05	0.00	0.00	7.09	4.61	0.00	0.00	8.51
					4.61	0.00	0.00	2.50	4.67	0.00	0.00	2.50
30x50	213	222	QFissi Solai(Sb.35)	PolG	-0.00	0.00	0.00	1.41	0.08	0.00	0.00	1.41
					0.08	0.00	0.00	1.41	2.18	0.00	0.00	2.91
					2.18	0.00	0.00	2.91	4.01	0.00	0.00	4.21
					4.01	0.00	0.00	1.41	4.61	0.00	0.00	1.41
					4.61	0.00	0.00	1.41	4.67	0.00	0.00	1.41
30x50	213	222	QV Solai(Sb.35)	PolG	-0.00	0.00	0.00	3.20	0.08	0.00	0.00	3.20
					0.08	0.00	0.00	3.22	2.18	0.00	0.00	6.61
					2.18	0.00	0.00	6.61	4.01	0.00	0.00	9.57
					4.01	0.00	0.00	3.22	4.61	0.00	0.00	3.20
					4.61	0.00	0.00	3.20	4.67	0.00	0.00	3.20
30x50	213	222	QV SolaiPsi0(Sb.35)	PolG	-0.00	0.00	0.00	2.24	0.08	0.00	0.00	2.24
					0.08	0.00	0.00	2.25	2.18	0.00	0.00	4.63
					2.18	0.00	0.00	4.63	4.01	0.00	0.00	6.70
					4.01	0.00	0.00	2.25	4.61	0.00	0.00	2.24
					4.61	0.00	0.00	2.24	4.67	0.00	0.00	2.24
30x50	213	222	QV SolaiPsi1(Sb.35)	PolG	-0.00	0.00	0.00	2.24	0.08	0.00	0.00	2.24
					0.08	0.00	0.00	2.25	2.18	0.00	0.00	4.63
					2.18	0.00	0.00	4.63	4.01	0.00	0.00	6.70
					4.01	0.00	0.00	2.25	4.61	0.00	0.00	2.24
					4.61	0.00	0.00	2.24	4.67	0.00	0.00	2.24
30x50	213	222	QV SolaiPsi2(Sb.35)	PolG	-0.00	0.00	0.00	1.92	0.08	0.00	0.00	1.92
					0.08	0.00	0.00	1.93	2.18	0.00	0.00	3.96
					2.18	0.00	0.00	3.96	4.01	0.00	0.00	5.74
					4.01	0.00	0.00	1.93	4.61	0.00	0.00	1.92
					4.61	0.00	0.00	1.92	4.67	0.00	0.00	1.92

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	213	222	Neve	PolG	0.08	0.00	0.00	0.00	2.18	0.00	0.00	0.41
					2.18	0.00	0.00	0.41	4.01	0.00	0.00	0.76
					4.01	0.00	0.00	0.00	4.61	0.00	0.00	0.00
30x50	213	222	Neve(Sb.35)	PolG	0.00	0.00	0.00	0.38	4.67	0.00	0.00	0.38
30x50	213	222	Neve	PolG	0.08	0.00	0.00	0.00	4.61	0.00	0.00	0.00
30x50	213	222	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	213	222	Tamponamento	PolG	0.08	0.00	0.00	2.40	4.69	0.00	0.00	2.40
30x50	222	225	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.48	0.00	0.00	3.75
30x50	222	225	QP Solai	PolG	0.00	0.00	0.00	2.87	1.17	0.00	0.00	2.51
					1.17	0.00	0.00	8.50	1.82	0.00	0.00	9.32
					1.82	0.00	0.00	9.32	2.89	0.00	0.00	9.32
					2.89	0.00	0.00	6.82	3.48	0.00	0.00	6.82
30x50	222	225	QFissi Solai	PolG	0.00	0.00	0.00	1.41	0.60	0.00	0.00	1.41
					0.60	0.00	0.00	4.64	1.76	0.00	0.00	5.45
					1.76	0.00	0.00	5.45	2.89	0.00	0.00	5.45
					2.89	0.00	0.00	4.05	3.48	0.00	0.00	4.05
30x50	222	225	QV Solai	PolG	0.00	0.00	0.00	3.21	0.60	0.00	0.00	3.20
					0.60	0.00	0.00	10.54	1.76	0.00	0.00	12.39
					1.76	0.00	0.00	12.39	2.89	0.00	0.00	12.39
					2.89	0.00	0.00	9.19	3.48	0.00	0.00	9.19
30x50	222	225	QV SolaiPsi0	PolG	0.00	0.00	0.00	2.25	0.60	0.00	0.00	2.24
					0.60	0.00	0.00	7.37	1.76	0.00	0.00	8.67
					1.76	0.00	0.00	8.67	2.89	0.00	0.00	8.68
					2.89	0.00	0.00	6.44	3.48	0.00	0.00	6.44
30x50	222	225	QV SolaiPsi1	PolG	0.00	0.00	0.00	2.25	0.60	0.00	0.00	2.24
					0.60	0.00	0.00	7.37	1.76	0.00	0.00	8.67
					1.76	0.00	0.00	8.67	2.89	0.00	0.00	8.68
					2.89	0.00	0.00	6.44	3.48	0.00	0.00	6.44
30x50	222	225	QV SolaiPsi2	PolG	0.00	0.00	0.00	1.93	0.60	0.00	0.00	1.92
					0.60	0.00	0.00	6.32	1.76	0.00	0.00	7.44
					1.76	0.00	0.00	7.44	2.89	0.00	0.00	7.44
					2.89	0.00	0.00	5.52	3.48	0.00	0.00	5.52
30x50	222	225	Neve	PolG	0.00	0.00	0.00	0.00	0.60	0.00	0.00	0.00
					0.60	0.00	0.00	0.88	1.76	0.00	0.00	1.10
					1.76	0.00	0.00	1.10	3.48	0.00	0.00	1.10
30x50	222	225	Neve(Sb.34)	PolG	0.00	0.00	0.00	0.38	2.89	0.00	0.00	0.38
30x50	222	225	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	222	225	Tamponamento	PolG	0.00	0.00	0.00	2.40	2.91	0.00	0.00	2.40
Trave 204												
30x50	223	226	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	1.66	0.00	0.00	3.75
30x50	223	226	QP Solai	PolG	0.00	0.00	0.00	9.32	1.43	0.00	0.00	9.32
					1.43	0.00	0.00	6.82	1.66	0.00	0.00	6.82
30x50	223	226	QFissi Solai	PolG	0.00	0.00	0.00	5.45	1.43	0.00	0.00	5.45
					1.43	0.00	0.00	4.05	1.66	0.00	0.00	4.05
30x50	223	226	QV Solai	PolG	0.00	0.00	0.00	12.39	1.43	0.00	0.00	12.39
					1.43	0.00	0.00	9.19	1.66	0.00	0.00	9.19
30x50	223	226	QV SolaiPsi0	PolG	0.00	0.00	0.00	8.67	1.43	0.00	0.00	8.68
					1.43	0.00	0.00	6.44	1.66	0.00	0.00	6.44
30x50	223	226	QV SolaiPsi1	PolG	0.00	0.00	0.00	8.67	1.43	0.00	0.00	8.68
					1.43	0.00	0.00	6.44	1.66	0.00	0.00	6.44
30x50	223	226	QV SolaiPsi2	PolG	0.00	0.00	0.00	7.44	1.43	0.00	0.00	7.44
					1.43	0.00	0.00	5.52	1.66	0.00	0.00	5.52
30x50	223	226	Neve(Sb.32)	PolG	0.00	0.00	0.00	0.38	1.43	0.00	0.00	0.38
30x50	223	226	Neve	PolG	0.00	0.00	0.00	1.10	1.66	0.00	0.00	1.10
30x50	223	226	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	223	226	Tamponamento	PolG	0.00	0.00	0.00	2.40	1.43	0.00	0.00	2.40
Trave 205												
30x50	223	217	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.10	0.00	0.00	3.75
30x50	223	217	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	3.89	2.80	0.00	0.00	3.89
					2.80	0.00	0.00	2.50	3.10	0.00	0.00	2.50
30x50	223	217	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.27	2.95	0.00	0.00	2.27
					2.95	0.00	0.00	1.41	3.10	0.00	0.00	1.41

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	223	217	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	5.15	2.95	0.00	0.00	5.15
					2.95	0.00	0.00	3.20	3.10	0.00	0.00	3.20
30x50	223	217	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.61	2.95	0.00	0.00	3.61
					2.95	0.00	0.00	2.24	3.10	0.00	0.00	2.24
30x50	223	217	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.61	2.95	0.00	0.00	3.61
					2.95	0.00	0.00	2.24	3.10	0.00	0.00	2.24
30x50	223	217	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	3.09	2.95	0.00	0.00	3.09
					2.95	0.00	0.00	1.92	3.10	0.00	0.00	1.92
30x50	223	217	Neve(Sb.31)	PolG	0.00	0.00	0.00	0.38	3.10	0.00	0.00	0.38
30x50	223	217	Neve	PolG	0.15	0.00	0.00	0.23	2.95	0.00	0.00	0.23
30x50	223	217	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	223	217	Tamponamento	PolG	0.00	0.00	0.00	2.40	3.10	0.00	0.00	2.40
Trave 206												
30x50	217	218	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	1.79	0.00	0.00	3.75
30x50	217	218	QP Solai(Sb.30)	PolG	-0.00	0.00	0.00	5.05	1.78	0.00	0.00	4.96
					1.78	0.00	0.00	2.50	1.79	0.00	0.00	2.50
30x50	217	218	QFissi Solai(Sb.30)	PolG	-0.00	0.00	0.00	2.90	1.79	0.00	0.00	2.85
30x50	217	218	QV Solai(Sb.30)	PolG	-0.00	0.00	0.00	6.58	1.79	0.00	0.00	6.47
30x50	217	218	QV SolaiPsi0(Sb.30)	PolG	-0.00	0.00	0.00	4.61	1.79	0.00	0.00	4.53
30x50	217	218	QV SolaiPsi1(Sb.30)	PolG	-0.00	0.00	0.00	4.61	1.79	0.00	0.00	4.53
30x50	217	218	QV SolaiPsi2(Sb.30)	PolG	-0.00	0.00	0.00	3.95	1.79	0.00	0.00	3.88
30x50	217	218	Neve	PolG	0.00	0.00	0.00	0.39	1.79	0.00	0.00	0.39
30x50	217	218	Neve(Sb.30)	PolG	0.00	0.00	0.00	0.38	1.79	0.00	0.00	0.38
30x50	217	218	Neve	PolG	0.00	0.00	0.00	0.02	1.79	0.00	0.00	0.00
30x50	217	218	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	217	218	Tamponamento	PolG	-0.00	0.00	0.00	2.40	1.79	0.00	0.00	2.40
30x50	218	219	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.27	0.00	0.00	3.75
30x50	218	219	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	3.88	4.27	0.00	0.00	3.88
30x50	218	219	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.24	4.27	0.00	0.00	2.24
30x50	218	219	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	5.08	4.27	0.00	0.00	5.08
30x50	218	219	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.56	4.27	0.00	0.00	3.56
30x50	218	219	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.56	4.27	0.00	0.00	3.56
30x50	218	219	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	3.05	4.27	0.00	0.00	3.05
30x50	218	219	Neve	PolG	0.15	0.00	0.00	0.23	4.27	0.00	0.00	0.23
30x50	218	219	Neve(Sb.29)	PolG	0.00	0.00	0.00	0.38	4.27	0.00	0.00	0.38
30x50	218	219	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	218	219	Tamponamento	PolG	0.00	0.00	0.00	2.40	4.27	0.00	0.00	2.40
Trave 207												
30x50	204	205	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.90	0.00	0.00	3.75
30x50	204	205	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.35	0.00	0.00	2.50
					0.35	0.00	0.00	3.95	3.50	0.00	0.00	4.93
					3.50	0.00	0.00	4.93	5.60	0.00	0.00	4.97
					5.60	0.00	0.00	2.50	5.90	0.00	0.00	2.50
30x50	204	205	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.26	3.44	0.00	0.00	2.83
					3.44	0.00	0.00	2.83	5.75	0.00	0.00	2.85
					5.75	0.00	0.00	1.41	5.90	0.00	0.00	1.41
30x50	204	205	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	5.13	3.44	0.00	0.00	6.42
					3.44	0.00	0.00	6.42	5.75	0.00	0.00	6.47
					5.75	0.00	0.00	3.20	5.90	0.00	0.00	3.20
30x50	204	205	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.59	3.44	0.00	0.00	4.50
					3.44	0.00	0.00	4.50	5.75	0.00	0.00	4.53

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					5.75	0.00	0.00	2.24	5.90	0.00	0.00	2.24
30x50	204	205	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.59	3.44	0.00	0.00	4.50
					3.44	0.00	0.00	4.50	5.75	0.00	0.00	4.53
					5.75	0.00	0.00	2.24	5.90	0.00	0.00	2.24
30x50	204	205	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	3.08	3.44	0.00	0.00	3.85
					3.44	0.00	0.00	3.85	5.75	0.00	0.00	3.88
					5.75	0.00	0.00	1.92	5.90	0.00	0.00	1.92
30x50	204	205	Neve	PolG	0.15	0.00	0.00	0.23	3.44	0.00	0.00	0.39
					3.44	0.00	0.00	0.39	5.75	0.00	0.00	0.39
30x50	204	205	Neve(Sb.25)	PolG	0.00	0.00	0.00	0.38	5.90	0.00	0.00	0.38
30x50	204	205	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	204	205	Tamponamento	PolG	0.00	0.00	0.00	2.40	5.90	0.00	0.00	2.40
30x50	205	206	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.97	0.00	0.00	3.75
30x50	205	206	QP Solai	PolG	0.00	0.00	0.00	3.50	3.97	0.00	0.00	3.50
30x50	205	206	QFissi Solai	PolG	0.00	0.00	0.00	2.02	3.97	0.00	0.00	2.02
30x50	205	206	QV Solai	PolG	0.00	0.00	0.00	4.59	3.97	0.00	0.00	4.59
30x50	205	206	QV SolaiPsi0	PolG	0.00	0.00	0.00	3.21	3.97	0.00	0.00	3.21
30x50	205	206	QV SolaiPsi1	PolG	0.00	0.00	0.00	3.21	3.97	0.00	0.00	3.21
30x50	205	206	QV SolaiPsi2	PolG	0.00	0.00	0.00	2.75	3.97	0.00	0.00	2.75
30x50	205	206	Neve	PolG	0.00	0.00	0.00	0.17	3.97	0.00	0.00	0.17
30x50	205	206	Neve(Sb.26)	PolG	0.00	0.00	0.00	0.38	3.97	0.00	0.00	0.38
30x50	205	206	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	205	206	Tamponamento	PolG	0.00	0.00	0.00	2.40	3.97	0.00	0.00	2.40
Trave 208												
30x50	209	214	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.30	0.00	0.00	3.75
30x50	209	214	QP Solai	PolG	0.30	0.00	0.00	4.99	3.23	0.00	0.00	4.09
					3.23	0.00	0.00	4.09	3.30	0.00	0.00	3.13
30x50	209	214	QFissi Solai	PolG	0.15	0.00	0.00	3.20	3.30	0.00	0.00	2.65
30x50	209	214	QV Solai	PolG	0.15	0.00	0.00	7.27	3.30	0.00	0.00	6.03
30x50	209	214	QV SolaiPsi0	PolG	0.15	0.00	0.00	5.09	3.30	0.00	0.00	4.22
30x50	209	214	QV SolaiPsi1	PolG	0.15	0.00	0.00	5.09	3.30	0.00	0.00	4.22
30x50	209	214	QV SolaiPsi2	PolG	0.15	0.00	0.00	4.36	3.30	0.00	0.00	3.62
30x50	209	214	Neve	PolG	0.15	0.00	0.00	0.00	3.30	0.00	0.00	0.15
30x50	209	214	Neve	PolG	0.15	0.00	0.00	0.33	3.30	0.00	0.00	0.03
30x50	209	214	Neve	PolG	0.15	0.00	0.00	0.54	3.30	0.00	0.00	0.54
30x50	209	214	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	214	217	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.33	0.00	0.00	3.75
30x50	214	217	QP Solai	PolG	0.42	0.00	0.00	5.67	0.60	0.00	0.00	5.59
					0.60	0.00	0.00	8.72	4.88	0.00	0.00	6.71
					4.88	0.00	0.00	3.13	5.03	0.00	0.00	3.13
30x50	214	217	QFissi Solai	PolG	0.30	0.00	0.00	1.97	0.36	0.00	0.00	1.97
					0.36	0.00	0.00	5.34	4.94	0.00	0.00	4.13
					4.94	0.00	0.00	1.97	5.18	0.00	0.00	1.97
30x50	214	217	QV Solai	PolG	0.30	0.00	0.00	4.48	0.36	0.00	0.00	4.48
					0.36	0.00	0.00	12.13	4.94	0.00	0.00	9.38
					4.94	0.00	0.00	4.48	5.18	0.00	0.00	4.48
30x50	214	217	QV SolaiPsi0	PolG	0.30	0.00	0.00	3.14	0.36	0.00	0.00	3.14
					0.36	0.00	0.00	8.49	4.94	0.00	0.00	6.57
					4.94	0.00	0.00	3.14	5.18	0.00	0.00	3.14
30x50	214	217	QV SolaiPsi1	PolG	0.30	0.00	0.00	3.14	0.36	0.00	0.00	3.14
					0.36	0.00	0.00	8.49	4.94	0.00	0.00	6.57
					4.94	0.00	0.00	3.14	5.18	0.00	0.00	3.14
30x50	214	217	QV SolaiPsi2	PolG	0.30	0.00	0.00	2.69	0.36	0.00	0.00	2.69
					0.36	0.00	0.00	7.28	4.94	0.00	0.00	5.63
					4.94	0.00	0.00	2.69	5.18	0.00	0.00	2.69
30x50	214	217	Neve	PolG	0.36	0.00	0.00	0.75	4.94	0.00	0.00	0.31
30x50	214	217	Neve	PolG	0.30	0.00	0.00	0.54	5.18	0.00	0.00	0.54
30x50	214	217	Neve	PolG	0.36	0.00	0.00	0.16	4.94	0.00	0.00	0.27
30x50	214	217	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 209												
30x50	204	209	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.23	0.00	0.00	3.75
30x50	204	209	QP Solai(Sb.37)	PolG	-0.00	0.00	0.00	2.50	0.29	0.00	0.00	2.50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					0.29	0.00	0.00	3.42	3.23	0.00	0.00	4.36
30x50	204	209	QFissi Solai(Sb.37)	PolG	-0.00	0.00	0.00	2.02	3.23	0.00	0.00	2.60
30x50	204	209	QV Solai(Sb.37)	PolG	-0.00	0.00	0.00	4.60	3.23	0.00	0.00	5.92
30x50	204	209	QV SolaiPsi0(Sb.37)	PolG	-0.00	0.00	0.00	3.22	3.23	0.00	0.00	4.14
30x50	204	209	QV SolaiPsi1(Sb.37)	PolG	-0.00	0.00	0.00	3.22	3.23	0.00	0.00	4.14
30x50	204	209	QV SolaiPsi2(Sb.37)	PolG	-0.00	0.00	0.00	2.76	3.23	0.00	0.00	3.55
30x50	204	209	Neve	PolG	0.00	0.00	0.00	0.16	3.23	0.00	0.00	0.01
30x50	204	209	Neve	PolG	0.00	0.00	0.00	0.01	3.23	0.00	0.00	0.32
30x50	204	209	Neve(Sb.37)	PolG	0.00	0.00	0.00	0.38	3.23	0.00	0.00	0.38
30x50	204	209	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	204	209	Tamponamento	PolG	-0.00	0.00	0.00	2.40	3.23	0.00	0.00	2.40
30x50	209	213	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.11	0.00	0.00	3.75
30x50	209	213	QP Solai	PolG	-0.00	0.00	0.00	2.50	0.30	0.00	0.00	2.50
					0.30	0.00	0.00	3.44	2.80	0.00	0.00	3.44
					2.80	0.00	0.00	2.50	3.11	0.00	0.00	2.50
30x50	209	213	QFissi Solai	PolG	-0.00	0.00	0.00	1.41	0.15	0.00	0.00	1.41
					0.15	0.00	0.00	2.01	2.96	0.00	0.00	2.01
					2.96	0.00	0.00	1.41	3.11	0.00	0.00	1.41
30x50	209	213	QV Solai	PolG	-0.00	0.00	0.00	3.20	0.15	0.00	0.00	3.20
					0.15	0.00	0.00	4.58	2.96	0.00	0.00	4.58
					2.96	0.00	0.00	3.20	3.11	0.00	0.00	3.20
30x50	209	213	QV SolaiPsi0	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.21	2.96	0.00	0.00	3.21
					2.96	0.00	0.00	2.24	3.11	0.00	0.00	2.24
30x50	209	213	QV SolaiPsi1	PolG	-0.00	0.00	0.00	2.24	0.15	0.00	0.00	2.24
					0.15	0.00	0.00	3.21	2.96	0.00	0.00	3.21
					2.96	0.00	0.00	2.24	3.11	0.00	0.00	2.24
30x50	209	213	QV SolaiPsi2	PolG	-0.00	0.00	0.00	1.92	0.15	0.00	0.00	1.92
					0.15	0.00	0.00	2.75	2.96	0.00	0.00	2.75
					2.96	0.00	0.00	1.92	3.11	0.00	0.00	1.92
30x50	209	213	Neve(Sb.36)	PolG	0.00	0.00	0.00	0.38	3.11	0.00	0.00	0.38
30x50	209	213	Neve	PolG	0.15	0.00	0.00	0.17	2.96	0.00	0.00	0.17
30x50	209	213	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	209	213	Tamponamento	PolG	-0.00	0.00	0.00	2.40	3.11	0.00	0.00	2.40
Trave 210												
60x25	214	216	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.10	0.00	0.00	3.75
60x25	214	216	QP Solai	PolG	0.30	0.00	0.00	2.32	2.80	0.00	0.00	2.32
60x25	214	216	QFissi Solai	PolG	0.15	0.00	0.00	1.47	2.95	0.00	0.00	1.47
60x25	214	216	QV Solai	PolG	0.15	0.00	0.00	3.33	2.95	0.00	0.00	3.33
60x25	214	216	QV SolaiPsi0	PolG	0.15	0.00	0.00	2.33	2.95	0.00	0.00	2.33
60x25	214	216	QV SolaiPsi1	PolG	0.15	0.00	0.00	2.33	2.95	0.00	0.00	2.33
60x25	214	216	QV SolaiPsi2	PolG	0.15	0.00	0.00	2.00	2.95	0.00	0.00	2.00
60x25	214	216	Neve	PolG	0.15	0.00	0.00	0.23	2.95	0.00	0.00	0.23
60x25	214	216	Neve	PolG	0.15	0.00	0.00	0.17	2.95	0.00	0.00	0.17
60x25	214	216	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 211												
30x50	204	214	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	5.04	0.00	0.00	3.75
30x50	204	214	QP Solai	PolG	0.30	0.00	0.00	6.64	0.42	0.00	0.00	6.64
					0.42	0.00	0.00	6.65	2.50	0.00	0.00	9.24
					2.50	0.00	0.00	9.24	3.79	0.00	0.00	7.63
					3.79	0.00	0.00	7.63	4.61	0.00	0.00	6.60
					4.61	0.00	0.00	6.60	4.92	0.00	0.00	6.59
30x50	204	214	QFissi Solai	PolG	0.06	0.00	0.00	0.01	0.15	0.00	0.00	0.07
					0.15	0.00	0.00	4.02	2.50	0.00	0.00	5.67
					2.50	0.00	0.00	5.67	3.78	0.00	0.00	4.76
					3.78	0.00	0.00	4.76	4.98	0.00	0.00	3.92
30x50	204	214	QV Solai	PolG	0.06	0.00	0.00	0.02	0.15	0.00	0.00	0.16
					0.15	0.00	0.00	9.13	2.50	0.00	0.00	12.88
					2.50	0.00	0.00	12.88	3.78	0.00	0.00	10.82
					3.78	0.00	0.00	10.82	4.98	0.00	0.00	8.90
30x50	204	214	QV SolaiPsi0	PolG	0.06	0.00	0.00	0.01	0.15	0.00	0.00	0.11
					0.15	0.00	0.00	6.39	2.50	0.00	0.00	9.01
					2.50	0.00	0.00	9.01	3.78	0.00	0.00	7.57
					3.78	0.00	0.00	7.57	4.98	0.00	0.00	6.23

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
30x50	204	214	QV SolaiPsi1	PolG	0.06	0.00	0.00	0.01	0.15	0.00	0.00	0.11
					0.15	0.00	0.00	6.39	2.50	0.00	0.00	9.01
					2.50	0.00	0.00	9.01	3.78	0.00	0.00	7.57
					3.78	0.00	0.00	7.57	4.98	0.00	0.00	6.23
30x50	204	214	QV SolaiPsi2	PolG	0.06	0.00	0.00	0.01	0.15	0.00	0.00	0.10
					0.15	0.00	0.00	5.48	2.50	0.00	0.00	7.73
					2.50	0.00	0.00	7.73	3.78	0.00	0.00	6.49
					3.78	0.00	0.00	6.49	4.98	0.00	0.00	5.34
30x50	204	214	Neve	PolG	0.15	0.00	0.00	1.08	4.98	0.00	0.00	1.07
30x50	204	214	Neve	PolG	0.06	0.00	0.00	0.00	4.98	0.00	0.00	0.00
30x50	204	214	Neve	PolG	0.15	0.00	0.00	0.00	4.98	0.00	0.00	0.00
30x50	204	214	Neve	PolG	0.06	0.00	0.00	0.00	2.50	0.00	0.00	0.47
					2.50	0.00	0.00	0.47	4.98	0.00	0.00	0.00
30x50	204	214	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 212												
30x50	205	210	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.79	0.00	0.00	3.75
30x50	205	210	QP Solai	PolG	0.31	0.00	0.00	11.98	3.48	0.00	0.00	11.94
					3.48	0.00	0.00	6.60	3.79	0.00	0.00	6.59
30x50	205	210	QFissi Solai	PolG	0.16	0.00	0.00	7.16	3.63	0.00	0.00	7.14
					3.63	0.00	0.00	3.92	3.79	0.00	0.00	3.92
30x50	205	210	QV Solai	PolG	0.16	0.00	0.00	16.28	3.63	0.00	0.00	16.22
					3.63	0.00	0.00	8.91	3.79	0.00	0.00	8.90
30x50	205	210	QV SolaiPsi0	PolG	0.16	0.00	0.00	11.39	3.63	0.00	0.00	11.35
					3.63	0.00	0.00	6.23	3.79	0.00	0.00	6.23
30x50	205	210	QV SolaiPsi1	PolG	0.16	0.00	0.00	11.39	3.63	0.00	0.00	11.35
					3.63	0.00	0.00	6.23	3.79	0.00	0.00	6.23
30x50	205	210	QV SolaiPsi2	PolG	0.16	0.00	0.00	9.77	3.63	0.00	0.00	9.73
					3.63	0.00	0.00	5.34	3.79	0.00	0.00	5.34
30x50	205	210	Neve	PolG	0.16	0.00	0.00	0.88	3.63	0.00	0.00	0.88
30x50	205	210	Neve	PolG	0.16	0.00	0.00	1.08	3.79	0.00	0.00	1.07
30x50	205	210	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	210	218	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.70	0.00	0.00	3.75
30x50	210	218	QP Solai	PolG	0.00	0.00	0.00	5.35	0.01	0.00	0.00	5.35
					0.01	0.00	0.00	11.94	1.14	0.00	0.00	11.92
					1.14	0.00	0.00	11.92	4.30	0.00	0.00	7.98
					4.30	0.00	0.00	7.98	4.40	0.00	0.00	5.35
30x50	210	218	QFissi Solai	PolG	0.00	0.00	0.00	3.22	0.01	0.00	0.00	3.22
					0.01	0.00	0.00	7.14	1.21	0.00	0.00	7.13
					1.21	0.00	0.00	7.13	4.44	0.00	0.00	4.85
					4.44	0.00	0.00	4.85	4.56	0.00	0.00	3.22
30x50	210	218	QV Solai	PolG	0.00	0.00	0.00	7.31	0.01	0.00	0.00	7.31
					0.01	0.00	0.00	16.22	1.21	0.00	0.00	16.20
					1.21	0.00	0.00	16.20	4.44	0.00	0.00	11.02
					4.44	0.00	0.00	11.02	4.56	0.00	0.00	7.31
30x50	210	218	QV SolaiPsi0	PolG	0.00	0.00	0.00	5.12	0.01	0.00	0.00	5.12
					0.01	0.00	0.00	11.35	1.21	0.00	0.00	11.34
					1.21	0.00	0.00	11.34	4.44	0.00	0.00	7.72
					4.44	0.00	0.00	7.72	4.56	0.00	0.00	5.12
30x50	210	218	QV SolaiPsi1	PolG	0.00	0.00	0.00	5.12	0.01	0.00	0.00	5.12
					0.01	0.00	0.00	11.35	1.21	0.00	0.00	11.34
					1.21	0.00	0.00	11.34	4.44	0.00	0.00	7.72
					4.44	0.00	0.00	7.72	4.56	0.00	0.00	5.12
30x50	210	218	QV SolaiPsi2	PolG	0.00	0.00	0.00	4.39	0.01	0.00	0.00	4.39
					0.01	0.00	0.00	9.73	1.21	0.00	0.00	9.72
					1.21	0.00	0.00	9.72	4.44	0.00	0.00	6.61
					4.44	0.00	0.00	6.61	4.56	0.00	0.00	4.39
30x50	210	218	Neve	PolG	0.00	0.00	0.00	0.88	4.55	0.00	0.00	0.88
30x50	210	218	Neve	PolG	0.01	0.00	0.00	1.07	1.21	0.00	0.00	1.07
					1.21	0.00	0.00	1.07	4.44	0.00	0.00	0.45
					4.44	0.00	0.00	0.45	4.56	0.00	0.00	0.00
30x50	210	218	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 213												
30x50	206	211	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	3.47	0.00	0.00	3.75
30x50	206	211	QP Solai	PolG	0.00	0.00	0.00	7.85	3.17	0.00	0.00	7.85

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
					3.17	0.00	0.00	2.50	3.77	0.00	0.00	2.50
30x50	206	211	QFissi Solai	PolG	0.00	0.00	0.00	4.63	3.32	0.00	0.00	4.63
					3.32	0.00	0.00	1.41	3.77	0.00	0.00	1.41
30x50	206	211	QV Solai	PolG	0.00	0.00	0.00	10.51	3.32	0.00	0.00	10.51
					3.32	0.00	0.00	3.20	3.77	0.00	0.00	3.20
30x50	206	211	QV SolaiPsi0	PolG	0.00	0.00	0.00	7.36	3.32	0.00	0.00	7.36
					3.32	0.00	0.00	2.24	3.77	0.00	0.00	2.24
30x50	206	211	QV SolaiPsi1	PolG	0.00	0.00	0.00	7.36	3.32	0.00	0.00	7.36
					3.32	0.00	0.00	2.24	3.77	0.00	0.00	2.24
30x50	206	211	QV SolaiPsi2	PolG	0.00	0.00	0.00	6.31	3.32	0.00	0.00	6.31
					3.32	0.00	0.00	1.92	3.77	0.00	0.00	1.92
30x50	206	211	Neve(Sb.27)	PolG	0.00	0.00	0.00	0.38	3.77	0.00	0.00	0.38
30x50	206	211	Neve	PolG	0.00	0.00	0.00	0.88	3.32	0.00	0.00	0.88
30x50	206	211	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	206	211	Tamponamento	PolG	0.30	0.00	0.00	2.40	3.77	0.00	0.00	2.40
30x50	211	219	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.70	0.00	0.00	3.75
30x50	211	219	QP Solai	PolG	0.00	0.00	0.00	7.85	4.40	0.00	0.00	7.85
					4.40	0.00	0.00	2.50	4.70	0.00	0.00	2.50
30x50	211	219	QFissi Solai	PolG	0.00	0.00	0.00	4.63	4.55	0.00	0.00	4.63
					4.55	0.00	0.00	1.41	4.70	0.00	0.00	1.41
30x50	211	219	QV Solai	PolG	0.00	0.00	0.00	10.51	4.55	0.00	0.00	10.51
					4.55	0.00	0.00	3.20	4.70	0.00	0.00	3.20
30x50	211	219	QV SolaiPsi0	PolG	0.00	0.00	0.00	7.36	4.55	0.00	0.00	7.36
					4.55	0.00	0.00	2.24	4.70	0.00	0.00	2.24
30x50	211	219	QV SolaiPsi1	PolG	0.00	0.00	0.00	7.36	4.55	0.00	0.00	7.36
					4.55	0.00	0.00	2.24	4.70	0.00	0.00	2.24
30x50	211	219	QV SolaiPsi2	PolG	0.00	0.00	0.00	6.31	4.55	0.00	0.00	6.31
					4.55	0.00	0.00	1.92	4.70	0.00	0.00	1.92
30x50	211	219	Neve(Sb.28)	PolG	0.00	0.00	0.00	0.38	4.70	0.00	0.00	0.38
30x50	211	219	Neve	PolG	0.00	0.00	0.00	0.88	4.55	0.00	0.00	0.88
30x50	211	219	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	211	219	Tamponamento	PolG	0.00	0.00	0.00	2.40	4.70	0.00	0.00	2.40
Trave 214												
30x50	210	211	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.27	0.00	0.00	3.75
30x50	210	211	QP Solai	PolG	0.30	0.00	0.00	2.37	4.27	0.00	0.00	2.37
30x50	210	211	QFissi Solai	PolG	0.15	0.00	0.00	1.44	4.27	0.00	0.00	1.44
30x50	210	211	QV Solai	PolG	0.15	0.00	0.00	3.27	4.27	0.00	0.00	3.27
30x50	210	211	QV SolaiPsi0	PolG	0.15	0.00	0.00	2.29	4.27	0.00	0.00	2.29
30x50	210	211	QV SolaiPsi1	PolG	0.15	0.00	0.00	2.29	4.27	0.00	0.00	2.29
30x50	210	211	QV SolaiPsi2	PolG	0.15	0.00	0.00	1.96	4.27	0.00	0.00	1.96
30x50	210	211	Neve	PolG	0.15	0.00	0.00	0.23	4.27	0.00	0.00	0.23
30x50	210	211	Neve	PolG	0.15	0.00	0.00	0.17	4.27	0.00	0.00	0.17
30x50	210	211	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Trave 8000												
30x50	37	38	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	4.05	0.00	0.00	3.75
30x50	37	38	QP Solai(Sb.1)	PolG	-0.00	0.00	0.00	2.25	4.05	0.00	0.00	2.25
30x50	37	38	QFissi Solai(Sb.1)	PolG	-0.00	0.00	-0.00	3.90	4.05	0.00	-0.00	3.90
30x50	37	38	QV Solai(Sb.1)	PolG	-0.00	0.00	-0.00	6.00	4.05	0.00	-0.00	6.00
30x50	37	38	QV SolaiPsi0(Sb.1)	PolG	-0.00	0.00	-0.00	4.20	4.05	0.00	-0.00	4.20
30x50	37	38	QV SolaiPsi1(Sb.1)	PolG	-0.00	0.00	-0.00	4.20	4.05	0.00	-0.00	4.20
30x50	37	38	QV SolaiPsi2(Sb.1)	PolG	-0.00	0.00	0.00	3.60	4.05	0.00	0.00	3.60
30x50	37	38	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
30x50	38	35	Peso Proprio	UnifG	0.00	0.00	0.00	3.75	1.73	0.00	0.00	3.75
30x50	38	35	QP Solai(Sb.2)	PolG	-0.00	0.00	0.00	2.25	1.73	0.00	0.00	2.25
30x50	38	35	QFissi Solai(Sb.2)	PolG	-0.00	0.00	0.00	3.90	1.73	0.00	0.00	3.90
30x50	38	35	QV Solai(Sb.2)	PolG	-0.00	0.00	0.00	6.00	1.73	0.00	0.00	6.00
30x50	38	35	QV SolaiPsi0(Sb.2)	PolG	-0.00	0.00	0.00	4.20	1.73	0.00	0.00	4.20
30x50	38	35	QV SolaiPsi1(Sb.2)	PolG	-0.00	0.00	0.00	4.20	1.73	0.00	0.00	4.20
30x50	38	35	QV SolaiPsi2(Sb.2)	PolG	-0.00	0.00	0.00	3.60	1.73	0.00	0.00	3.60
30x50	38	35	Termico	Termico	ΔXY=15.00°C,ΔXZ=15.00°C							
Fondazione 9001												
F50x100	2	3	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.14	0.00	0.00	12.50
F50x100	2	3	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
F50x100	3	4	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.63	0.00	0.00	12.50
F50x100	3	4	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	3	4	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.63	0.00	0.00	9.34
F50x100	4	5	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.90	0.00	0.00	12.50
F50x100	4	5	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	4	5	Tamponamento	PolG	0.00	0.00	0.00	9.34	5.90	0.00	0.00	9.34
F50x100	5	6	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.97	0.00	0.00	12.50
F50x100	5	6	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	5	6	Tamponamento	PolG	0.00	0.00	0.00	9.34	3.97	0.00	0.00	9.34
F50x100	6	7	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.30	0.00	0.00	12.50
F50x100	6	7	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	6	7	Tamponamento	PolG	0.00	0.00	0.00	9.34	5.30	0.00	0.00	9.34
Fondazione 9002												
F50x100	10	11	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.27	0.00	0.00	12.50
F50x100	10	11	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	11	12	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.30	0.00	0.00	12.50
F50x100	11	12	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9003												
F50x100	17	18	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	1.79	0.00	0.00	12.50
F50x100	17	18	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	17	18	Tamponamento	PolG	0.00	0.00	0.00	9.34	1.79	0.00	0.00	9.34
F50x100	18	19	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.27	0.00	0.00	12.50
F50x100	18	19	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	18	19	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.27	0.00	0.00	9.34
F50x100	19	20	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.30	0.00	0.00	12.50
F50x100	19	20	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9004												
F50x100	27	28	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.00	0.00	0.00	12.50
F50x100	27	28	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	27	28	Tamponamento	PolG	0.00	0.00	0.00	9.34	5.00	0.00	0.00	9.34
Fondazione 9005												
F50x100	15	13	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.79	0.00	0.00	12.50
F50x100	15	13	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9006												
F50x100	21	22	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.74	0.00	0.00	12.50
F50x100	21	22	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9007												
F50x100	24	25	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.45	0.00	0.00	12.50
F50x100	24	25	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	25	26	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	6.04	0.00	0.00	12.50
F50x100	25	26	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9008												
F50x100	29	30	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.34	0.00	0.00	12.50
F50x100	29	30	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	29	30	Tamponamento	PolG	0.00	0.00	0.00	9.34	5.34	0.00	0.00	9.34
F50x100	30	31	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	6.14	0.00	0.00	12.50
F50x100	30	31	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	30	31	Tamponamento	PolG	0.00	0.00	0.00	9.34	6.14	0.00	0.00	9.34
Fondazione 9009												
F50x100	2	15	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.82	0.00	0.00	12.50
F50x100	2	15	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	2	15	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.82	0.00	0.00	9.34
F50x100	15	21	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.31	0.00	0.00	12.50
F50x100	15	21	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	15	21	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.31	0.00	0.00	9.34
F50x100	21	24	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	2.88	0.00	0.00	12.50
F50x100	21	24	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	21	24	Tamponamento	PolG	0.00	0.00	0.00	9.34	2.88	0.00	0.00	9.34
F50x100	24	29	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.40	0.00	0.00	12.50
F50x100	24	29	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	24	29	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.40	0.00	0.00	9.34
Fondazione 9010												
F50x100	13	22	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.61	0.00	0.00	12.50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
F50x100	13	22	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	22	25	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	2.88	0.00	0.00	12.50
F50x100	22	25	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	25	30	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.40	0.00	0.00	12.50
F50x100	25	30	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9011												
F50x100	23	26	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	1.89	0.00	0.00	12.50
F50x100	23	26	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	23	26	Tamponamento	PolG	0.00	0.00	0.00	9.34	1.43	0.00	0.00	9.34
F50x100	26	31	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.40	0.00	0.00	12.50
F50x100	26	31	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	26	31	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.40	0.00	0.00	9.34
Fondazione 9012												
F50x100	2	8	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	2.52	0.00	0.00	12.50
F50x100	2	8	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	2	8	Tamponamento	PolG	1.19	0.00	0.00	9.34	3.71	0.00	0.00	9.34
F50x100	8	13	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.28	0.00	0.00	12.50
F50x100	8	13	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	13	16	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.30	0.00	0.00	12.50
F50x100	13	16	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	16	23	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.33	0.00	0.00	12.50
F50x100	16	23	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	16	23	Tamponamento	PolG	0.00	0.00	0.00	9.34	5.33	0.00	0.00	9.34
Fondazione 9013												
F50x100	3	9	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.28	0.00	0.00	12.50
F50x100	3	9	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	9	14	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.30	0.00	0.00	12.50
F50x100	9	14	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	14	17	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	5.33	0.00	0.00	12.50
F50x100	14	17	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	14	17	Tamponamento	PolG	-0.00	0.00	0.00	9.34	5.33	0.00	0.00	9.34
Fondazione 9014												
F50x100	17	23	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.10	0.00	0.00	12.50
F50x100	17	23	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	17	23	Tamponamento	PolG	-0.00	0.00	0.00	5.04	3.10	0.00	0.00	5.04
Fondazione 9015												
F50x100	14	16	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.10	0.00	0.00	12.50
F50x100	14	16	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9016												
F50x100	9	13	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.11	0.00	0.00	12.50
F50x100	9	13	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9017												
F50x100	3	8	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.05	0.00	0.00	12.50
F50x100	3	8	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	3	8	Tamponamento	PolG	0.00	0.00	0.00	9.34	3.05	0.00	0.00	9.34
Fondazione 9018												
F50x100	4	14	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.72	0.00	0.00	12.50
F50x100	4	14	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9019												
F50x100	5	10	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.77	0.00	0.00	12.50
F50x100	5	10	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	10	18	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.70	0.00	0.00	12.50
F50x100	10	18	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
Fondazione 9020												
F50x100	6	11	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.77	0.00	0.00	12.50
F50x100	6	11	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	11	19	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.70	0.00	0.00	12.50
F50x100	11	19	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	19	27	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.13	0.00	0.00	12.50
F50x100	19	27	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	19	27	Tamponamento	PolG	0.02	0.00	0.00	9.34	4.15	0.00	0.00	9.34
Fondazione 9021												
F50x100	7	12	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	3.77	0.00	0.00	12.50

Sezione	Ni	Nf	Cond.	Tipo c.	Xi	QXi	QYi	QZi	Xf	QXf	QYf	QZf
F50x100	7	12	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	7	12	Tamponamento	PolG	0.00	0.00	0.00	9.34	3.77	0.00	0.00	9.34
F50x100	12	20	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.70	0.00	0.00	12.50
F50x100	12	20	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	12	20	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.70	0.00	0.00	9.34
F50x100	20	28	Peso Proprio	UnifG	0.00	0.00	0.00	12.50	4.13	0.00	0.00	12.50
F50x100	20	28	Termico	Termico	ΔXY=10.00°C,ΔXZ=10.00°C							
F50x100	20	28	Tamponamento	PolG	0.00	0.00	0.00	9.34	4.13	0.00	0.00	9.34

Tabella solai tipo

Sol.N°	Descrizione	Spessore	QP	QF	QVar.	ψ0	ψ1	ψ2	Luce netta	Def	%QX	%QY
		m	kN/m^2	kN/m^2	kN/m^2							
1	Scuola	0.25	3.13	2.46	3.00	0.70	0.70	0.60	Si	No	80	20
2	Terrazzo	0.25	3.13	1.76	4.00	0.70	0.70	0.60	Si	No	80	20
3	Scala	0.15	1.50	2.60	4.00	0.70	0.70	0.60	Si	No	100	0

Dati solai

Solaio n°	Nodi	Tipo
1	118-110-111-119	Scuola
1	114-104-105-110-118-117	Scuola
1	110-105-106-111	Scuola
1	119-111-112-120	Terrazzo
1	111-106-107-112	Terrazzo
2	108-102-103	Terrazzo
3	130-125-126-131	Terrazzo
3	115-113-122-121	Terrazzo
3	124-121-122-125	Terrazzo
3	129-124-125-130	Terrazzo
4	109-103-104-114	Terrazzo
4	116-113-109-114	Scuola
4	113-108-103-109	Terrazzo
5	122-113-116-123-126-125	Scuola
6	127-119-120-128	Terrazzo
7	115-102-108-113	Terrazzo
8	222-213-216-223-226-225	Terrazzo
9	223-216-214-217	Terrazzo
10	216-213-209-214	Terrazzo
11	218-217-214-204-205-210	Terrazzo
11	218-210-211-219	Terrazzo
11	210-205-206-211	Terrazzo
11	214-209-204	Terrazzo

Tabulati di verifica

L'esito di ogni elaborazione viene sintetizzato nei disegni e schemi grafici allegati, che evidenziano i valori numerici nei punti e/o nelle sezioni significative, ai fini della valutazione del comportamento complessivo della struttura, e quelli necessari ai fini delle verifiche di misura della sicurezza.

Di seguito si riportano le tabelle relative a:

- Baricentri rigidezze e masse
- Forze sismiche e masse
- Spostamenti Relativi dei nodi (SLD)
- Fattori di partecipazione e masse modali
- Massime tensioni sul terreno aste
- Massimi spostamenti dei nodi

- Massime reazioni vincolari
- Massimi spostamenti degli impalcati
- Massimi spostamenti degli impalcati (SLD)
- Massime sollecitazioni travi
- Massime sollecitazioni pilastri
- Massime sollecitazioni travi di fondazione

Centri di rigidezza e Centri di massa

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Centri rigidezze

Piano	Kx	Ky	Kxy	Kϕ	X	Y	$r^2/ls^2>=1$
	kN/m	kN/m	kN/m	kN*m/rad	m	m	
1	3.991421E05	3.721288E05	3.598796E04	3.418134E07	11.62	7.23	1.153
2	1.168746E05	9.936423E04	1.002472E04	5.517353E06	10.82	5.80	1.619

Ellissi delle rigidezze

Piano	Kξ	Kη	alfa	rξ	rη
	kN/m	kN/m	°	m	m
1	4.240745E05	3.471964E05	-34.71	9.92	8.98
2	1.214291E05	9.480970E04	24.43	7.63	6.74

Baricentri masse per posizione masse

Piano	Pos.Masse	X	Y	Peso Sism.
		m	m	kN
0	1	0.00	0.00	0.00
0	2	0.00	0.00	0.00
0	3	0.00	0.00	0.00
0	4	0.00	0.00	0.00
1	1	11.38	6.09	4331.83
1	2	12.62	6.91	4331.83
1	3	11.38	7.73	4331.83
1	4	10.13	6.91	4331.83
2	1	12.35	4.97	1764.31
2	2	13.06	5.56	1764.31
2	3	12.35	6.14	1764.31
2	4	11.63	5.56	1764.31

Risultati Analisi Dinamica - Baricentri masse e masse

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	4356.01	11.40	6.09	4.31
2	Si	1770.62	12.37	4.97	8.14

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	4356.01	12.65	6.91	4.31
2	Si	1770.62	13.08	5.55	8.14

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00

Piano	Rigido	Massa	X	Y	Z
1	Si	4356.01	11.40	7.73	4.31
2	Si	1770.62	12.37	6.13	8.14

Piano	Rigido	Massa	X	Y	Z
		kN	m	m	m
0	No	0.00	0.00	0.00	0.00
1	Si	4356.01	10.15	6.91	4.31
2	Si	1770.62	11.65	5.55	8.14

Verifica Degli Spostamenti Relativi

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Interp.	Comb.	ηXv	ηXh	ηYv	ηYh	Nodo1	Nodo2	η	ηAmm	Cs
		cm	cm	cm	cm			cm	cm	
0-1	(53+54)-IV-3	0.01	0.17	0.02	0.41	2	102	0.43	2.19	5.1
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	3	103	0.42	2.19	5.2
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	4	104	0.43	2.19	5.1
0-1	(53+54)-VI-4	0.01	0.14	0.01	0.45	5	105	0.47	2.19	4.7
0-1	(53+54)-VI-4	0.01	0.14	0.01	0.51	6	106	0.52	2.19	4.2
0-1	(53+54)-II-4	0.01	0.16	0.01	0.59	7	107	0.60	2.19	3.6
0-1	(53+54)-IV-3	0.01	0.16	0.02	0.41	8	108	0.42	2.19	5.2
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	9	109	0.42	2.19	5.2
0-1	(53+54)-VI-4	0.01	0.06	0.01	0.45	10	110	0.46	2.19	4.8
0-1	(53+54)-VI-4	0.01	0.06	0.01	0.51	11	111	0.52	2.19	4.2
0-1	(53+54)-II-4	0.01	0.07	0.01	0.59	12	112	0.60	2.19	3.6
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	13	113	0.42	2.19	5.2
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	14	114	0.43	2.19	5.1
0-1	(53+54)-IV-3	0.01	0.16	0.02	0.41	15	115	0.43	2.19	5.1
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	16	116	0.42	2.19	5.2
0-1	(53+54)-VI-4	0.04	0.02	0.05	0.18	17	35	0.23	1.33	5.7
0-1	(53+54)-VI-4	0.01	0.01	0.01	0.45	18	118	0.46	2.19	4.8
0-1	(53+54)-VI-4	0.01	0.01	0.01	0.51	19	119	0.52	2.19	4.2
0-1	(53+54)-II-4	0.01	0.00	0.01	0.59	20	120	0.60	2.19	3.6
0-1	(53+54)-IV-3	0.01	0.15	0.02	0.41	21	121	0.43	2.19	5.1
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	22	122	0.42	2.19	5.2
0-1	(53+54)-VIII-4	0.01	0.12	0.01	0.29	23	36	0.30	1.33	4.5
0-1	(53+54)-IV-3	0.01	0.15	0.02	0.41	24	124	0.43	2.19	5.1
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	25	125	0.42	2.19	5.2
0-1	(53+54)-VIII-4	0.01	0.01	0.01	0.41	26	126	0.43	2.19	5.1
0-1	(53+54)-VI-4	0.01	0.05	0.01	0.51	27	127	0.53	2.19	4.2
0-1	(53+54)-II-4	0.01	0.07	0.01	0.59	28	128	0.60	2.19	3.6
0-1	(53+54)-IV-3	0.01	0.15	0.02	0.41	29	129	0.43	2.19	5.1
0-1	(53+54)-VIII-4	0.01	0.01	0.02	0.41	30	130	0.42	2.19	5.2
0-1	(53+54)-VIII-4	0.01	0.01	0.01	0.41	31	131	0.43	2.19	5.1
1-2	(53+54)-VI-4	0.04	0.02	0.02	0.63	35	217	0.65	2.73	4.2
1-2	(53+54)-VIII-4	0.01	0.10	0.03	0.49	36	223	0.52	2.73	5.3
1-2	(53+54)-I-4	0.01	0.40	0.01	0.04	104	204	0.40	1.87	4.6
1-2	(53+54)-VI-4	0.01	0.19	0.01	0.44	105	205	0.46	1.87	4.1
1-2	(53+54)-II-4	0.01	0.22	0.02	0.54	106	206	0.56	1.87	3.3
1-2	(53+54)-III-3	0.01	0.35	0.01	0.18	109	209	0.36	1.87	5.2
1-2	(53+54)-VI-4	0.01	0.06	0.01	0.43	110	210	0.45	1.87	4.2
1-2	(53+54)-II-4	0.01	0.07	0.02	0.54	111	211	0.56	1.87	3.3
1-2	(53+54)-IV-3	0.01	0.16	0.01	0.35	113	213	0.36	1.87	5.2
1-2	(53+54)-VIII-4	0.01	0.01	0.01	0.36	114	214	0.37	1.87	5.1
1-2	(53+54)-VIII-4	0.01	0.01	0.01	0.35	116	216	0.36	1.87	5.2
1-2	(53+54)-VI-4	0.01	0.00	0.01	0.43	118	218	0.45	1.87	4.2
1-2	(53+54)-II-4	0.01	0.03	0.02	0.54	119	219	0.56	1.87	3.3
1-2	(53+54)-IV-3	0.01	0.16	0.01	0.35	122	222	0.36	1.87	5.2
1-2	(53+54)-V-3	0.01	0.38	0.01	0.03	125	225	0.39	1.87	4.8
1-2	(53+54)-V-3	0.01	0.38	0.01	0.01	126	226	0.39	1.87	4.8

Interp.	Comb.	ηXv	ηXh	ηYv	ηYh	Nodo1	Nodo2	η	ηAmm	Cs
Minimo										
1-2	(53+54)-II-4	0.01	0.07	0.02	0.54	111	211	0.56	1.87	3.3

Periodi di vibrazione e Masse modali

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Posizione masse 1

Numero di Frequenze calcolate =25, filtrate=14

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3425	-20.039	229.061	3938.04	514543.26	0.64	83.55
2(2)	0.3071	-222.124	-3.998	483853.02	156.79	78.57	0.03
3(3)	0.2489	65.128	55.089	41595.85	29761.51	6.75	4.83
4(4)	0.1500	-3.651	-38.850	130.72	14801.21	0.02	2.40
5(5)	0.1319	-44.465	56.710	19389.38	31538.48	3.15	5.12
6(6)	0.1276	-56.164	-36.242	30933.69	12880.95	5.02	2.09
7(7)	0.1211	26.627	3.115	6952.70	95.16	1.13	0.02
8(8)	0.1102	-10.815	-8.933	1147.00	782.58	0.19	0.13
9(12)	0.0931	24.517	-9.919	5894.37	964.82	0.96	0.16
10(14)	0.0891	-23.004	-15.345	5189.33	2309.27	0.84	0.37
11(17)	0.0823	-17.029	-1.067	2843.81	11.16	0.46	0.00
12(19)	0.0788	-16.731	-3.703	2745.16	134.44	0.45	0.02
13(23)	0.0675	-9.251	4.778	839.33	223.92	0.14	0.04
14(25)	0.0638	-8.302	1.797	675.83	31.66	0.11	0.01
Somma delle Masse Modali [kgm*g]				606128.25	608235.22		
Masse strutturali libere [kgm*g]				615853.65	615853.65		
Percentuale				98.42	98.76	98.42	98.76

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1(1)	0.3425	414.442	1684409.60	3.97
2(2)	0.3071	-669.326	4393358.52	10.36
3(3)	0.2489	-1687.166	27914924.96	65.85
4(4)	0.1500	-829.300	6744411.45	15.91
5(5)	0.1319	-286.575	805373.94	1.90
6(6)	0.1276	17.216	2906.43	0.01
7(7)	0.1211	23.143	5252.35	0.01
8(8)	0.1102	-29.264	8398.14	0.02
9(12)	0.0931	-38.696	14684.01	0.03
10(14)	0.0891	-50.027	24542.93	0.06
11(17)	0.0823	-33.246	10839.30	0.03
12(19)	0.0788	53.501	28070.56	0.07
13(23)	0.0675	65.832	42500.35	0.10
14(25)	0.0638	14.378	2027.37	0.00

Posizione masse 2

Numero di Frequenze calcolate =25, filtrate=18

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3538	-27.441	221.166	7384.31	479687.56	1.20	77.89
2(2)	0.3019	-229.118	-17.106	514800.51	2869.53	83.59	0.47
3(3)	0.2461	26.246	78.819	6755.28	60923.33	1.10	9.89
4(4)	0.1606	13.620	-49.000	1819.27	23545.76	0.30	3.82
5(5)	0.1274	-71.764	-19.989	50504.61	3918.48	8.20	0.64

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
6(6)	0.1230	-15.896	57.328	2477.86	32229.95	0.40	5.23
7(7)	0.1194	-20.614	3.906	4167.39	149.60	0.68	0.02
8(8)	0.1149	4.809	8.724	226.77	746.41	0.04	0.12
9(10)	0.1001	10.441	-1.381	1069.12	18.70	0.17	0.00
10(11)	0.0960	13.005	9.935	1658.57	968.01	0.27	0.16
11(12)	0.0945	6.737	-14.443	445.12	2045.73	0.07	0.33
12(13)	0.0923	-24.467	4.248	5870.45	176.97	0.95	0.03
13(16)	0.0846	-12.707	-1.858	1583.57	33.85	0.26	0.01
14(18)	0.0832	-10.781	-5.308	1139.93	276.30	0.19	0.04
15(20)	0.0748	-14.995	-2.682	2205.07	70.53	0.36	0.01
16(21)	0.0748	-8.819	-7.272	762.73	518.58	0.12	0.08
17(22)	0.0725	-18.581	0.441	3385.94	1.91	0.55	0.00
18(23)	0.0700	9.630	-4.488	909.37	197.54	0.15	0.03
Somma delle Masse Modali [kgm*g]				607165.88	608378.72		
Masse strutturali libere [kgm*g]				615853.65	615853.65		
Percentuale				98.59	98.79	98.59	98.79

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1(1)	0.3538	867.417	7378643.53	16.75
2(2)	0.3019	-257.492	650204.06	1.48
3(3)	0.2461	-1670.009	27350070.76	62.09
4(4)	0.1606	-787.843	6086949.39	13.82
5(5)	0.1274	-207.837	423609.43	0.96
6(6)	0.1230	-346.518	1177529.78	2.67
7(7)	0.1194	-34.270	11517.44	0.03
8(8)	0.1149	57.137	32014.87	0.07
9(10)	0.1001	-142.338	198684.24	0.45
10(11)	0.0960	2.975	86.82	0.00
11(12)	0.0945	116.683	133516.18	0.30
12(13)	0.0923	41.990	17291.07	0.04
13(16)	0.0846	76.284	57067.85	0.13
14(18)	0.0832	-58.884	34003.20	0.08
15(20)	0.0748	-21.171	4395.55	0.01
16(21)	0.0748	-37.549	13826.63	0.03
17(22)	0.0725	23.241	5297.04	0.01
18(23)	0.0700	-84.327	69735.68	0.16

Posizione masse 3

Numero di Frequenze calcolate =25, filtrate=18

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3443	55.849	-221.581	30587.81	481489.94	4.97	78.18
2(2)	0.3008	-223.959	-60.484	491877.19	35875.27	79.87	5.83
3(3)	0.2546	23.905	-51.822	5604.21	26335.81	0.91	4.28
4(4)	0.1562	33.383	-31.696	10928.47	9852.30	1.77	1.60
5(5)	0.1312	-20.418	-69.863	4088.33	47865.16	0.66	7.77
6(6)	0.1234	57.736	-9.632	32689.55	909.77	5.31	0.15
7(7)	0.1193	-33.345	-3.789	10903.93	140.78	1.77	0.02
8(8)	0.1071	2.915	-13.982	83.31	1917.25	0.01	0.31
9(10)	0.1026	-10.250	14.959	1030.27	2194.46	0.17	0.36
10(11)	0.0990	-9.299	-6.893	847.91	465.93	0.14	0.08
11(12)	0.0960	26.565	0.131	6920.35	0.17	1.12	0.00
12(15)	0.0887	12.647	1.745	1568.49	29.86	0.25	0.00
13(16)	0.0852	-4.969	-9.474	242.15	880.17	0.04	0.14
14(18)	0.0810	11.355	-0.031	1264.43	0.01	0.21	0.00
15(19)	0.0769	8.299	-2.870	675.42	80.80	0.11	0.01

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
16(20)	0.0763	20.639	7.235	4177.46	513.31	0.68	0.08
17(21)	0.0738	14.835	0.847	2158.17	7.04	0.35	0.00
18(22)	0.0711	11.183	-4.586	1226.50	206.28	0.20	0.03
Somma delle Masse Modali [kgm*g]				606873.95	608764.32		
Masse strutturali libere [kgm*g]				615853.65	615853.65		
Percentuale				98.54	98.85	98.54	98.85

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1(1)	0.3443	-520.714	2659003.55	6.14
2(2)	0.3008	276.726	750968.96	1.73
3(3)	0.2546	1806.792	32013791.95	73.90
4(4)	0.1562	-715.261	5017062.98	11.58
5(5)	0.1312	51.160	25667.70	0.06
6(6)	0.1234	421.671	1743683.50	4.02
7(7)	0.1193	-125.447	154327.90	0.36
8(8)	0.1071	4.900	235.42	0.00
9(10)	0.1026	61.275	36820.18	0.08
10(11)	0.0990	136.878	183733.44	0.42
11(12)	0.0960	-30.347	9031.55	0.02
12(15)	0.0887	78.116	59841.96	0.14
13(16)	0.0852	-1.447	20.55	0.00
14(18)	0.0810	-66.356	43179.39	0.10
15(19)	0.0769	48.782	23337.17	0.05
16(20)	0.0763	60.916	36390.08	0.08
17(21)	0.0738	3.038	90.50	0.00
18(22)	0.0711	-32.129	10123.09	0.02

Posizione masse 4

Numero di Frequenze calcolate =25, filtrate=17

N	T	Coeff. Partecipazione		Masse Modali		Percentuali	
	s			kgm*g			
		Dir=0°	Dir=90°	Dir=0°	Dir=90°	Dir=0°	Dir=90°
1(1)	0.3380	46.927	-230.246	21595.95	519880.20	3.51	84.42
2(2)	0.3010	226.411	45.173	502708.68	20011.20	81.63	3.25
3(3)	0.2563	-21.605	-21.687	4577.60	4612.50	0.74	0.75
4(4)	0.1465	-20.558	-2.149	4144.50	45.29	0.67	0.01
5(5)	0.1345	23.456	-73.894	5395.31	53547.61	0.88	8.69
6(6)	0.1270	66.327	22.280	43142.38	4868.15	7.01	0.79
7(7)	0.1148	-22.853	-4.114	5121.70	166.02	0.83	0.03
8(8)	0.1103	-0.038	-11.427	0.01	1280.59	0.00	0.21
9(9)	0.1026	15.940	-3.696	2491.60	133.98	0.40	0.02
10(10)	0.1006	-9.893	10.325	959.72	1045.52	0.16	0.17
11(11)	0.0963	-12.970	6.417	1649.64	403.77	0.27	0.07
12(12)	0.0947	-15.241	-6.524	2278.08	417.42	0.37	0.07
13(13)	0.0921	-7.405	-10.167	537.73	1013.70	0.09	0.16
14(16)	0.0839	30.512	6.491	9129.63	413.15	1.48	0.07
15(18)	0.0811	-0.142	-9.350	0.20	857.40	0.00	0.14
16(20)	0.0754	15.702	1.674	2417.84	27.49	0.39	0.00
17(25)	0.0643	8.166	1.209	653.98	14.35	0.11	0.00
Somma delle Masse Modali [kgm*g]				606804.54	608738.33		
Masse strutturali libere [kgm*g]				615853.65	615853.65		
Percentuale				98.53	98.84	98.53	98.84

Masse e coefficienti di partecipazione rotazionali:

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali

N	T(s)	Coeff. Partecipazione	Masse Modali	Percentuali
			kgm*g	
1(1)	0.3380	87.236	74630.05	0.18
2(2)	0.3010	120.141	141548.91	0.34
3(3)	0.2563	1857.191	33824680.46	81.19
4(4)	0.1465	745.595	5451635.17	13.09
5(5)	0.1345	-24.680	5973.19	0.01
6(6)	0.1270	351.686	1212917.92	2.91
7(7)	0.1148	-69.831	47820.75	0.11
8(8)	0.1103	56.414	31210.23	0.07
9(9)	0.1026	-52.213	26735.35	0.06
10(10)	0.1006	-104.986	108088.69	0.26
11(11)	0.0963	68.719	46309.92	0.11
12(12)	0.0947	48.010	22603.82	0.05
13(13)	0.0921	-184.666	334420.27	0.80
14(16)	0.0839	83.890	69013.82	0.17
15(18)	0.0811	-3.098	94.09	0.00
16(20)	0.0754	-48.720	23277.05	0.06
17(25)	0.0643	-22.831	5111.74	0.01

Risultati Analisi Dinamica - Massime tensioni sul terreno aste

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5
			MPa	MPa	MPa	MPa	MPa	MPa
9001	2	3	0.07(20)	0.07(20)	0.07(20)	0.07(20)	0.07(20)	0.08(20)
9001	6	7	0.10(1)	0.10(1)	0.09(1)	0.09(1)	0.09(20)	0.10(20)
9001	3	4	0.08(20)	0.08(20)	0.09(1)	0.09(1)	0.10(1)	0.11(1)
9001	4	5	0.11(1)	0.11(1)	0.11(1)	0.12(1)	0.12(1)	0.12(1)
9001	5	6	0.12(1)	0.12(1)	0.11(1)	0.11(1)	0.11(1)	0.10(1)
9002	10	11	0.11(5)	0.11(5)	0.10(5)	0.10(5)	0.10(5)	0.09(5)
9002	11	12	0.09(5)	0.09(5)	0.08(5)	0.08(5)	0.07(5)	0.07(1)
9003	17	18	0.12(1)	0.12(1)	0.12(1)	0.12(1)	0.12(1)	0.12(1)
9003	19	20	0.09(5)	0.08(5)	0.08(5)	0.07(5)	0.07(5)	0.07(1)
9003	18	19	0.12(1)	0.11(1)	0.10(1)	0.10(5)	0.09(5)	0.09(5)
9004	27	28	0.09(20)	0.09(20)	0.08(20)	0.08(20)	0.09(20)	0.10(20)
9005	15	13	0.06(1)	0.06(5)	0.06(5)	0.07(5)	0.07(5)	0.08(5)
9006	21	22	0.07(1)	0.06(5)	0.07(5)	0.07(5)	0.08(5)	0.09(5)
9007	24	25	0.07(1)	0.07(5)	0.07(5)	0.07(5)	0.08(5)	0.08(5)
9007	25	26	0.08(5)	0.09(5)	0.09(5)	0.09(5)	0.10(5)	0.12(1)
9008	29	30	0.09(20)	0.08(20)	0.08(20)	0.08(1)	0.08(1)	0.08(1)
9008	30	31	0.08(1)	0.08(1)	0.08(1)	0.08(20)	0.09(20)	0.11(20)
9009	2	15	0.07(20)	0.06(20)	0.06(1)	0.06(1)	0.06(1)	0.07(1)
9009	21	24	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.07(1)
9009	24	29	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.08(20)	0.09(20)
9009	15	21	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.07(1)
9010	13	22	0.08(5)	0.08(5)	0.09(5)	0.09(5)	0.09(5)	0.09(5)
9010	25	30	0.09(5)	0.08(5)	0.08(5)	0.08(5)	0.07(1)	0.08(1)
9010	22	25	0.09(5)	0.09(5)	0.09(5)	0.09(5)	0.09(5)	0.09(5)
9011	23	26	0.12(1)	0.12(1)	0.12(1)	0.12(1)	0.12(1)	0.12(1)
9011	26	31	0.12(1)	0.11(1)	0.11(1)	0.11(1)	0.11(20)	0.11(20)
9012	16	23	0.10(5)	0.10(5)	0.10(5)	0.11(5)	0.11(1)	0.12(1)
9012	8	13	0.06(1)	0.07(5)	0.07(5)	0.07(5)	0.08(5)	0.08(5)
9012	13	16	0.08(5)	0.08(5)	0.09(5)	0.09(5)	0.10(5)	0.10(5)
9012	2	8	0.07(20)	0.07(20)	0.06(1)	0.06(1)	0.06(1)	0.06(1)
9013	14	17	0.10(5)	0.10(5)	0.11(5)	0.11(5)	0.11(1)	0.12(1)
9013	9	14	0.09(1)	0.09(1)	0.09(5)	0.10(5)	0.10(5)	0.10(5)
9013	3	9	0.08(20)	0.08(1)	0.08(1)	0.08(1)	0.09(1)	0.09(1)
9014	17	23	0.12(1)	0.12(1)	0.12(1)	0.12(1)	0.12(1)	0.12(1)
9015	14	16	0.11(5)	0.10(5)	0.10(5)	0.10(5)	0.10(5)	0.10(5)
9016	9	13	0.09(1)	0.09(5)	0.09(5)	0.09(5)	0.08(5)	0.08(5)
9017	3	8	0.07(1)	0.07(1)	0.07(1)	0.07(5)	0.07(5)	0.07(5)

Asta	N.in.	N.fin.	0/5	1/5	2/5	3/5	4/5	5/5
9018	4	14	0.11(1)	0.10(1)	0.10(1)	0.10(5)	0.10(5)	0.10(5)
9019	10	18	0.11(5)	0.11(5)	0.11(5)	0.11(5)	0.11(5)	0.12(1)
9019	5	10	0.12(1)	0.12(1)	0.11(1)	0.11(1)	0.11(5)	0.11(5)
9020	11	19	0.09(5)	0.09(5)	0.09(5)	0.09(5)	0.09(5)	0.09(5)
9020	19	27	0.09(5)	0.09(5)	0.08(5)	0.08(1)	0.09(1)	0.09(20)
9020	6	11	0.10(1)	0.10(1)	0.09(5)	0.09(5)	0.09(5)	0.09(5)
9021	7	12	0.10(20)	0.09(20)	0.08(20)	0.08(1)	0.08(1)	0.07(1)
9021	20	28	0.07(1)	0.07(1)	0.08(1)	0.08(20)	0.09(20)	0.10(20)
9021	12	20	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.07(1)	0.07(1)

Risultati Analisi Dinamica - Spostamenti massimi - Nodi

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	cm	cm	cm	°	°	°
2	0.00(1)	0.00(1)	-0.33(20)	0.02(6)	0.02(22-I-1)	0.00(1)
3	0.00(1)	0.00(1)	-0.35(1)	0.02(6)	0.02(22-I-1)	0.00(1)
4	0.00(1)	0.00(1)	-0.51(1)	0.03(20)	0.02(1)	0.00(1)
5	0.00(1)	0.00(1)	-0.56(1)	0.02(20)	-0.01(20)	0.00(1)
6	0.00(1)	0.00(1)	-0.48(1)	0.03(20)	-0.01(22-II-1)	0.00(1)
7	0.00(1)	0.00(1)	-0.45(20)	0.03(20)	0.02(6)	0.00(1)
8	0.00(1)	0.00(1)	-0.30(5)	-0.01(23-I-4)	0.01(22-I-1)	0.00(1)
9	0.00(1)	0.00(1)	-0.42(1)	-0.01(23-I-4)	0.02(20)	0.00(1)
10	0.00(1)	0.00(1)	-0.53(5)	0.01(23-II-2)	-0.03(20)	0.00(1)
11	0.00(1)	0.00(1)	-0.44(5)	0.01(23-II-2)	-0.01(22-II-2)	0.00(1)
12	0.00(1)	0.00(1)	-0.35(1)	0.01(23-II-2)	0.02(6)	0.00(1)
13	0.00(1)	0.00(1)	-0.37(5)	-0.01(23-I-4)	0.02(1)	0.00(1)
14	0.00(1)	0.00(1)	-0.49(5)	-0.01(23-I-4)	0.01(20)	0.00(1)
15	0.00(1)	0.00(1)	-0.31(1)	-0.01(22-I-4)	-0.02(20)	0.00(1)
16	0.00(1)	0.00(1)	-0.47(5)	-0.01(20)	0.01(22-I-4)	0.00(1)
17	0.00(1)	0.00(1)	-0.56(1)	-0.02(20)	0.00(22-I-2)	0.00(1)
18	0.00(1)	0.00(1)	-0.55(1)	-0.03(20)	-0.01(20)	0.00(1)
19	0.00(1)	0.00(1)	-0.42(5)	0.01(25-II-2)	-0.02(20)	0.00(1)
20	0.00(1)	0.00(1)	-0.34(1)	-0.01(23-I-2)	0.02(6)	0.00(1)
21	0.00(1)	0.00(1)	-0.32(1)	-0.01(23-I-4)	-0.02(20)	0.00(1)
22	0.00(1)	0.00(1)	-0.43(5)	0.01(25-II-4)	0.03(20)	0.00(1)
23	0.00(1)	0.00(1)	-0.56(1)	0.01(25-II-4)	0.02(20)	0.00(1)
24	0.00(1)	0.00(1)	-0.33(1)	-0.01(23-I-4)	-0.02(20)	0.00(1)
25	0.00(1)	0.00(1)	-0.40(5)	0.01(23-II-4)	0.01(1)	0.00(1)
26	0.00(1)	0.00(1)	-0.55(1)	0.02(23-II-4)	0.04(20)	0.00(1)
27	0.00(1)	0.00(1)	-0.42(20)	-0.03(6)	-0.02(22-II-3)	0.00(1)
28	0.00(1)	0.00(1)	-0.44(20)	-0.03(20)	0.02(6)	0.00(1)
29	0.00(1)	0.00(1)	-0.41(20)	-0.03(20)	-0.02(22-II-3)	0.00(1)
30	0.00(1)	0.00(1)	-0.36(1)	-0.02(6)	0.01(22-I-3)	0.00(1)
31	0.00(1)	0.00(1)	-0.50(20)	-0.02(6)	0.04(20)	0.00(1)
35	0.17(22-I-2)	0.21(23-I-1)	-0.58(1)	0.06(23-II-1)	-0.05(22-II-3)	-0.03(6)
36	-0.20(22-II-3)	-0.25(23-II-4)	-0.58(1)	-0.06(23-I-1)	0.04(22-I-3)	0.04(20)
37	0.03(22-I-2)	0.04(23-I-4)	-0.50(5)	-0.04(23-I-4)	0.03(22-I-2)	0.02(6)
38	0.15(22-I-2)	0.19(23-I-4)	-0.71(5)	0.04(22-I-2)	-0.05(23-I-1)	0.01(22-I-1)
39	-0.17(22-II-3)	-0.27(23-II-4)	-0.61(5)	0.03(22-I-2)	-0.04(23-I-4)	0.01(23-II-4)
102	0.31(22-I-1)	0.35(23-I-4)	-0.36(20)	-0.04(23-I-4)	0.04(22-I-1)	-0.01(23-II-2)
103	0.31(22-I-1)	0.36(23-I-4)	-0.38(20)	0.04(6)	0.03(22-I-1)	-0.01(23-II-2)
104	0.31(22-I-1)	0.36(23-I-4)	-0.54(1)	-0.05(23-I-4)	-0.04(24-II-1)	-0.01(23-II-2)
105	0.31(22-I-1)	0.39(23-I-2)	-0.60(1)	-0.04(23-I-2)	-0.03(24-II-1)	-0.01(23-II-2)
106	0.31(22-I-1)	0.44(23-I-2)	-0.50(1)	-0.05(23-I-2)	-0.04(22-II-1)	-0.01(23-II-2)
107	0.31(22-I-1)	0.51(23-I-2)	-0.42(20)	-0.04(23-I-2)	-0.04(24-II-1)	-0.01(23-II-2)
108	0.29(22-I-1)	0.36(23-I-4)	-0.32(1)	-0.03(23-I-4)	0.02(23-II-4)	-0.01(23-II-2)
109	0.29(22-I-1)	0.36(23-I-4)	-0.44(1)	-0.05(23-I-4)	-0.04(22-II-1)	-0.01(23-II-2)

Nodo	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
110	0.28(22-I-2)	0.39(23-I-2)	-0.58(5)	-0.05(23-I-2)	0.02(22-I-1)	-0.01(23-II-2)
111	0.28(22-I-2)	0.44(23-I-2)	-0.49(5)	-0.03(23-I-2)	-0.04(22-II-1)	-0.01(23-II-2)
112	0.28(22-I-2)	0.51(23-I-2)	-0.36(1)	-0.04(23-I-2)	-0.03(22-II-2)	-0.01(23-II-2)
113	0.28(22-I-2)	0.36(23-I-4)	-0.42(5)	-0.04(23-I-4)	-0.04(22-II-2)	-0.01(23-II-2)
114	0.28(22-I-2)	0.36(23-I-4)	-0.54(5)	0.03(23-II-4)	0.03(22-I-2)	-0.01(23-II-2)
115	0.28(22-I-2)	0.35(23-I-4)	-0.31(1)	-0.03(23-I-4)	0.06(5)	-0.01(23-II-2)
116	0.28(22-I-2)	0.36(23-I-4)	-0.50(5)	-0.04(23-I-4)	0.03(22-I-3)	-0.01(23-II-2)
117	0.27(22-I-3)	0.38(23-I-1)	-0.59(1)	0.07(23-II-2)	-0.03(22-II-3)	-0.01(23-II-2)
118	0.27(22-I-3)	0.39(23-I-2)	-0.56(1)	0.05(23-II-2)	-0.02(22-II-3)	-0.01(23-II-2)
119	0.27(22-I-3)	0.44(23-I-2)	-0.46(5)	0.03(23-II-2)	-0.04(22-II-3)	-0.01(23-II-2)
120	0.27(22-I-3)	0.51(23-I-2)	-0.35(1)	-0.04(23-I-2)	-0.05(22-II-3)	-0.01(23-II-2)
121	0.28(22-I-3)	0.35(23-I-4)	-0.32(1)	-0.02(23-I-4)	0.08(5)	-0.01(23-II-2)
122	0.28(22-I-3)	0.36(23-I-4)	-0.45(5)	-0.03(23-I-4)	-0.05(22-II-3)	-0.01(23-II-2)
123	0.28(22-I-3)	0.36(23-I-4)	-0.59(1)	0.03(23-II-3)	-0.04(23-I-2)	-0.01(23-II-2)
124	0.29(22-I-3)	0.35(23-I-4)	-0.34(1)	-0.02(23-I-4)	0.06(5)	-0.01(23-II-2)
125	0.29(22-I-3)	0.36(23-I-4)	-0.45(5)	0.03(23-II-4)	-0.02(24-II-3)	-0.01(23-II-2)
126	0.29(22-I-3)	0.36(23-I-4)	-0.56(1)	0.03(23-II-4)	-0.05(22-II-3)	-0.01(23-II-2)
127	0.29(22-I-3)	0.45(23-I-2)	-0.43(20)	0.05(23-II-2)	0.04(22-I-3)	-0.01(23-II-2)
128	0.29(22-I-3)	0.51(23-I-2)	-0.40(20)	0.04(23-II-2)	0.04(22-I-3)	-0.01(23-II-2)
129	0.30(22-I-3)	0.35(23-I-4)	-0.41(20)	0.03(23-II-4)	0.05(22-I-3)	-0.01(23-II-2)
130	0.30(22-I-3)	0.36(23-I-4)	-0.38(1)	0.05(23-II-4)	-0.04(22-II-3)	-0.01(23-II-2)
131	0.30(22-I-3)	0.36(23-I-4)	-0.45(20)	0.03(23-II-4)	-0.05(22-II-3)	-0.01(23-II-2)
204	0.63(22-I-1)	0.67(23-I-4)	-0.57(1)	0.05(6)	0.04(22-I-1)	0.02(23-I-2)
205	0.63(22-I-1)	0.78(23-I-2)	-0.61(1)	0.04(6)	-0.02(22-II-1)	0.02(23-I-2)
206	0.63(22-I-1)	0.92(23-I-2)	-0.52(1)	-0.04(23-I-2)	-0.04(22-II-1)	0.02(23-I-2)
209	0.59(22-I-1)	0.66(23-I-4)	-0.47(1)	0.03(20)	0.03(22-I-3)	0.02(23-I-2)
210	0.56(22-I-1)	0.77(23-I-2)	-0.60(5)	-0.04(23-I-2)	-0.04(20)	0.02(23-I-2)
211	0.56(22-I-1)	0.92(23-I-2)	-0.51(5)	-0.02(23-I-2)	-0.04(22-II-1)	0.02(23-I-2)
213	0.55(22-I-2)	0.65(23-I-4)	-0.43(1)	-0.02(23-I-4)	-0.04(6)	0.02(23-I-2)
214	0.55(22-I-2)	0.67(23-I-4)	-0.55(5)	0.03(23-II-4)	0.04(22-I-2)	0.02(23-I-2)
216	0.53(22-I-2)	0.66(23-I-4)	-0.51(1)	-0.03(23-I-4)	0.03(22-I-2)	0.02(23-I-2)
217	0.53(22-I-3)	0.72(23-I-1)	-0.61(1)	0.04(23-II-2)	-0.02(22-II-3)	0.02(23-I-2)
218	0.53(22-I-3)	0.77(23-I-2)	-0.58(1)	0.04(23-II-2)	-0.02(20)	0.02(23-I-2)
219	0.53(22-I-3)	0.92(23-I-2)	-0.47(5)	0.05(23-II-2)	-0.03(22-II-3)	0.02(23-I-2)
222	0.54(22-I-3)	0.65(23-I-4)	-0.47(5)	0.03(25-II-4)	0.06(22-I-3)	0.02(23-I-2)
223	0.55(22-I-3)	0.68(23-I-4)	-0.59(1)	0.03(23-II-4)	-0.04(22-II-3)	0.02(23-I-2)
225	0.56(22-I-3)	0.65(23-I-4)	-0.45(5)	0.03(23-II-4)	0.05(22-I-3)	0.02(23-I-2)
226	0.56(22-I-3)	0.68(23-I-4)	-0.57(1)	0.03(23-II-4)	-0.04(22-II-3)	0.02(23-I-2)

Risultati Analisi Dinamica - Reazioni massime - Nodi

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Nodo	Rx	Ry	Rz	Mx	My	Mz
	kN	kN	kN	kN*m	kN*m	kN*m
2	99.56(22-II-1)	29.02(23-II-4)	0	0	0	-294.59(6)
3	101.72(22-II-1)	20.75(23-II-4)	0	0	0	-204.61(20)
4	76.66(22-II-1)	15.76(23-II-4)	0	0	0	-105.31(20)
5	-42.92(22-I-1)	13.29(25-II-2)	0	0	0	-95.68(6)
6	-46.84(22-I-1)	14.36(23-II-2)	0	0	0	-100.55(6)
7	-54.63(22-I-1)	26.39(23-II-2)	0	0	0	11.90(23-I-2)
8	27.36(22-II-1)	26.99(23-II-4)	0	0	0	99.75(20)
9	34.75(22-II-4)	38.63(23-II-1)	0	0	0	-103.68(20)
10	-12.52(22-I-2)	43.80(25-II-1)	0	0	0	-100.21(20)
11	-43.41(22-I-2)	19.32(23-II-2)	0	0	0	-8.84(23-I-2)
12	-15.76(22-I-1)	-75.56(23-I-2)	0	0	0	99.48(20)
13	34.94(22-II-3)	45.92(23-II-4)	0	0	0	100.62(20)
14	82.33(22-II-3)	84.20(23-II-1)	0	0	0	-27.68(20)
15	16.96(22-II-2)	50.75(23-II-4)	0	0	0	-100.44(6)
16	26.24(22-II-3)	28.41(23-II-4)	0	0	0	101.41(20)
17	-69.43(23-II-3)	-38.67(23-I-3)	0	0	0	-87.93(20)
18	-47.39(22-I-3)	-16.33(23-I-2)	0	0	0	99.61(6)

Nodo	Rx	Ry	Rz	Mx	My	Mz
19	-45.13(22-I-2)	-20.42(23-I-2)	0	0	0	-9.03(23-I-2)
20	-12.51(22-I-4)	77.27(23-II-2)	0	0	0	97.63(6)
21	20.55(22-II-3)	-53.98(23-I-4)	0	0	0	-99.83(6)
22	-12.98(22-I-3)	-47.80(23-I-4)	0	0	0	100.10(6)
23	71.26(22-II-3)	-61.29(23-I-4)	0	0	0	92.25(20)
24	17.75(22-II-3)	-52.99(23-I-4)	0	0	0	-97.63(20)
25	12.11(22-II-3)	-50.92(23-I-4)	0	0	0	-9.40(23-I-2)
26	-10.08(22-I-3)	-58.33(23-I-1)	0	0	0	96.88(20)
27	-42.71(20)	-25.95(23-I-2)	0	0	0	-11.54(23-I-2)
28	-36.69(22-I-3)	-30.49(23-I-2)	0	0	0	194.73(20)
29	-43.98(6)	-18.82(23-I-4)	0	0	0	-8.65(22-I-3)
30	-70.92(22-I-3)	-19.28(23-I-4)	0	0	0	96.58(6)
31	-40.55(22-I-3)	-29.59(23-I-1)	0	0	0	199.18(20)

Risultati Analisi Dinamica - Spostamenti massimi - Impalcati

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	cm	cm	cm	°	°	°
1	0.27(22-I-2)	0.35(23-I-4)	-0.31(1-1)	0.00(1-1)	0.00(1-1)	-0.01(23-I-2)
2	0.54(22-I-2)	0.69(23-II-1)	-0.37(1-1)	0.00(1-1)	0.00(1-1)	0.02(23-II-2)

Risultati Analisi Dinamica - Spostamenti massimi - Impalcati (SLD)

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

la tripletta (Cb [-SubC-Cbm]) indica la Combinazione - SottoCombinazione sismica - Posizione Masse, nel caso non sismico mancano SubC-Cbm

Piano	Trasl. X	Trasl. Y	Trasl. Z	Rotaz. X	Rotaz. Y	Rotaz. Z
	cm	cm	cm	°	°	°
1	0.29(53-I-2)	0.39(54-I-4)	-0.23(26-1)	0.00(26-1)	0.00(26-1)	-0.01(54-I-2)
2	0.60(53-I-2)	0.76(54-II-1)	-0.26(26-1)	0.00(26-1)	0.00(26-1)	0.02(54-II-2)

Risultati Analisi Dinamica - Sollecitazioni massime - Inviluppi - Travi

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	N.fin.	kN	kN	kN	kN*m	kN*m	kN*m
101	129	0	0.37(20)	-99.31(1)	3.96(20)	100.34(22-II-3)	27.33(20)
	130	0	0.37(20)	95.54(5)	3.96(20)	101.38(22-I-3)	25.50(6)
101	130	0	0.20(23-I-4)	-111.48(1)	2.77(23-I-4)	122.14(1)	25.96(20)
	131	0	0.20(23-I-4)	94.66(5)	2.77(23-I-4)	99.74(22-I-3)	26.83(6)
102	124	0	0.15(23-II-4)	-103.27(1)	1.66(23-II-4)	57.58(22-II-3)	26.21(20)
	125	0	0.15(23-II-4)	120.61(5)	1.66(23-II-4)	105.70(5)	26.52(6)
102	125	0	-0.09(22-I-1)	-136.19(1)	-1.22(22-I-1)	163.80(5)	26.37(6)
	126	0	-0.09(22-I-1)	103.63(1)	-1.22(22-I-1)	84.52(22-I-3)	26.33(20)
103	121	0	0.10(25-II-4)	-118.75(1)	1.25(25-II-4)	74.23(1)	26.21(20)
	122	0	0.10(25-II-4)	114.60(5)	1.25(25-II-4)	81.34(5)	26.48(21)
104	115	0	-0.11(23-I-2)	-87.81(1)	-1.40(23-I-2)	56.65(22-II-2)	26.23(6)
	113	0	-0.11(23-I-2)	81.94(5)	-1.40(23-I-2)	74.49(22-I-2)	26.64(20)
105	102	0	-2.96(6)	-45.66(20)	-7.28(6)	-50.20(22-I-4)	23.26(20)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	108	0	-2.96(6)	51.11(22-I-2)	-7.28(6)	-60.77(6)	30.08(6)
105	108	0	1.41(6)	-75.78(1)	5.74(6)	64.08(23-II-4)	28.65(6)
	113	0	1.41(6)	45.47(23-I-4)	5.74(6)	-56.49(20)	25.14(20)
105	113	0	1.15(5)	-71.84(22-II-3)	4.76(5)	98.93(22-II-3)	25.77(20)
	116	0	1.15(5)	52.78(22-I-3)	4.76(5)	-67.11(20)	28.07(6)
105	116	0	-0.30(23-I-2)	-93.01(1)	-3.21(23-I-2)	93.87(22-II-3)	26.79(6)
	123	0	-0.30(23-I-2)	82.86(5)	-3.21(23-I-2)	69.19(22-I-3)	25.93(20)
106	103	0	1.07(25-II-4)	-71.37(20)	4.37(25-II-4)	74.36(22-II-3)	25.05(20)
	109	0	1.07(25-II-4)	47.14(22-I-3)	4.37(25-II-4)	-71.17(20)	27.71(21)
106	109	0	1.65(23-I-4)	-71.36(22-II-3)	6.79(23-I-4)	89.27(22-II-3)	27.95(20)
	114	0	1.65(23-I-4)	43.21(22-I-3)	6.79(23-I-4)	-58.87(20)	25.89(6)
106	114	0	-0.51(23-I-2)	-102.45(1)	-5.38(23-I-2)	106.28(23-II-1)	25.78(6)
	117	0	-0.51(23-I-2)	75.41(5)	-5.38(23-I-2)	79.08(23-I-1)	27.15(20)
107	102	0	0.21(20)	-56.26(1)	2.08(20)	78.07(22-II-1)	26.88(20)
	103	0	0.21(20)	50.67(5)	2.08(20)	56.00(22-I-1)	25.85(6)
107	103	0	-0.77(20)	-78.38(1)	-6.21(20)	119.19(22-II-1)	24.78(6)
	104	0	-0.77(20)	54.66(22-I-1)	-6.21(20)	-80.96(22-II-1)	28.13(20)
107	104	0	0.14(20)	-107.04(1)	1.76(20)	138.80(22-II-1)	26.74(20)
	105	0	0.14(20)	101.25(5)	1.76(20)	121.00(22-I-1)	26.11(6)
107	105	0	-0.30(23-I-2)	-73.77(22-II-1)	-1.80(23-I-2)	92.84(22-II-1)	26.57(6)
	106	0	-0.30(23-I-2)	85.99(22-I-1)	-1.80(23-I-2)	116.32(22-I-1)	26.26(20)
107	106	0	0.21(20)	-54.46(20)	2.20(20)	68.24(22-II-1)	26.90(20)
	107	0	0.21(20)	56.68(5)	2.20(20)	94.30(22-I-1)	25.86(6)
108	107	0	-1.35(22-I-1)	-69.12(1)	-7.23(22-I-1)	68.47(23-II-2)	27.59(6)
	112	0	-1.35(22-I-1)	84.49(23-I-2)	-7.23(22-I-1)	108.53(23-I-2)	25.91(20)
108	112	0	-0.48(20)	-94.81(1)	-3.99(20)	107.15(23-II-2)	25.30(6)
	120	0	-0.48(20)	89.93(5)	-3.99(20)	121.81(23-I-2)	27.47(20)
108	120	0	0.74(5)	-95.44(1)	4.78(5)	104.93(23-II-2)	27.41(20)
	128	0	0.74(5)	72.65(23-I-2)	4.78(5)	78.47(23-I-2)	26.11(6)
109	106	0	-0.29(25-I-2)	-89.85(1)	-1.53(25-I-2)	86.23(23-II-2)	26.28(21)
	111	0	-0.29(25-I-2)	128.37(1)	-1.53(25-I-2)	119.92(23-I-2)	26.43(6)
109	111	0	0.21(25-II-2)	-142.21(1)	1.77(25-II-2)	103.98(23-II-2)	26.48(20)
	119	0	0.21(25-II-2)	138.55(5)	1.77(25-II-2)	121.01(23-I-2)	26.23(21)
110	119	0	-0.51(6)	-92.95(1)	-3.21(6)	75.57(23-II-2)	25.75(20)
	127	0	-0.51(6)	69.17(5)	-3.21(6)	65.07(23-I-2)	27.38(6)
111	102	0	0.93(22-II-1)	-65.63(1)	8.08(22-II-1)	65.45(23-II-4)	27.17(20)
	115	0	0.93(22-II-1)	86.51(5)	8.08(22-II-1)	86.55(23-I-4)	26.73(6)
111	115	0	0.53(5)	-50.10(1)	3.70(5)	67.02(23-II-4)	27.10(20)
	121	0	0.53(5)	54.53(23-I-4)	3.70(5)	75.19(23-I-4)	26.30(6)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
111	121	0	-1.36(5)	-57.80(23-II-4)	-4.30(5)	61.32(23-II-4)	26.17(6)
	124	0	-1.36(5)	61.85(23-I-4)	-4.30(5)	69.48(23-I-4)	27.76(20)
111	124	0	-1.06(22-II-3)	-61.63(1)	-7.68(22-II-3)	64.40(23-II-4)	26.65(6)
	129	0	-1.06(22-II-3)	41.32(23-I-4)	-7.68(22-II-3)	-59.48(6)	27.34(20)
112	113	0	-0.51(5)	-64.49(1)	-4.10(5)	81.49(23-II-4)	26.64(6)
	122	0	-0.51(5)	92.33(5)	-4.10(5)	101.28(23-I-4)	26.75(20)
112	122	0	3.01(5)	-99.53(23-II-4)	9.52(5)	96.43(23-II-4)	28.69(20)
	125	0	3.01(5)	114.48(23-I-4)	9.52(5)	119.91(23-I-4)	26.94(6)
112	125	0	-1.13(21)	-39.83(1)	-3.48(21)	35.21(23-II-4)	50.49(6)
	130	0	-1.13(21)	38.59(5)	-3.48(21)	37.43(23-I-4)	55.16(21)
113	123	0	-12.53(23-II-4)	-116.76(23-II-1)	-13.90(23-II-4)	-98.96(23-I-2)	27.00(6)
	126	0	-12.53(23-II-4)	157.87(23-I-1)	-13.90(23-II-4)	122.27(23-I-1)	30.15(20)
113	126	0	-0.62(6)	-48.05(23-II-1)	-4.54(6)	63.97(23-II-1)	25.73(20)
	131	0	-0.62(6)	56.72(23-I-1)	-4.54(6)	73.84(23-I-1)	27.72(6)
114	116	0	0.38(23-I-4)	-33.28(23-I-4)	1.40(23-I-4)	51.51(23-I-4)	26.54(20)
	114	0	0.38(23-I-4)	34.05(23-II-4)	1.40(23-I-4)	45.08(23-II-4)	26.30(6)
115	113	0	-1.04(23-I-2)	-46.77(5)	-1.68(23-I-2)	40.00(23-I-4)	52.63(6)
	109	0	-1.04(23-I-2)	28.96(23-II-4)	-1.68(23-I-2)	23.82(23-II-4)	53.12(20)
116	108	0	2.37(20)	-61.45(22-II-1)	8.39(20)	83.15(22-II-1)	29.95(20)
	103	0	2.37(20)	-41.27(22-II-1)	8.39(20)	-72.46(22-II-1)	22.77(6)
117	117	0	5.71(25-I-4)	-116.40(22-II-3)	9.11(25-I-4)	110.41(22-II-3)	26.72(20)
	118	0	5.71(25-I-4)	103.59(22-I-3)	9.11(25-I-4)	97.26(22-I-3)	26.32(21)
117	118	0	-0.41(23-II-4)	-69.01(22-II-3)	-2.83(23-II-4)	80.01(22-II-3)	26.38(6)
	119	0	-0.41(23-II-4)	82.99(22-I-3)	-2.83(23-II-4)	117.29(22-I-3)	26.61(20)
117	119	0	-0.56(23-I-2)	-41.30(1)	-2.46(23-I-2)	36.19(5)	53.24(6)
	120	0	-0.56(23-I-2)	38.88(5)	-2.46(23-I-2)	33.62(22-I-3)	52.93(20)
118	127	0	-0.19(22-I-2)	-62.14(20)	-1.81(22-I-2)	59.89(22-II-3)	26.32(6)
	128	0	-0.19(22-I-2)	53.77(5)	-1.81(22-I-2)	-77.61(6)	26.43(20)
119	110	0	-0.44(23-II-4)	-38.88(22-II-1)	-3.03(23-II-4)	50.80(24-II-1)	26.36(6)
	111	0	-0.44(23-II-4)	51.33(22-I-1)	-3.03(23-II-4)	81.10(22-I-1)	26.44(20)
119	111	0	0.26(23-II-2)	-42.48(1)	2.74(23-II-2)	61.44(22-II-1)	26.86(20)
	112	0	0.26(23-II-2)	37.08(22-I-1)	2.74(23-II-2)	49.50(22-I-1)	26.12(6)
120	105	0	0.38(22-II-1)	-78.73(23-II-2)	2.08(22-II-1)	78.94(23-II-2)	25.86(20)
	110	0	0.38(22-II-1)	110.71(5)	2.08(22-II-1)	127.24(23-I-2)	26.89(6)
120	110	0	0.19(6)	-118.22(1)	1.56(6)	129.52(23-II-2)	26.79(6)
	118	0	0.19(6)	90.58(5)	1.56(6)	111.10(23-I-2)	25.97(20)
121	104	0	0.38(22-II-1)	-94.96(1)	3.63(22-II-1)	86.37(23-II-	27.03(20)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
						4)	
	114	0	0.38(22-II-1)	100.42(5)	3.63(22-II-1)	91.30(23-I-4)	25.98(6)
122	36	-35.98(5)	11.80(23-II-1)	-93.64(23-I-2)	7.22(22-II-4)	110.38(23-I-2)	23.63(20)
	35	-35.98(5)	11.80(23-II-1)	89.43(23-II-2)	7.22(22-II-4)	103.09(23-II-2)	-18.62(23-II-4)
123	36	100.61(22-II-3)	-5.37(22-II-3)	-38.73(22-I-3)	-6.18(6)	0	-12.95(22-II-3)
	39	100.61(22-II-3)	-5.37(22-II-3)	25.89(22-II-3)	-6.18(6)	-41.59(22-I-3)	17.63(6)
123	39	96.79(22-II-3)	-4.75(20)	-28.74(5)	3.53(6)	-42.36(22-I-3)	18.72(6)
	116	120.01(22-II-3)	-4.75(20)	41.67(1)	3.53(6)	0	32.58(20)
201	225	0	-0.10(23-I-2)	-86.65(1)	-1.39(23-I-2)	69.03(22-II-3)	26.27(6)
	226	0	-0.10(23-I-2)	69.11(5)	-1.39(23-I-2)	59.67(22-I-3)	26.48(20)
202	213	0	1.00(23-II-4)	-80.89(20)	4.12(23-II-4)	79.42(22-II-3)	26.05(20)
	216	0	1.00(23-II-4)	51.67(22-I-3)	4.12(23-II-4)	-88.23(6)	26.82(6)
202	216	0	0.41(6)	-102.46(1)	4.40(6)	97.55(5)	27.45(6)
	223	0	0.41(6)	82.80(5)	4.40(6)	54.67(22-I-3)	25.41(20)
203	213	0	0.54(23-II-2)	-64.47(1)	4.31(23-II-2)	68.69(23-II-4)	26.32(20)
	222	0	0.54(23-II-2)	69.14(5)	4.31(23-II-2)	73.43(23-I-4)	26.82(6)
203	222	0	1.61(22-II-2)	-74.53(1)	7.35(22-II-2)	74.86(23-II-4)	29.06(20)
	225	0	1.61(22-II-2)	70.34(23-I-4)	7.35(22-II-2)	72.41(23-I-4)	24.79(6)
204	223	0	-5.59(23-II-4)	-87.14(23-II-1)	-6.20(23-II-4)	56.71(23-II-2)	29.09(6)
	226	0	-5.59(23-II-4)	95.45(23-I-1)	-6.20(23-II-4)	80.61(23-I-1)	25.11(20)
205	223	0	-1.24(23-I-2)	-63.80(23-I-2)	-4.52(23-I-2)	79.21(23-I-2)	27.18(6)
	217	0	-1.24(23-I-2)	56.95(23-II-2)	-4.52(23-I-2)	68.86(23-II-2)	25.80(20)
206	217	0	6.02(22-II-2)	-74.55(22-II-3)	7.70(22-II-2)	54.58(22-II-3)	23.52(20)
	218	0	6.02(22-II-2)	59.13(22-I-3)	7.70(22-II-2)	-73.19(6)	31.67(6)
206	218	0	0.29(23-II-2)	-54.51(1)	2.00(23-II-2)	64.39(22-II-3)	26.40(20)
	219	0	0.29(23-II-2)	59.76(22-I-3)	2.00(23-II-2)	82.31(22-I-3)	26.37(6)
207	204	0	-0.16(6)	-89.22(1)	-2.11(6)	112.49(22-II-1)	25.99(20)
	205	0	-0.16(6)	78.77(5)	-2.11(6)	90.70(22-I-1)	26.82(6)
207	205	0	0.18(23-II-2)	-57.26(22-II-1)	1.04(23-II-2)	68.32(22-II-1)	26.39(20)
	206	0	0.18(23-II-2)	63.39(22-I-1)	1.04(23-II-2)	90.49(22-I-1)	26.39(6)
208	209	0	1.02(22-I-1)	-80.59(20)	4.22(22-I-1)	84.27(22-II-3)	25.00(20)
	214	0	1.02(22-I-1)	39.17(22-I-3)	4.22(22-I-1)	-82.32(20)	28.00(6)
208	214	0	0.45(6)	-109.45(1)	4.81(6)	101.93(5)	27.55(6)
	217	0	0.45(6)	79.54(5)	4.81(6)	58.46(23-I-1)	25.54(20)
209	204	0	-1.36(22-I-1)	-35.24(22-I-1)	-5.37(22-I-1)	-56.79(20)	28.34(6)
	209	0	-1.36(22-I-1)	61.18(1)	-5.37(22-I-1)	45.74(22-II-1)	25.15(20)
209	209	0	0.85(23-II-2)	-36.89(5)	3.11(23-II-2)	-67.69(6)	26.80(20)
	213	0	0.85(23-II-2)	58.58(20)	3.11(23-II-2)	42.25(22-II-1)	26.26(6)
210	214	0	0.82(22-II-1)	-24.39(5)	1.32(22-II-1)	-33.48(6)	52.91(20)
	216	0	0.82(22-II-1)	29.48(20)	1.32(22-II-1)	19.27(23-I-4)	52.88(6)
211	204	0	0.40(22-II-1)	-98.09(1)	3.85(22-II-1)	73.18(1)	27.18(20)
	214	0	0.40(22-II-1)	96.00(5)	3.85(22-II-1)	76.43(5)	25.91(6)
212	205	0	-0.63(21)	-90.78(1)	-3.42(21)	54.08(23-II-	25.17(6)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
						2)	
	210	0	-0.63(21)	120.65(5)	-3.42(21)	106.31(23-I-2)	27.54(21)
212	210	0	0.33(6)	-136.18(1)	2.73(6)	103.71(23-II-2)	27.12(6)
	218	0	0.33(6)	94.99(5)	2.73(6)	82.85(23-I-2)	25.61(20)
213	206	0	0.46(23-II-2)	-65.07(20)	2.10(23-II-2)	44.77(23-II-2)	26.86(20)
	211	0	0.46(23-II-2)	89.45(5)	2.10(23-II-2)	80.59(5)	26.17(6)
213	211	0	-0.27(22-I-1)	-106.62(1)	-2.24(22-I-1)	75.63(23-II-2)	26.21(6)
	219	0	-0.27(22-I-1)	89.42(5)	-2.24(22-I-1)	78.48(23-I-2)	26.71(20)
214	210	0	0.40(23-I-2)	-39.99(20)	2.76(23-I-2)	38.83(22-II-1)	26.14(20)
	211	0	0.40(23-I-2)	45.44(22-I-1)	2.76(23-I-2)	73.89(22-I-1)	26.60(6)
8000	37	-110.78(22-II-3)	-2.71(23-II-4)	-51.01(1)	2.93(20)	0	25.11(6)
	38	-85.53(22-II-3)	-2.71(23-II-4)	31.75(5)	2.93(20)	-54.43(22-I-3)	20.90(20)
8000	38	-86.99(22-II-3)	-6.24(22-II-1)	21.01(22-I-3)	-6.74(20)	-56.54(22-I-3)	19.97(20)
	35	-86.99(22-II-3)	-6.24(22-II-1)	45.00(1)	-6.74(20)	0	19.43(20)

Risultati Analisi Dinamica - Sollecitazioni massime - Inviluppi - Pilastri

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	N.fin.	kN	kN	kN	kN*m	kN*m	kN*m
2	2	-226.24(20)	-99.56(22-II-1)	-29.02(23-II-4)	-4.39(23-II-2)	-110.42(6)	-345.44(22-II-1)
	102	-172.74(20)	-99.56(22-II-1)	-29.02(23-II-4)	-4.39(23-II-2)	-60.97(23-II-4)	91.76(22-II-1)
3	3	-210.56(1)	-101.72(22-II-1)	-20.75(23-II-4)	-2.53(23-II-2)	-76.20(6)	-265.03(22-II-1)
	103	-176.32(1)	-101.72(22-II-1)	-20.75(23-II-4)	-2.53(23-II-2)	-44.95(23-II-4)	181.53(22-II-1)
4	4	-508.33(1)	-76.66(22-II-1)	-15.76(23-II-4)	-2.53(23-II-2)	-61.30(21)	-246.24(22-II-1)
	104	-474.08(1)	-76.66(22-II-1)	-15.76(23-II-4)	-2.53(23-II-2)	-39.14(20)	158.04(20)
4	104	-236.93(1)	-58.02(22-II-1)	-26.56(23-II-4)	4.94(23-I-2)	-61.41(6)	105.73(6)
	204	-207.68(1)	-58.02(22-II-1)	-26.56(23-II-4)	4.94(23-I-2)	-54.03(23-II-4)	118.14(22-II-1)
5	5	-494.34(1)	42.92(22-I-1)	-13.29(25-II-2)	-1.70(23-II-2)	-49.84(20)	116.62(22-I-1)
	105	-468.66(1)	42.92(22-I-1)	-13.29(25-II-2)	-1.70(23-II-2)	-27.19(23-II-2)	-72.14(22-I-1)
5	105	-237.61(1)	56.08(22-I-1)	-21.84(23-II-2)	3.33(23-I-2)	-42.67(6)	94.63(22-I-1)
	205	-215.67(1)	56.08(22-I-1)	-21.84(23-II-2)	3.33(23-I-2)	-42.91(23-II-2)	-115.78(22-I-1)
6	6	-367.86(1)	46.84(22-I-1)	-14.36(23-II-2)	-1.70(23-II-2)	-53.50(20)	121.47(22-I-1)
	106	-342.18(1)	46.84(22-I-1)	-14.36(23-II-2)	-1.70(23-II-2)	-28.96(23-II-2)	-84.44(22-I-1)
6	106	-130.13(1)	55.24(22-I-1)	-26.99(23-II-2)	3.33(23-I-2)	48.28(23-II-2)	101.85(22-I-1)
	206	-108.20(1)	55.24(22-I-1)	-26.99(23-II-2)	3.33(23-I-2)	-52.95(23-II-2)	-105.43(22-I-1)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
7	7	-152.72(1)	54.63(22-I-1)	-26.39(23-II-2)	-2.53(23-II-2)	-78.51(20)	167.03(22-I-1)
	107	-118.48(1)	54.63(22-I-1)	-26.39(23-II-2)	-2.53(23-II-2)	-56.74(23-II-2)	80.55(6)
8	8	-183.38(5)	-28.94(22-II-1)	-13.96(22-II-3)	-1.70(23-II-2)	-30.53(6)	-78.35(22-II-1)
	108	-157.69(5)	-28.94(22-II-1)	-13.96(22-II-3)	-1.70(23-II-2)	-38.32(20)	48.69(22-II-1)
9	9	-333.07(5)	-8.70(23-I-4)	-47.54(23-II-1)	-2.11(23-II-2)	131.51(23-II-1)	-26.72(23-I-4)
	109	-303.10(5)	-8.70(23-I-4)	-47.54(23-II-1)	-2.11(23-II-2)	-124.69(20)	50.14(6)
9	109	-183.96(1)	-17.90(22-II-1)	-30.54(22-II-3)	4.13(23-I-2)	-75.31(6)	25.91(6)
	209	-158.36(1)	-17.90(22-II-1)	-30.54(22-II-3)	4.13(23-I-2)	-52.31(22-II-3)	56.63(20)
10	10	-584.33(1)	12.52(22-I-2)	-43.80(25-II-1)	-1.70(23-II-2)	-125.45(23-I-2)	50.29(20)
	110	-558.65(1)	12.52(22-I-2)	-43.80(25-II-1)	-1.70(23-II-2)	-81.90(23-II-1)	-22.76(22-I-2)
10	110	-304.55(1)	-16.32(24-II-1)	-66.06(23-II-2)	3.33(23-I-2)	112.85(23-II-2)	42.84(6)
	210	-282.61(1)	-16.32(24-II-1)	-66.06(23-II-2)	3.33(23-I-2)	-135.11(23-II-2)	31.93(24-II-1)
11	11	-634.66(5)	43.41(22-I-2)	-19.32(23-II-2)	-1.70(23-II-2)	-45.01(23-I-2)	112.91(22-I-2)
	111	-608.98(5)	43.41(22-I-2)	-19.32(23-II-2)	-1.70(23-II-2)	-41.05(23-II-2)	-78.03(22-I-2)
11	111	-258.65(5)	39.47(22-I-1)	-36.26(23-II-2)	3.33(23-I-2)	65.60(23-II-2)	75.26(22-I-1)
	211	-236.72(5)	39.47(22-I-1)	-36.26(23-II-2)	3.33(23-I-2)	-70.39(23-II-2)	-73.02(22-I-1)
12	12	-237.40(5)	15.76(22-I-1)	75.56(23-I-2)	-1.70(23-II-2)	-187.14(23-I-2)	34.39(22-I-1)
	112	-211.72(5)	15.76(22-I-1)	75.56(23-I-2)	-1.70(23-II-2)	144.56(23-I-2)	41.70(6)
13	13	-535.87(1)	14.89(23-II-4)	-50.36(23-II-4)	-2.11(23-II-2)	139.45(23-II-4)	32.11(23-II-4)
	113	-505.91(1)	14.89(23-II-4)	-50.36(23-II-4)	-2.11(23-II-2)	-124.13(21)	47.77(6)
13	113	-227.13(20)	20.17(23-II-4)	-39.80(22-II-3)	4.13(23-I-2)	-84.90(6)	48.07(20)
	213	-201.53(20)	20.17(23-II-4)	-39.80(22-II-3)	4.13(23-I-2)	-78.91(23-II-4)	-37.37(23-II-4)
14	14	-617.41(5)	-14.78(23-I-4)	-111.32(22-II-3)	18.97(6)	127.79(23-II-1)	-32.75(23-I-4)
	37	-612.73(5)	-14.78(23-I-4)	-111.32(22-II-3)	18.97(6)	-41.14(6)	21.00(6)
14	37	-523.57(5)	-13.56(23-I-4)	-28.21(23-II-1)	-4.15(6)	46.22(23-II-1)	30.09(6)
	114	-502.57(5)	-13.56(23-I-4)	-28.21(23-II-1)	-4.15(6)	-80.66(20)	47.34(20)
14	114	-267.98(5)	-21.95(23-I-4)	-40.51(22-II-3)	3.33(23-I-2)	69.98(22-II-3)	-40.20(23-I-4)
	214	-246.05(5)	-21.95(23-I-4)	-40.51(22-II-3)	3.33(23-I-2)	-118.84(20)	42.10(23-I-4)
15	15	-246.96(1)	-16.96(22-II-2)	-50.75(23-II-4)	-1.70(23-II-2)	-127.72(23-I-4)	44.89(6)
	115	-221.28(1)	-16.96(22-II-2)	-50.75(23-II-4)	-1.70(23-II-2)	-98.30(23-II-4)	41.53(22-II-2)
16	16	-415.03(5)	-10.50(23-I-4)	-32.67(22-II-3)	-1.70(23-II-2)	88.53(22-II-3)	38.61(6)
	116	-389.35(5)	-10.50(23-I-4)	-32.67(22-II-3)	-1.70(23-II-2)	-95.58(20)	22.71(20)
16	116	-178.07(5)	12.24(6)	-47.73(22-II-	3.33(23-I-2)	79.94(22-II-	51.33(6)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
				3)		3)	
	216	-156.14(5)	12.24(6)	-47.73(22-II-3)	3.33(23-I-2)	-120.40(20)	19.08(23-I-4)
17	17	-452.05(1)	26.21(5)	-75.26(23-II-3)	-11.94(6)	167.91(23-II-3)	42.46(20)
	35	-433.83(1)	26.21(5)	-75.26(23-II-3)	-11.94(6)	-81.17(20)	-47.06(23-II-1)
17	35	-337.65(1)	-52.65(22-II-3)	53.65(23-I-3)	18.73(6)	-124.91(20)	-37.18(23-II-1)
	117	-325.91(1)	-52.65(22-II-3)	53.65(23-I-3)	18.73(6)	-100.32(6)	56.74(20)
17	117	-198.21(1)	28.57(22-I-3)	50.82(22-II-3)	4.13(23-I-2)	-119.95(20)	52.16(22-I-3)
	217	-172.61(1)	28.57(22-I-3)	50.82(22-II-3)	4.13(23-I-2)	120.95(23-I-2)	-55.02(22-I-3)
18	18	-375.75(5)	47.39(22-I-3)	16.33(23-I-2)	-1.70(23-II-2)	-37.04(25-I-2)	119.23(22-I-3)
	118	-350.07(5)	47.39(22-I-3)	16.33(23-I-2)	-1.70(23-II-2)	-41.88(6)	-89.37(22-I-2)
18	118	-177.31(5)	56.48(22-I-3)	30.33(23-I-2)	3.33(23-I-2)	-53.62(23-I-2)	99.79(22-I-3)
	218	-155.37(5)	56.48(22-I-3)	30.33(23-I-2)	3.33(23-I-2)	60.14(23-I-2)	-112.03(22-I-3)
19	19	-547.00(1)	45.13(22-I-2)	20.42(23-I-2)	-1.70(23-II-2)	-47.51(23-I-2)	122.15(22-I-3)
	119	-521.32(1)	45.13(22-I-2)	20.42(23-I-2)	-1.70(23-II-2)	42.17(23-I-2)	-76.50(22-I-2)
19	119	-169.54(5)	43.62(22-I-3)	35.77(23-I-2)	3.33(23-I-2)	-65.10(23-I-2)	78.53(20)
	219	-147.60(5)	43.62(22-I-3)	35.77(23-I-2)	3.33(23-I-2)	69.04(23-I-2)	-91.42(22-I-3)
20	20	-251.76(1)	12.51(22-I-4)	-77.27(23-II-2)	-1.70(23-II-2)	185.63(23-II-2)	28.77(22-I-4)
	120	-226.08(1)	12.51(22-I-4)	-77.27(23-II-2)	-1.70(23-II-2)	-153.57(23-II-2)	-26.16(22-I-4)
21	21	-231.49(1)	-20.55(22-II-3)	53.98(23-I-4)	-1.70(23-II-2)	-129.89(23-I-4)	46.94(6)
	121	-205.81(1)	-20.55(22-II-3)	53.98(23-I-4)	-1.70(23-II-2)	-110.31(25-II-4)	51.50(22-II-3)
22	22	-461.60(1)	12.98(22-I-3)	47.80(23-I-4)	-1.70(23-II-2)	-122.31(23-I-4)	24.99(22-I-3)
	122	-435.91(1)	12.98(22-I-3)	47.80(23-I-4)	-1.70(23-II-2)	87.75(25-I-4)	51.25(6)
22	122	-171.49(1)	10.38(20)	-41.06(23-II-4)	3.33(23-I-2)	76.83(23-II-4)	46.91(20)
	222	-149.55(1)	10.38(20)	-41.06(23-II-4)	3.33(23-I-2)	80.13(23-I-4)	8.55(22-II-3)
23	23	-420.62(1)	-45.76(22-II-3)	71.80(23-I-3)	14.98(20)	-163.20(23-I-3)	-66.55(22-II-3)
	36	-402.40(1)	-45.76(22-II-3)	71.80(23-I-3)	14.98(20)	-91.67(6)	55.63(22-II-3)
23	36	-317.99(23-II-1)	49.08(22-II-3)	-65.19(23-II-1)	-23.17(20)	-64.05(6)	51.40(20)
	123	-308.96(23-II-1)	49.08(22-II-3)	-65.19(23-II-1)	-23.17(20)	-86.80(20)	-45.72(22-II-3)
23	123	-197.70(1)	27.03(23-I-4)	-44.16(23-II-2)	4.13(23-I-2)	-92.53(6)	50.68(23-I-4)
	223	-172.10(1)	27.03(23-I-4)	-44.16(23-II-2)	4.13(23-I-2)	-106.37(23-II-2)	-50.70(23-I-4)
24	24	-214.04(1)	-17.75(22-II-3)	52.99(23-I-4)	-1.70(23-II-2)	-124.85(23-I-4)	45.91(6)
	124	-188.36(1)	-17.75(22-II-3)	52.99(23-I-4)	-1.70(23-II-2)	107.79(23-I-4)	43.18(22-II-3)
25	25	-602.54(1)	-12.11(22-II-3)	50.92(23-I-4)	-1.70(23-II-2)	-129.93(23-I-4)	-30.47(22-II-3)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	125	-576.86(1)	-12.11(22-II-3)	50.92(23-I-4)	-1.70(23-II-2)	93.81(23-I-4)	44.24(21)
25	125	-180.78(1)	-25.16(22-II-3)	42.79(23-I-4)	3.33(23-I-2)	-75.48(23-I-4)	-41.91(22-II-3)
	225	-158.84(1)	-25.16(22-II-3)	42.79(23-I-4)	3.33(23-I-2)	85.32(23-I-4)	52.45(22-II-3)
26	26	-402.18(23-I-4)	10.08(22-I-3)	58.33(23-I-1)	-1.70(23-II-2)	-144.48(23-I-1)	-25.02(22-II-3)
	126	-382.42(23-I-4)	10.08(22-I-3)	58.33(23-I-1)	-1.70(23-II-2)	111.67(23-I-1)	46.36(6)
26	126	-158.99(23-I-4)	22.99(22-I-3)	55.13(23-I-1)	3.33(23-I-2)	-102.38(23-I-1)	41.93(20)
	226	-142.11(23-I-4)	22.99(22-I-3)	55.13(23-I-1)	3.33(23-I-2)	104.39(23-I-1)	-45.59(22-I-3)
27	27	-157.84(1)	42.71(20)	25.95(23-I-2)	-2.53(23-II-2)	-57.63(23-I-2)	186.99(20)
	127	-123.60(1)	42.71(20)	25.95(23-I-2)	-2.53(23-II-2)	56.30(23-I-2)	-40.36(22-I-3)
28	28	-156.34(5)	36.69(22-I-3)	30.49(23-I-2)	-2.53(23-II-2)	-66.89(23-I-2)	114.21(22-I-3)
	128	-122.10(5)	36.69(22-I-3)	30.49(23-I-2)	-2.53(23-II-2)	66.96(23-I-2)	78.33(6)
29	29	-167.95(1)	43.98(6)	18.82(23-I-4)	-2.53(23-II-2)	-42.95(23-I-4)	197.56(20)
	129	-133.71(1)	43.98(6)	18.82(23-I-4)	-2.53(23-II-2)	-56.47(6)	72.98(22-II-3)
30	30	-279.40(1)	70.92(22-I-3)	19.28(23-I-4)	-2.53(23-II-2)	-48.71(23-I-4)	187.29(22-I-3)
	130	-245.16(1)	70.92(22-I-3)	19.28(23-I-4)	-2.53(23-II-2)	35.93(23-I-4)	-124.06(22-I-3)
31	31	-181.72(5)	40.55(22-I-3)	29.59(23-I-1)	-2.53(23-II-2)	-67.22(23-I-1)	-143.36(22-II-3)
	131	-147.47(5)	40.55(22-I-3)	29.59(23-I-1)	-2.53(23-II-2)	62.68(23-I-1)	75.82(6)

Risultati Analisi Dinamica - Sollecitazioni massime - Inviluppi - Travi di fondazione

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
	N.fin.	kN	kN	kN	kN*m	kN*m	kN*m
9001	2	0	0	148.19(20)	-5.87(24-II-4)	-310.85(20)	97.56(6)
	3	0	0	-91.05(22-II-4)	-5.93(24-II-4)	-133.90(6)	97.56(6)
9001	3	0	0	74.32(24-I-1)	17.03(5)	-244.64(6)	97.56(6)
	4	0	0	-158.47(1)	17.06(5)	-327.91(20)	97.56(6)
9001	4	0	0	200.99(1)	-5.04(24-II-3)	-479.51(20)	97.56(6)
	5	0	0	-219.75(1)	-4.50(24-II-3)	-488.95(20)	97.56(6)
9001	5	0	0	184.29(1)	6.95(20)	-395.70(20)	97.56(6)
	6	0	0	-91.93(5)	9.29(20)	-187.09(20)	97.56(6)
9001	6	0	0	190.74(20)	-6.45(22-II-2)	-339.64(20)	97.56(6)
	7	0	0	-94.64(23-II-2)	6.90(24-I-2)	-122.18(24-II-1)	97.56(6)
9002	10	0	0	156.18(5)	-5.50(23-II-1)	-132.46(20)	97.56(6)
	11	0	0	-159.47(5)	-4.65(22-II-4)	-225.63(20)	97.56(6)
9002	11	0	0	201.86(1)	-6.55(22-II-	-360.38(20)	97.56(6)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
					3)		
	12	0	0	-97.95(5)	-6.87(23-I-2)	-43.91(22-II-1)	97.56(6)
9003	17	0	0	122.03(1)	-32.96(22-I-1)	-422.74(20)	97.56(6)
	18	0	0	-45.93(25-I-4)	-33.27(22-I-1)	-322.46(20)	97.56(6)
9003	18	0	0	198.30(1)	36.90(20)	-455.25(20)	97.56(6)
	19	0	0	-83.98(22-II-3)	35.40(20)	-146.73(20)	97.56(6)
9003	19	0	0	181.64(1)	-10.51(22-I-3)	-284.70(20)	97.56(6)
	20	0	0	-104.92(5)	-10.33(22-I-3)	-41.70(22-II-3)	97.56(6)
9004	27	0	0	148.32(20)	-28.09(22-I-3)	-236.57(20)	97.56(6)
	28	0	0	-100.30(23-I-2)	-28.08(22-I-3)	-101.32(22-II-3)	97.56(6)
9005	15	0	0	108.26(5)	-8.37(22-II-1)	-66.65(20)	97.56(6)
	13	0	0	-149.78(1)	-8.25(22-II-1)	-231.31(20)	97.56(6)
9006	21	0	0	115.59(5)	3.72(20)	-64.13(21)	97.56(6)
	22	0	0	-161.05(5)	3.67(20)	-90.11(20)	97.56(6)
9007	24	0	0	95.39(5)	11.65(20)	-49.65(21)	97.56(6)
	25	0	0	-171.29(1)	11.67(1)	-290.49(20)	97.56(6)
9007	25	0	0	223.66(1)	7.02(22-II-3)	-408.97(20)	97.56(6)
	26	0	0	-188.41(5)	8.02(22-II-3)	-106.97(20)	97.56(6)
9008	29	0	0	124.24(20)	16.59(22-II-3)	-249.31(20)	97.56(6)
	30	0	0	-88.80(22-II-3)	16.17(22-II-3)	-139.16(20)	97.56(6)
9008	30	0	0	156.86(20)	14.01(22-II-3)	-336.00(20)	97.56(6)
	31	0	0	-125.36(23-I-2)	15.24(22-II-3)	-155.13(22-II-3)	97.56(6)
9009	2	0	0	108.70(24-II-1)	-24.88(22-I-1)	-166.10(24-II-1)	97.56(6)
	15	0	0	-94.21(20)	-23.30(22-I-1)	-231.35(20)	97.56(6)
9009	15	0	0	71.85(23-I-4)	5.91(22-II-1)	-248.39(20)	97.56(6)
	21	0	0	-79.81(23-II-4)	-7.16(6)	-219.71(20)	97.56(6)
9009	21	0	0	69.37(20)	7.23(20)	-235.94(20)	97.56(6)
	24	0	0	-49.86(23-II-4)	5.98(20)	-147.19(6)	97.56(6)
9009	24	0	0	122.22(20)	-15.31(22-II-3)	-235.47(20)	97.56(6)
	29	0	0	-79.71(22-II-3)	-16.50(22-II-3)	-47.22(23-II-4)	97.56(6)
9010	13	0	0	108.28(23-I-4)	21.08(20)	-220.68(20)	97.56(6)
	22	0	0	-175.02(5)	23.81(20)	-385.91(20)	97.56(6)
9010	22	0	0	144.52(20)	-56.46(20)	-356.92(20)	97.56(6)
	25	0	0	-56.86(5)	-55.01(20)	-153.07(20)	97.56(6)
9010	25	0	0	181.12(1)	-15.29(22-II-3)	-311.44(20)	97.56(6)
	30	0	0	-75.96(5)	-15.33(22-II-3)	51.66(25-I-4)	97.56(6)
9011	23	0	0	199.20(20)	89.31(20)	-487.37(20)	97.56(6)
	26	0	0	73.31(6)	90.48(20)	-234.58(20)	97.56(6)
9011	26	0	0	231.93(20)	-26.84(22-II-3)	-382.01(20)	97.56(6)
	31	0	0	-76.18(23-II-2)	-26.66(22-II-3)	75.76(23-I-2)	97.56(6)

Asta	N.in.	N	Ty	Tz	Mt	My	Mz
9012	2	0	0	75.18(22-I-1)	-27.13(6)	206.97(22-II-1)	97.56(6)
	8	0	0	-100.20(22-II-1)	-26.66(6)	-81.64(6)	97.56(6)
9012	8	0	0	83.04(23-I-4)	22.86(23-I-4)	-103.64(21)	97.56(6)
	13	0	0	-94.74(23-II-4)	22.70(23-I-4)	-139.17(6)	97.56(6)
9012	13	0	0	63.78(1)	-37.75(20)	-209.67(20)	97.56(6)
	16	0	0	-145.95(5)	-37.56(20)	-297.77(20)	97.56(6)
9012	16	0	0	188.22(1)	17.00(20)	-395.14(20)	97.56(6)
	23	0	0	-164.72(5)	17.02(20)	-258.21(20)	97.56(6)
9013	3	0	0	70.75(22-I-1)	9.21(23-I-4)	84.90(24-II-1)	97.56(6)
	9	0	0	-139.47(1)	9.04(23-I-4)	-232.07(20)	97.56(6)
9013	9	0	0	175.36(20)	-32.44(20)	-370.81(20)	97.56(6)
	14	0	0	-99.23(5)	-31.42(20)	-112.82(20)	97.56(6)
9013	14	0	0	191.99(1)	-24.61(20)	-383.84(20)	97.56(6)
	17	0	0	-169.73(5)	-24.97(20)	-259.83(20)	97.56(6)
9014	17	0	0	172.56(20)	10.65(22-I-3)	-481.01(20)	97.56(6)
	23	0	0	-124.76(23-II-2)	11.20(22-I-3)	-313.52(20)	97.56(6)
9015	14	0	0	146.44(1)	7.66(22-II-1)	-203.96(20)	97.56(6)
	16	0	0	-86.86(5)	8.03(22-II-1)	-102.47(20)	97.56(6)
9016	9	0	0	83.44(5)	10.10(6)	-52.10(23-I-4)	97.56(6)
	13	0	0	-176.80(20)	10.74(20)	-318.96(20)	97.56(6)
9017	3	0	0	64.73(24-II-1)	-12.01(23-I-4)	82.37(22-I-1)	97.56(6)
	8	0	0	-81.83(22-I-1)	-11.24(23-I-4)	-129.10(20)	97.56(6)
9018	4	0	0	157.75(5)	-11.32(5)	-96.52(20)	97.56(6)
	14	0	0	-196.10(1)	-10.07(22-II-2)	-250.34(20)	97.56(6)
9019	5	0	0	100.79(5)	-37.48(20)	-53.61(20)	97.56(6)
	10	0	0	-227.39(1)	-38.95(20)	-321.49(20)	97.56(6)
9019	10	0	0	217.53(1)	26.21(20)	-255.95(20)	97.56(6)
	18	0	0	-179.04(5)	24.19(20)	-84.64(23-II-3)	97.56(6)
9020	6	0	0	102.78(5)	3.06(20)	-78.04(20)	97.56(6)
	11	0	0	-148.63(5)	2.31(20)	-180.92(20)	97.56(6)
9020	11	0	0	134.12(5)	-11.22(20)	-182.40(20)	97.56(6)
	19	0	0	-157.89(5)	-12.48(20)	-266.20(20)	97.56(6)
9020	19	0	0	164.52(20)	36.43(22-I-3)	-308.64(20)	97.56(6)
	27	0	0	-71.10(22-II-3)	36.70(22-I-3)	62.12(22-I-3)	97.56(6)
9021	7	0	0	76.32(22-I-1)	19.14(22-II-1)	-90.55(20)	97.56(6)
	12	0	0	-78.71(1)	18.09(22-II-1)	-120.88(20)	97.56(6)
9021	12	0	0	96.46(23-I-2)	4.42(23-I-4)	-216.39(20)	97.56(6)
	20	0	0	-98.99(23-II-2)	4.12(23-I-4)	-179.45(20)	97.56(6)
9021	20	0	0	114.64(20)	22.37(22-I-3)	-179.68(6)	97.56(6)
	28	0	0	-85.65(22-I-3)	23.37(22-I-3)	-85.57(23-II-2)	97.56(6)

Verifiche stato limite ultimo

Verifica Punzonamento

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Simbologia

Nodo Nodo in cui la verifica è condotta
Comb Combinazione in cui la forze di punzonamento e' massima
U [cm] Perimetro della sezione critica
Hp [cm] Altezza della piastra
Fpunz. [kN] Forza di punzonamento
FRes. [kN] Forza resistente al punzonamento
Afx [cmq] Armatura (se richiesta) in direzione X della piastra
Afy [cmq] Armatura (se richiesta) in direzione Y della piastra

Nodo	Comb	U	Hp	Fpunz.	FRes.	Afx	Afy
		cm	cm	kN	kN	cmq	cmq
109	(22+23)-IV-2	60.00	25.00	32.30	89.53	0.00	0.00
113	5	0.00	25.00	46.77	0.00	0.42	0.42
119	1	60.00	25.00	41.30	89.53	0.00	0.00
120	5	0.00	25.00	38.88	0.00	0.35	0.35
125	1	114.33	25.00	39.83	170.60	0.00	0.00
130	5	0.00	25.00	38.59	0.00	0.35	0.35
214	(22+23)-IV-2	60.00	25.00	24.86	89.53	0.00	0.00
216	20	0.00	25.00	29.48	0.00	0.27	0.27

Verifica delle travi di fondazione

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Simbologia:

Terreno Nome della stratigrafia per travi Winkler
L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica
B[cm]: Larghezza
H[cm]: Altezza
Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
X [cm] Punto di verifica
ILN Inizio luce netta
CAMP Punto di massimo momento sia superiore che inferiore ad esclusione degli estremi
FLN Fine luce netta
M- [kN*m] Momento negativo massimo di calcolo([1])
N- [kN] Sforzo normale corrispondente ad M-

M+ [kN*m] Momento positivo massimo di calcolo([1])
N+ [kN] Sforzo normale corrispondente ad M+
ΔM- [kN*m] Incremento di M- per la traslazione del diagramma del momento a causa del taglio
ΔM+ [kN*m] Incremento di M+ per la traslazione del diagramma del momento a causa del taglio
Afs [cmq] Area di ferro superiore
Afi [cmq] Area di ferro inferiore
εsc- Deformazione nel cls per effetto di M-:N-([4])
εsc+ Deformazione nel cls per effetto di M+:N+([4])
εsf- Deformazione nell'acciaio per effetto di M-:N-([4])
εsf+ Deformazione nell'acciaio per effetto di M+:N+([4])
C- Combinazione di carico generatore di M-:N-
C+ Combinazione di carico generatore di M+:N+
x- [cm] Profondità asse neutro per la combinazione C-([5])
d- [cm] Altezza utile della sezione per la combinazione C-([6])
x+ [cm] Profondità asse neutro per la combinazione C+([5])
d+ [cm] Altezza utile della sezione per la combinazione C+([6])
Mr- [kN*m] Momento resistente superiore
Mr+ [kN*m] Momento resistente inferiore
Stato- Stato della sezione per la combinazione C-([7])
Stato+ Stato della sezione per la combinazione C+([7])
Comb Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
- C Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
    1) Sc = + SismaZ*fz + SismaX*fx + SismaY*fy
    2) Sc = + SismaZ*fz + SismaX*fx - SismaY*fy
    3) Sc = + SismaZ*fz - SismaX*fx + SismaY*fy
    4) Sc = + SismaZ*fz - SismaX*fx - SismaY*fy.
    5) Sc = - SismaZ*fz + SismaX*fx + SismaY*fy
    6) Sc = - SismaZ*fz + SismaX*fx - SismaY*fy
    7) Sc = - SismaZ*fz - SismaX*fx + SismaY*fy
    8) Sc = - SismaZ*fz - SismaX*fx - SismaY*fy.

Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).
Sez Sezione di verifica [Sinistra/Destra]
Td [kN] Taglio di verifica([2])
VRdns [kN] Resistenza a taglio in assenza di armature
VRcd [kN] Resistenza taglio-compressione calcestruzzo
VRsd [kN] Resistenza taglio-trazione acciaio
VRd [kN] Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kN] Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
Mt [kN*m] Momento torcente
Tpl [kN] Taglio dovuto ai momenti resistenti alle estremità della trave
Mr [kN*m] Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto
Dx [cm] Distanza dall'estremo da armare con staffe
Staffe [cmq] Area delle staffe
cot(θ) cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
F.Par. [cmq] Area armatura longitudinale di parete([3])
Cs Coefficiente di sicurezza definito dal rapporto Fr/Fd (Fr=resistenza,Fd=azione)
ζ_E Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Simbologia verifica travi collegamento:
Comb Combinazione più gravosa

Nsd [kN] Azione verticale negli elementi collegati, nella combinazione specificata
α Coefficiente in funzione della classe di terreno (NTC 7.2.5.1)
a/g Punto di aggancio dello spettro di accelerazione [a/g=Sa(0)]
N Sforzo normale di verifica N=α*Nsd*a/g
Af [cmq] Area di ferro complessiva nella sezione
NRd C [kN] Resistenza a compressione della sezione
NRd T [kN] Resistenza a trazione della sezione

Verifiche duttilità (quando richieste):
Zona Sezione di verifica dell'elemento
Comb. Combinazione di verifica
Nmax [kN] Sforzo Normale massimo
Dir Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kN*m] Momento di snervamento corrispondente a Nmax
MrU [kN*m] Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
ϕy[1/m] Curvatura allo snervamento (ϕy= MrU/Mry * ϕ'y)
ϕu[1/m] Curvatura allo corrispondente a MrU
μ Capacita in duttilità della sezione
F.Conf Fattore di confinamento adottato (= fck,c/fck)
μd Richiesta in duttilità della sezione
Cs Livello di sicurezza (Cs=μ/μd)

Note Verifica travi:
([1]) il valore del momento di verifica è dato da M +ΔM
([2]) Td è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di Tpl ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di comportamento
([3]) armatura necessaria per la sola verifica a torsione
([4]) le deformazioni sono stampate a meno del fattore 10^{-3}
([5]) distanza tra la fibra di cls compressa piu' lontata e l'asse neutro in direzione ortogonale all'asse neutro
([6]) distanza tra le fibre sollecitate piu' lontane dall'asse neutro: nel caso di sezione parzializzata le due fibre sono quella di cls compresso e quella dell'acciaio teso piu lontane da n-n, mentre nel caso di sezione completamente compressa le due fibre sono le due di cls compresso piu lontane da n-n
([7]) Indica lo stato della sezione se: completamente compressa (Compr.),completamente tesa (Tesa), parzializzata (Parz.)

Trave di fondazione: 9001 [2,3], Pilastrate [2,3] Sez. R: By=50.00 cm Bz=100.00 cm L=514.30 cm Ln=514.30 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	56.07	310.85	62.15	--	12.72	12.72	463.51	463.51	(22+23)-I-4	20	1.5
51.43	91.70	240.59	40.54	70.26	12.72	12.72	463.51	463.51	(22+23)-I-4	20	1.5
CAMP	137.18	182.10	--	128.76	12.72	12.72	463.51	463.51	(22+23)-I-4	20	1.5
462.87	38.22	121.87	64.82	12.04	12.72	12.72	463.51	463.51	(22+23)-I-4	6	3.5
FLN	21.30	133.90	60.07	--	12.72	12.72	463.51	463.51	5	6	3.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.15	96.00	0.220	21.47	96.00	0.224	463.51	463.51	(22+23)-I-4	20	Parz.	Parz.
51.43	21.17	96.00	0.221	21.47	96.00	0.224	463.51	463.51	(22+23)-I-4	20	Parz.	Parz.
CAMP	21.18	96.00	0.221	21.47	96.00	0.224	463.51	463.51	(22+23)-I-4	20	Parz.	Parz.
462.87	21.13	96.00	0.220	21.18	96.00	0.221	463.51	463.51	(22+23)-I-4	6	Parz.	Parz.
FLN	21.09	96.00	0.220	21.18	96.00	0.221	463.51	463.51	5	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-

V-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	148.19	--	1523.88	339.88	339.88	5.95	0.00	463.51	151.00	10.33	0.00	2.3
Cen	80.30	--	1523.88	266.42	266.42	--	--	--	--	7.88	--	3.3
Des	99.83	--	1523.88	339.88	339.88	6.47	0.00	463.51	151.00	10.35	0.00	3.4

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.12

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	5.95	326.62	148.19	1523.88	0.12
Des.	6.47	326.62	99.83	1523.88	0.09

Trave di fondazione: 9001 [3,4], Pilastrate [3,4] Sez. R: By=50.00 cm Bz=100.00 cm L=463.50 cm Ln=463.50 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	151.99	244.64	--	--	12.72	12.72	463.51	463.51	(22+23)-III-3	6	1.9
46.35	138.97	218.98	13.02	25.66	12.72	12.72	463.51	463.51	(22+23)-III-3	6	1.9
CAMP	122.43	218.41	29.56	109.50	12.72	12.72	463.51	463.51	(22+23)-III-3	20	1.4
417.15	-1.67	266.85	17.43	61.06	12.72	12.72	463.51	463.51	(24+25)-III-2	20	1.4
FLN	-22.42	327.91	36.08	--	12.72	12.72	463.51	463.51	(24+25)-III-2	20	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.21	96.00	0.221	21.36	96.00	0.222	463.51	463.51	(22+23)-III-3	6	Parz.	Parz.
46.35	21.21	96.00	0.221	21.36	96.00	0.222	463.51	463.51	(22+23)-III-3	6	Parz.	Parz.
CAMP	21.21	96.00	0.221	21.50	96.00	0.224	463.51	463.51	(22+23)-III-3	20	Parz.	Parz.
417.15	20.99	96.00	0.219	21.50	96.00	0.224	463.51	463.51	(24+25)-III-2	20	Parz.	Parz.
FLN	20.99	96.00	0.219	21.50	96.00	0.224	463.51	463.51	(24+25)-III-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(24+25)-III-2 Cen=(22+23)-III-3 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	87.17	--	1523.88	339.88	339.88	17.03	0.00	463.51	151.00	10.84	0.00	3.9
Cen	77.65	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	3.4
Des	158.47	--	1523.88	339.88	339.88	17.06	0.00	463.51	151.00	10.84	0.00	2.1

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.16

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	17.03	326.62	87.17	1523.88	0.11
Des.	17.06	326.62	158.47	1523.88	0.16

Trave di fondazione: 9001 [4,5], Pilastrate [4,5] Sez. R: By=50.00 cm Bz=100.00 cm L=590.40 cm Ln=590.40 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	11.72	479.51	30.64	--	12.72	15.27	463.53	554.97	(24+25)-III-3	20	1.2
59.04	29.40	375.73	18.81	103.78	12.72	15.27	463.53	554.97	(24+25)-I-4	20	1.2
CAMP	48.89	294.66	--	175.58	12.72	15.27	463.53	554.97	(24+25)-I-4	20	1.2
531.36	7.08	379.37	24.68	109.58	12.72	15.27	463.53	554.97	(24+25)-III-2	20	1.1

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
FLN	-11.75	488.95	37.82	--	12.72	15.27	463.53	554.97	(24+25)-I-1	20	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	20.59	96.00	0.214	23.66	96.00	0.246	463.53	554.97	(24+25)-III-3	20	Parz.	Parz.
59.04	20.60	96.00	0.215	23.66	96.00	0.246	463.53	554.97	(24+25)-I-4	20	Parz.	Parz.
CAMP	20.60	96.00	0.215	23.65	96.00	0.246	463.53	554.97	(24+25)-I-4	20	Parz.	Parz.
531.36	20.57	96.00	0.214	23.68	96.00	0.247	463.53	554.97	(24+25)-III-2	20	Parz.	Parz.
FLN	20.56	96.00	0.214	23.68	96.00	0.247	463.53	554.97	(24+25)-I-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=(22+23)-I-4 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	200.99	--	1523.88	339.88	339.88	5.67	0.00	554.97	151.00	10.31	0.00	1.7
Cen	104.44	--	1523.88	271.18	271.18	--	--	--	--	8.02	--	2.6
Des	219.75	--	1523.88	339.88	339.88	5.36	0.00	463.53	151.00	10.30	0.00	1.5

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.16

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	5.67	326.62	200.99	1523.88	0.15
Des.	5.36	326.62	219.75	1523.88	0.16

Trave di fondazione: 9001 [5,6], Pilastrate [5,6] Sez. R: By=50.00 cm Bz=100.00 cm L=397.00 cm Ln=397.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	395.70	--	--	12.72	15.27	463.53	554.97	1	20	1.4
39.70	-49.58	328.67	65.33	67.03	12.72	15.27	463.53	554.97	(24+25)-III-2	20	1.4
CAMP	40.60	272.61	--	123.09	12.72	15.27	463.53	554.97	(22+23)-III-2	20	1.4
357.30	23.89	164.90	16.48	22.19	12.72	15.27	463.53	554.97	(22+23)-III-2	20	3.0
FLN	6.64	187.09	32.47	--	12.72	15.27	463.53	554.97	(22+23)-III-2	20	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	--	--	--	23.51	96.00	0.245	463.53	554.97	1	20	--	Parz.
39.70	20.55	96.00	0.214	23.51	96.00	0.245	463.53	554.97	(24+25)-III-2	20	Parz.	Parz.
CAMP	20.59	96.00	0.214	23.51	96.00	0.245	463.53	554.97	(22+23)-III-2	20	Parz.	Parz.
357.30	20.58	96.00	0.214	23.15	96.00	0.241	463.53	554.97	(22+23)-III-2	20	Parz.	Parz.
FLN	20.58	96.00	0.214	23.15	96.00	0.241	463.53	554.97	(22+23)-III-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	184.29	--	1523.88	339.88	339.88	6.95	0.00	554.97	151.00	10.37	0.00	1.8
Cen	74.98	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	3.5
Des	91.93	--	1523.88	339.88	339.88	9.29	0.00	463.53	151.00	10.48	0.00	3.7

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.14

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	6.95	326.62	184.29	1523.88	0.14
Des.	9.29	326.62	91.93	1523.88	0.09

Trave di fondazione: 9001 [6,7], Pilastrate [6,7] Sez. R: By=50.00 cm Bz=100.00 cm L=530.00 cm Ln=530.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-25.08	339.64	42.03	--	10.18	10.18	371.93	371.93	(24+25)-I-4	20	1.1
53.00	-50.52	246.24	88.74	93.40	10.18	10.18	371.93	371.93	(22+23)-VI-2	20	1.1
CAMP	141.84	167.80	--	171.84	10.18	10.18	371.93	371.93	(22+23)-III-2	20	1.1
477.00	142.05	98.96	--	39.45	10.18	10.18	371.93	371.93	(22+23)-I-1	(24+25)-I-4	2.6
FLN	134.81	138.41	--	--	10.18	10.18	371.93	371.93	(22+23)-I-1	(24+25)-I-4	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.32	96.00	0.201	19.89	96.00	0.207	371.93	371.93	(24+25)-I-4	20	Parz.	Parz.
53.00	19.35	96.00	0.202	19.89	96.00	0.207	371.93	371.93	(22+23)-VI-2	20	Parz.	Parz.
CAMP	19.53	96.00	0.203	19.89	96.00	0.207	371.93	371.93	(22+23)-III-2	20	Parz.	Parz.
477.00	19.53	96.00	0.203	19.52	96.00	0.203	371.93	371.93	(22+23)-I-1	(24+25)-I-4	Parz.	Parz.
FLN	19.51	96.00	0.203	19.52	96.00	0.203	371.93	371.93	(22+23)-I-1	(24+25)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-II-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	190.74	--	1523.88	339.88	339.88	6.75	0.00	371.93	151.00	10.36	0.00	1.8
Cen	107.94	--	1523.88	264.35	264.35	--	--	--	--	7.82	--	2.4
Des	100.20	--	1523.88	339.88	339.88	7.40	0.00	371.93	151.00	10.39	0.00	3.4

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.14

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	6.75	326.62	190.74	1523.88	0.14
Des.	7.40	326.62	100.20	1523.88	0.09

Trave di fondazione: 9002 [10,11], Pilastrate [10,11] Sez. R: By=50.00 cm Bz=100.00 cm L=427.00 cm Ln=427.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-65.43	132.46	119.06	--	10.18	10.18	371.93	371.93	5	20	2.8
42.70	-6.33	90.92	82.31	41.54	10.18	10.18	371.93	371.93	5	20	2.8
CAMP	85.50	124.48	--	101.16	10.18	10.18	371.93	371.93	5	20	1.6
384.30	-36.54	170.33	99.43	55.30	10.18	10.18	371.93	371.93	5	20	1.6
FLN	-35.48	225.63	72.40	--	10.18	10.18	371.93	371.93	(22+23)-III-2	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.38	96.00	0.202	19.51	96.00	0.203	371.93	371.93	5	20	Parz.	Parz.
42.70	19.42	96.00	0.202	19.51	96.00	0.203	371.93	371.93	5	20	Parz.	Parz.
CAMP	19.43	96.00	0.202	19.67	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.
384.30	19.39	96.00	0.202	19.67	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
FLN	19.35	96.00	0.202	19.67	96.00	0.205	371.93	371.93	(22+23)-III-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	156.18	--	1523.88	339.88	339.88	6.45	0.00	371.93	151.00	10.35	0.00	2.2
Cen	49.92	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	5.2
Des	159.47	--	1523.88	339.88	339.88	5.50	0.00	371.93	151.00	10.31	0.00	2.1

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.12

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	6.45	326.62	156.18	1523.88	0.12
Des.	5.50	326.62	159.47	1523.88	0.12

Trave di fondazione: 9002 [11,12], Pilastrate [11,12] Sez. R: By=50.00 cm Bz=100.00 cm L=530.00 cm Ln=530.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-42.25	360.38	62.03	--	10.18	10.18	371.93	371.93	(24+25)-I-4	20	1.0
53.00	-14.18	267.04	52.98	93.34	10.18	10.18	371.93	371.93	(22+23)-I-4	20	1.0
CAMP	99.64	187.42	--	172.96	10.18	10.18	371.93	371.93	5	20	1.0
477.00	45.39	14.00	50.20	32.32	10.18	10.18	371.93	371.93	5	(22+23)-III-3	3.9
FLN	45.71	46.31	39.68	--	10.18	10.18	371.93	371.93	(22+23)-III-2	(22+23)-III-3	4.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.32	96.00	0.201	17.47	96.00	0.182	371.93	371.93	(24+25)-I-4	20	Parz.	Parz.
53.00	19.35	96.00	0.202	17.47	96.00	0.182	371.93	371.93	(22+23)-I-4	20	Parz.	Parz.
CAMP	19.45	96.00	0.203	17.47	96.00	0.182	371.93	371.93	5	20	Parz.	Parz.
477.00	19.45	96.00	0.203	19.37	96.00	0.202	371.93	371.93	5	(22+23)-III-3	Parz.	Parz.
FLN	19.43	96.00	0.202	19.37	96.00	0.202	371.93	371.93	(22+23)-III-2	(22+23)-III-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	201.86	--	1523.88	339.88	339.88	7.88	0.00	371.93	151.00	10.42	0.00	1.7
Cen	113.56	--	1523.88	267.05	267.05	--	--	--	--	7.90	--	2.4
Des	97.95	--	1523.88	339.88	339.88	8.29	0.00	371.93	151.00	10.43	0.00	3.5

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.16

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	7.88	326.62	201.86	1523.88	0.16
Des.	8.29	326.62	97.95	1523.88	0.09

Trave di fondazione: 9003 [17,18], Pilastrate [17,18] Sez. R: By=50.00 cm Bz=100.00 cm L=179.02 cm Ln=179.30 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	422.74	--	--	12.72	15.27	463.53	554.97	1	20	1.3
17.93	--	402.93	--	19.80	12.72	15.27	463.53	554.97	1	20	1.3
CAMP	--	336.70	--	86.04	12.72	15.27	463.53	554.97	1	20	1.3

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
161.37	--	322.85	--	47.42	12.72	15.27	463.53	554.97	1	20	1.5
FLN	--	322.46	--	34.52	12.72	15.27	463.53	554.97	1	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	--	--	--	23.56	96.00	0.245	463.53	554.97	1	20	--	Parz.
17.93	--	--	--	23.56	96.00	0.245	463.53	554.97	1	20	--	Parz.
CAMP	--	--	--	23.56	96.00	0.245	463.53	554.97	1	20	--	Parz.
161.37	--	--	--	23.46	96.00	0.244	463.53	554.97	1	20	--	Parz.
FLN	--	--	--	23.44	96.00	0.244	463.53	554.97	1	20	--	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: 4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	122.03	--	1523.88	342.28	342.28	38.34	0.00	554.97	179.30	11.89	0.00	2.8
Des								463.53				

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.20

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	38.34	326.62	122.03	1523.88	0.20
Des.	38.60	326.62	122.03	1523.88	0.20

Trave di fondazione: 9003 [18,19], Pilastrate [18,19] Sez. R: By=50.00 cm Bz=100.00 cm L=427.00 cm Ln=427.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	0.16	455.25	27.74	--	12.72	15.27	463.53	554.97	(24+25)-V-3	20	1.2
42.70	16.16	379.10	12.52	76.15	12.72	15.27	463.53	554.97	(24+25)-V-3	20	1.2
CAMP	66.97	314.36	9.58	140.89	12.72	15.27	463.53	554.97	(24+25)-V-2	20	1.2
384.30	74.71	141.86	1.84	27.26	12.72	15.27	463.53	554.97	(24+25)-V-2	6	3.3
FLN	76.55	135.45	--	21.02	12.72	15.27	463.53	554.97	(24+25)-V-2	6	3.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	20.57	96.00	0.214	23.62	96.00	0.246	463.53	554.97	(24+25)-V-3	20	Parz.	Parz.
42.70	20.57	96.00	0.214	23.62	96.00	0.246	463.53	554.97	(24+25)-V-3	20	Parz.	Parz.
CAMP	20.64	96.00	0.215	23.62	96.00	0.246	463.53	554.97	(24+25)-V-2	20	Parz.	Parz.
384.30	20.64	96.00	0.215	23.12	96.00	0.241	463.53	554.97	(24+25)-V-2	6	Parz.	Parz.
FLN	20.64	96.00	0.215	23.10	96.00	0.241	463.53	554.97	(24+25)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=(22+23)-V-2 Des=(22+23)-V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	198.30	--	1523.88	339.88	339.88	36.90	0.00	554.97	151.00	11.75	0.00	1.7
Cen	92.91	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	2.8
Des	89.03	--	1523.88	339.88	339.88	35.40	0.00	463.53	151.00	11.68	0.00	3.8

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.24

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	36.90	326.62	198.30	1523.88	0.24

	TEd	TRcd	VEd	VRcd	ρ
Des.	35.40	326.62	89.03	1523.88	0.17

Trave di fondazione: 9003 [19,20], Pilastrate [19,20] Sez. R: By=50.00 cm Bz=100.00 cm L=530.00 cm Ln=530.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-47.56	284.70	69.98	--	10.18	10.18	371.93	371.93	(22+23)-I-4	20	1.3
53.00	-49.48	200.03	113.14	84.67	10.18	10.18	371.93	371.93	5	20	1.3
CAMP	115.95	129.09	--	155.61	10.18	10.18	371.93	371.93	5	20	1.3
477.00	46.36	13.08	59.93	32.56	10.18	10.18	371.93	371.93	5	(22+23)-V-3	3.5
FLN	42.27	45.64	50.23	--	10.18	10.18	371.93	371.93	(22+23)-V-2	(22+23)-V-3	4.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.33	96.00	0.201	19.78	96.00	0.206	371.93	371.93	(22+23)-I-4	20	Parz.	Parz.
53.00	19.39	96.00	0.202	19.78	96.00	0.206	371.93	371.93	5	20	Parz.	Parz.
CAMP	19.48	96.00	0.203	19.78	96.00	0.206	371.93	371.93	5	20	Parz.	Parz.
477.00	19.47	96.00	0.203	19.37	96.00	0.202	371.93	371.93	5	(22+23)-V-3	Parz.	Parz.
FLN	19.44	96.00	0.203	19.37	96.00	0.202	371.93	371.93	(22+23)-V-2	(22+23)-V-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	181.64	--	1523.88	339.88	339.88	11.31	0.00	371.93	151.00	10.57	0.00	1.9
Cen	98.03	--	1523.88	267.05	267.05	--	--	--	--	7.90	--	2.7
Des	104.92	--	1523.88	339.88	339.88	11.30	0.00	371.93	151.00	10.57	0.00	3.2

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	11.31	326.62	181.64	1523.88	0.15
Des.	11.30	326.62	104.92	1523.88	0.10

Trave di fondazione: 9004 [27,28], Pilastrate [27,28] Sez. R: By=50.00 cm Bz=100.00 cm L=500.00 cm Ln=500.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	4.96	236.57	50.99	--	10.18	10.18	371.93	371.93	(22+23)-VI-3	20	1.6
50.00	34.75	168.25	29.53	68.32	10.18	10.18	371.93	371.93	(22+23)-VI-3	20	1.6
CAMP	74.07	111.30	8.61	125.26	10.18	10.18	371.93	371.93	(22+23)-V-2	20	1.6
450.00	83.62	80.19	--	41.35	10.18	10.18	371.93	371.93	(22+23)-V-2	(22+23)-V-3	3.1
FLN	78.56	121.55	--	--	10.18	10.18	371.93	371.93	(24+25)-V-2	(22+23)-V-3	3.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.38	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-VI-3	20	Parz.	Parz.
50.00	19.40	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-VI-3	20	Parz.	Parz.
CAMP	19.43	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-V-2	20	Parz.	Parz.
450.00	19.43	96.00	0.202	19.49	96.00	0.203	371.93	371.93	(22+23)-V-2	(22+23)-V-3	Parz.	Parz.
FLN	19.42	96.00	0.202	19.49	96.00	0.203	371.93	371.93	(24+25)-V-2	(22+23)-V-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-

VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	148.32	--	1523.88	339.88	339.88	30.46	0.00	371.93	151.00	11.45	0.00	2.3
Cen	60.51	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.3
Des	106.62	--	1523.88	339.88	339.88	30.06	0.00	371.93	151.00	11.44	0.00	3.2

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.19

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	30.46	326.62	148.32	1523.88	0.19
Des.	30.06	326.62	106.62	1523.88	0.16

Trave di fondazione: 9005 [15,13], Pilastrate [15,13] Sez. R: By=50.00 cm Bz=100.00 cm L=531.07 cm Ln=578.55 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	32.55	66.65	58.60	--	10.18	10.18	371.93	371.93	(22+23)-III-3	20	4.1
57.85	44.34	31.24	68.76	35.42	10.18	10.18	371.93	371.93	5	20	3.3
CAMP	137.31	100.88	--	120.76	10.18	10.18	371.93	371.93	5	20	1.7
520.69	4.91	158.75	91.82	72.57	10.18	10.18	371.93	371.93	5	20	1.6
FLN	-69.75	231.31	123.96	--	10.18	10.18	371.93	371.93	5	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.44	96.00	0.203	19.40	96.00	0.202	371.93	371.93	(22+23)-III-3	20	Parz.	Parz.
57.85	19.48	96.00	0.203	19.40	96.00	0.202	371.93	371.93	5	20	Parz.	Parz.
CAMP	19.52	96.00	0.203	19.67	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.
520.69	19.45	96.00	0.203	19.68	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.
FLN	19.38	96.00	0.202	19.68	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=20 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	108.26	--	1523.88	339.88	339.88	8.75	0.00	371.93	151.00	10.46	0.00	3.1
Cen	65.77	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.0
Des	149.78	--	1523.88	339.88	339.88	8.71	0.00	371.93	151.00	10.45	0.00	2.3

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.12

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	8.75	326.62	108.26	1523.88	0.10
Des.	8.71	326.62	149.78	1523.88	0.12

Trave di fondazione: 9006 [21,22], Pilastrate [21,22] Sez. R: By=50.00 cm Bz=100.00 cm L=574.50 cm Ln=574.50 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	3.02	64.13	99.70	--	10.18	10.18	371.93	371.93	5	21	3.6
57.45	62.50	33.70	73.85	30.42	10.18	10.18	371.93	371.93	5	21	2.7
CAMP	162.14	-15.16	--	97.99	10.18	10.18	371.93	371.93	5	20	2.3
517.05	18.17	29.50	100.78	60.61	10.18	10.18	371.93	371.93	5	20	3.1
FLN	-63.90	90.11	136.80	--	10.18	10.18	371.93	371.93	5	20	4.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.46	96.00	0.203	19.40	96.00	0.202	371.93	371.93	5	21	Parz.	Parz.
57.45	19.52	96.00	0.203	19.40	96.00	0.202	371.93	371.93	5	21	Parz.	Parz.
CAMP	19.56	96.00	0.204	19.43	96.00	0.202	371.93	371.93	5	20	Parz.	Parz.
517.05	19.49	96.00	0.203	19.44	96.00	0.202	371.93	371.93	5	20	Parz.	Parz.
FLN	19.41	96.00	0.202	19.44	96.00	0.202	371.93	371.93	5	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=5 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	115.59	--	1523.88	339.88	339.88	3.72	0.00	371.93	151.00	10.22	0.00	2.9
Cen	61.18	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.3
Des	161.05	--	1523.88	339.88	339.88	3.71	0.00	371.93	151.00	10.22	0.00	2.1

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.12

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	3.72	326.62	115.59	1523.88	0.09
Des.	3.71	326.62	161.05	1523.88	0.12

Trave di fondazione: 9007 [24,25], Pilastrate [24,25] Sez. R: By=50.00 cm Bz=100.00 cm L=544.50 cm Ln=544.50 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	43.72	49.08	48.59	8.56	10.18	10.18	371.93	371.93	(22+23)-V-3	6	4.0
54.45	53.64	51.51	51.49	15.49	10.18	10.18	371.93	371.93	5	6	3.5
CAMP	111.69	148.33	--	140.88	10.18	10.18	371.93	371.93	5	20	1.3
490.05	-32.65	212.85	83.80	77.64	10.18	10.18	371.93	371.93	(22+23)-VI-3	20	1.3
FLN	-100.72	290.49	114.56	--	10.18	10.18	371.93	371.93	(22+23)-VI-3	20	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.44	96.00	0.203	19.39	96.00	0.202	371.93	371.93	(22+23)-V-3	6	Parz.	Parz.
54.45	19.46	96.00	0.203	19.40	96.00	0.202	371.93	371.93	5	6	Parz.	Parz.
CAMP	19.48	96.00	0.203	19.79	96.00	0.206	371.93	371.93	5	20	Parz.	Parz.
490.05	19.37	96.00	0.202	19.79	96.00	0.206	371.93	371.93	(22+23)-VI-3	20	Parz.	Parz.
FLN	19.31	96.00	0.201	19.79	96.00	0.206	371.93	371.93	(22+23)-VI-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=4 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	95.39	--	1523.88	339.88	339.88	11.65	0.00	371.93	151.00	10.59	0.00	3.6
Cen	87.77	--	1523.88	269.37	269.37	--	--	--	--	7.97	--	3.1
Des	171.29	--	1523.88	339.88	339.88	11.67	0.00	371.93	151.00	10.59	0.00	2.0

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	11.65	326.62	95.39	1523.88	0.10
Des.	11.67	326.62	171.29	1523.88	0.15

Trave di fondazione: 9007 [25,26], Pilastrate [25,26] Sez. R: By=50.00 cm Bz=100.00 cm L=604.50 cm Ln=604.50 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-94.56	408.97	107.77	--	10.18	12.72	371.92	463.46	(24+25)-VI-3	20	1.1
60.45	-34.21	292.07	94.44	116.89	10.18	12.72	371.92	463.46	(22+23)-VI-3	20	1.1
CAMP	149.46	192.70	--	191.32	10.18	12.72	371.92	463.46	5	20	1.2
544.05	18.06	31.11	104.34	86.48	10.18	12.72	371.92	463.46	5	(22+23)-VI-3	3.0
FLN	8.39	117.59	77.21	--	10.18	12.72	371.92	463.46	(22+23)-V-2	(22+23)-VI-3	3.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	18.86	96.00	0.196	22.17	96.00	0.231	371.92	463.46	(24+25)-VI-3	20	Parz.	Parz.
60.45	18.93	96.00	0.197	22.17	96.00	0.231	371.92	463.46	(22+23)-VI-3	20	Parz.	Parz.
CAMP	19.07	96.00	0.199	22.12	96.00	0.230	371.92	463.46	5	20	Parz.	Parz.
544.05	19.03	96.00	0.198	21.63	96.00	0.225	371.92	463.46	5	(22+23)-VI-3	Parz.	Parz.
FLN	18.97	96.00	0.198	21.63	96.00	0.225	371.92	463.46	(22+23)-V-2	(22+23)-VI-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=4 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	223.66	--	1523.88	339.88	339.88	7.50	0.00	463.46	151.00	10.40	0.00	1.5
Cen	120.91	--	1523.88	264.12	264.12	--	--	--	--	7.81	--	2.2
Des	188.41	--	1523.88	339.88	339.88	8.74	0.00	371.92	151.00	10.46	0.00	1.8

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.17

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	7.50	326.62	223.66	1523.88	0.17
Des.	8.74	326.62	188.41	1523.88	0.15

Trave di fondazione: 9008 [29,30], Pilastrate [29,30] Sez. R: By=50.00 cm Bz=100.00 cm L=534.50 cm Ln=534.50 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	84.34	249.31	28.94	--	10.18	10.18	371.93	371.93	(22+23)-V-3	20	1.5
53.45	103.54	189.40	10.51	59.91	10.18	10.18	371.93	371.93	(22+23)-V-3	20	1.5
CAMP	114.20	141.93	--	107.38	10.18	10.18	371.93	371.93	(22+23)-V-3	20	1.5
481.05	73.87	105.55	4.93	33.61	10.18	10.18	371.93	371.93	(22+23)-V-2	20	2.7
FLN	78.80	139.16	--	--	10.18	10.18	371.93	371.93	(22+23)-V-2	20	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.48	96.00	0.203	19.72	96.00	0.205	371.93	371.93	(22+23)-V-3	20	Parz.	Parz.
53.45	19.48	96.00	0.203	19.72	96.00	0.205	371.93	371.93	(22+23)-V-3	20	Parz.	Parz.
CAMP	19.48	96.00	0.203	19.72	96.00	0.205	371.93	371.93	(22+23)-V-3	20	Parz.	Parz.
481.05	19.42	96.00	0.202	19.52	96.00	0.203	371.93	371.93	(22+23)-V-2	20	Parz.	Parz.
FLN	19.42	96.00	0.202	19.52	96.00	0.203	371.93	371.93	(22+23)-V-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=(22+23)-V-2 Des=(22+23)-V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/	cmq	

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
										m		
Sin	124.24	--	1523.88	339.88	339.88	18.97	0.00	371.93	151.00	10.93	0.00	2.7
Cen	64.76	--	1523.88	263.99	263.99	--	--	--	--	7.81	--	4.1
Des	99.69	--	1523.88	339.88	339.88	18.39	0.00	371.93	151.00	10.90	0.00	3.4

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.14

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	18.97	326.62	124.24	1523.88	0.14
Des.	18.39	326.62	99.69	1523.88	0.12

Trave di fondazione: 9008 [30,31], Pilastrate [30,31] Sez. R: By=50.00 cm Bz=100.00 cm L=614.50 cm Ln=614.50 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	27.92	336.00	34.91	--	10.18	10.18	371.93	371.93	(22+23)-VI-3	20	1.1
61.45	51.53	246.22	19.83	89.78	10.18	10.18	371.93	371.93	(22+23)-VI-3	20	1.1
CAMP	127.91	169.80	--	144.43	10.18	10.18	371.93	371.93	(22+23)-V-2	20	1.2
553.05	119.23	128.84	--	58.51	10.18	10.18	371.93	371.93	(22+23)-V-2	(22+23)-V-3	2.0
FLN	85.10	187.35	30.47	--	10.18	10.18	371.93	371.93	(22+23)-VII-2	(22+23)-V-3	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.39	96.00	0.202	19.88	96.00	0.207	371.93	371.93	(22+23)-VI-3	20	Parz.	Parz.
61.45	19.41	96.00	0.202	19.88	96.00	0.207	371.93	371.93	(22+23)-VI-3	20	Parz.	Parz.
CAMP	19.50	96.00	0.203	19.84	96.00	0.207	371.93	371.93	(22+23)-V-2	20	Parz.	Parz.
553.05	19.49	96.00	0.203	19.61	96.00	0.204	371.93	371.93	(22+23)-V-2	(22+23)-V-3	Parz.	Parz.
FLN	19.48	96.00	0.203	19.61	96.00	0.204	371.93	371.93	(22+23)-VII-2	(22+23)-V-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-VI-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	156.86	--	1523.88	339.88	339.88	15.37	0.00	371.93	151.00	10.76	0.00	2.2
Cen	91.33	--	1523.88	263.99	263.99	--	--	--	--	7.81	--	2.9
Des	130.53	--	1523.88	339.88	339.88	16.65	0.00	371.93	151.00	10.82	0.00	2.6

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	15.37	326.62	156.86	1523.88	0.15
Des.	16.65	326.62	130.53	1523.88	0.14

Trave di fondazione: 9009 [2,15], Pilastrate [2,15] Sez. R: By=50.00 cm Bz=100.00 cm L=481.60 cm Ln=481.60 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	167.31	191.48	--	--	10.18	10.18	371.93	371.93	(22+23)-III-2	(24+25)-III-3	1.9
48.16	137.41	140.25	29.90	51.23	10.18	10.18	371.93	371.93	(22+23)-III-2	(24+25)-III-3	1.9
CAMP	108.75	151.67	58.56	79.68	10.18	10.18	371.93	371.93	(22+23)-III-2	20	1.6
433.44	30.05	188.77	--	42.59	10.18	10.18	371.93	371.93	(24+25)-III-3	20	1.6
FLN	24.90	231.35	--	--	10.18	10.18	371.93	371.93	(24+25)-III-3	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.57	96.00	0.204	19.61	96.00	0.204	371.93	371.93	(22+23)-III-2	(24+25)-III-3	Parz.	Parz.
48.16	19.57	96.00	0.204	19.61	96.00	0.204	371.93	371.93	(22+23)-III-2	(24+25)-III-3	Parz.	Parz.
CAMP	19.57	96.00	0.204	19.68	96.00	0.205	371.93	371.93	(22+23)-III-2	20	Parz.	Parz.
433.44	19.34	96.00	0.201	19.68	96.00	0.205	371.93	371.93	(24+25)-III-3	20	Parz.	Parz.
FLN	19.33	96.00	0.201	19.68	96.00	0.205	371.93	371.93	(24+25)-III-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(24+25)-III-3 Cen=(22+23)-III-2 Des=20

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	114.85	--	1523.88	339.88	339.88	26.26	0.00	371.93	151.00	11.26	0.00	3.0
Cen	56.54	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.6
Des	94.21	--	1523.88	339.88	339.88	24.61	0.00	371.93	151.00	11.18	0.00	3.6

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	26.26	326.62	114.85	1523.88	0.15
Des.	24.61	326.62	94.21	1523.88	0.14

Trave di fondazione: 9009 [15,21], Pilastrate [15,21] Sez. R: By=50.00 cm Bz=100.00 cm L=430.70 cm Ln=430.70 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	60.73	248.39	--	--	10.18	10.18	371.93	371.93	(24+25)-VIII-4	20	1.5
43.07	57.36	224.97	3.38	23.42	10.18	10.18	371.93	371.93	(24+25)-VIII-4	20	1.5
CAMP	76.66	206.06	15.50	42.34	10.18	10.18	371.93	371.93	(24+25)-IV-3	20	1.5
387.63	85.86	201.60	6.30	18.10	10.18	10.18	371.93	371.93	(24+25)-IV-3	20	1.7
FLN	92.16	219.71	--	--	10.18	10.18	371.93	371.93	(24+25)-IV-3	20	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.39	96.00	0.202	19.71	96.00	0.205	371.93	371.93	(24+25)-VIII-4	20	Parz.	Parz.
43.07	19.39	96.00	0.202	19.71	96.00	0.205	371.93	371.93	(24+25)-VIII-4	20	Parz.	Parz.
CAMP	19.44	96.00	0.203	19.71	96.00	0.205	371.93	371.93	(24+25)-IV-3	20	Parz.	Parz.
387.63	19.44	96.00	0.203	19.66	96.00	0.205	371.93	371.93	(24+25)-IV-3	20	Parz.	Parz.
FLN	19.44	96.00	0.203	19.66	96.00	0.205	371.93	371.93	(24+25)-IV-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-IV-3 Cen=(24+25)-IV-2 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	80.51	--	1523.88	339.88	339.88	6.92	0.00	371.93	151.00	10.37	0.00	4.2
Cen	53.29	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.9
Des	86.34	--	1523.88	339.88	339.88	7.16	0.00	371.93	151.00	10.38	0.00	3.9

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.08

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	6.92	326.62	80.51	1523.88	0.07
Des.	7.16	326.62	86.34	1523.88	0.08

Trave di fondazione: 9009 [21,24], Pilastrate [21,24] Sez. R: By=50.00 cm Bz=100.00 cm L=287.70 cm Ln=287.70 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	17.81	235.94	23.79	--	10.18	10.18	371.93	371.93	(22+23)-V-3	20	1.6
28.77	23.65	217.07	19.70	18.87	10.18	10.18	371.93	371.93	(22+23)-VII-3	20	1.6
CAMP	57.01	185.86	4.31	50.08	10.18	10.18	371.93	371.93	(22+23)-IV-3	20	1.6
258.93	60.14	150.39	1.19	22.47	10.18	10.18	371.93	371.93	(22+23)-IV-3	6	2.2
FLN	61.33	147.19	--	18.14	10.18	10.18	371.93	371.93	(22+23)-IV-3	6	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.36	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-V-3	20	Parz.	Parz.
28.77	19.36	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-VII-3	20	Parz.	Parz.
CAMP	19.39	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-IV-3	20	Parz.	Parz.
258.93	19.39	96.00	0.202	19.58	96.00	0.204	371.93	371.93	(22+23)-IV-3	6	Parz.	Parz.
FLN	19.39	96.00	0.202	19.57	96.00	0.204	371.93	371.93	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=20 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	69.37	--	1523.88	339.88	339.88	7.23	0.00	371.93	143.85	10.39	0.00	4.9
Des	54.07	--	1523.88	339.88	339.88	6.73	0.00	371.93	143.85	10.36	0.00	6.3

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.07

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	7.23	326.62	69.37	1523.88	0.07
Des.	6.73	326.62	54.07	1523.88	0.06

Trave di fondazione: 9009 [24,29], Pilastrate [24,29] Sez. R: By=50.00 cm Bz=100.00 cm L=439.90 cm Ln=439.90 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	44.04	235.47	17.98	--	10.18	10.18	371.93	371.93	(22+23)-VII-4	20	1.6
43.99	54.40	184.44	8.35	51.02	10.18	10.18	371.93	371.93	(22+23)-VII-4	20	1.6
CAMP	63.38	138.97	--	96.49	10.18	10.18	371.93	371.93	(22+23)-VII-4	20	1.6
395.91	40.89	33.71	9.68	22.75	10.18	10.18	371.93	371.93	(22+23)-IV-3	(22+23)-VIII-4	6.6
FLN	18.40	56.46	31.92	--	10.18	10.18	371.93	371.93	(22+23)-IV-3	(22+23)-VIII-4	6.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.39	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-VII-4	20	Parz.	Parz.
43.99	19.39	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-VII-4	20	Parz.	Parz.
CAMP	19.39	96.00	0.202	19.69	96.00	0.205	371.93	371.93	(22+23)-VII-	20	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
									4			
395.91	19.37	96.00	0.202	19.38	96.00	0.202	371.93	371.93	(22+23)-IV-3	(22+23)-VIII-4	Parz.	Parz.
FLN	19.37	96.00	0.202	19.38	96.00	0.202	371.93	371.93	(22+23)-IV-3	(22+23)-VIII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	122.22	--	1523.88	339.88	339.88	18.53	0.00	371.93	151.00	10.91	0.00	2.8
Cen	70.61	--	1523.88	272.45	272.45	--	--	--	--	8.06	--	3.9
Des	85.45	--	1523.88	339.88	339.88	19.90	0.00	371.93	151.00	10.97	0.00	4.0

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.14

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	18.53	326.62	122.22	1523.88	0.14
Des.	19.90	326.62	85.45	1523.88	0.12

Trave di fondazione: 9010 [13,22], Pilastrate [13,22] Sez. R: By=50.00 cm Bz=100.00 cm L=466.53 cm Ln=460.87 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	74.65	220.68	--	--	12.72	12.72	463.51	463.51	(24+25)-IV-2	20	2.1
46.09	74.51	190.72	0.15	29.96	12.72	12.72	463.51	463.51	(24+25)-IV-2	20	2.1
CAMP	67.15	267.45	7.50	118.47	12.72	12.72	463.51	463.51	(24+25)-IV-2	20	1.2
414.78	31.09	321.10	13.03	64.81	12.72	12.72	463.51	463.51	(22+23)-IV-3	20	1.2
FLN	11.98	385.91	31.17	--	12.72	12.72	463.51	463.51	(22+23)-IV-3	20	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.08	96.00	0.220	21.32	96.00	0.222	463.51	463.51	(24+25)-IV-2	20	Parz.	Parz.
46.09	21.08	96.00	0.220	21.32	96.00	0.222	463.51	463.51	(24+25)-IV-2	20	Parz.	Parz.
CAMP	21.08	96.00	0.220	21.60	96.00	0.225	463.51	463.51	(24+25)-IV-2	20	Parz.	Parz.
414.78	21.04	96.00	0.219	21.60	96.00	0.225	463.51	463.51	(22+23)-IV-3	20	Parz.	Parz.
FLN	21.04	96.00	0.219	21.60	96.00	0.225	463.51	463.51	(22+23)-IV-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-IV-3 Cen=(22+23)-IV-2 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	114.93	--	1523.88	339.88	339.88	21.08	0.00	463.51	151.00	11.02	0.00	3.0
Cen	92.31	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	2.8
Des	175.02	--	1523.88	339.88	339.88	23.81	0.00	463.51	151.00	11.15	0.00	1.9

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.19

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	21.08	326.62	114.93	1523.88	0.14
Des.	23.81	326.62	175.02	1523.88	0.19

Trave di fondazione: 9010 [22,25], Pilastrate [22,25] Sez. R: By=50.00 cm Bz=100.00 cm L=289.26 cm Ln=287.70 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	356.92	--	--	12.72	12.72	463.51	463.51	1	20	1.3
28.77	--	317.53	--	39.40	12.72	12.72	463.51	463.51	1	20	1.3
CAMP	7.72	251.73	--	105.19	12.72	12.72	463.51	463.51	(24+25)-VIII-1	20	1.3
258.93	5.90	155.02	--	43.51	12.72	12.72	463.51	463.51	(24+25)-IV-1	20	2.3
FLN	1.50	153.07	--	28.36	12.72	12.72	463.51	463.51	(24+25)-IV-1	20	2.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	--	--	--	21.55	96.00	0.224	463.51	463.51	1	20	--	Parz.
28.77	--	--	--	21.55	96.00	0.224	463.51	463.51	1	20	--	Parz.
CAMP	20.98	96.00	0.219	21.55	96.00	0.224	463.51	463.51	(24+25)-VIII-1	20	Parz.	Parz.
258.93	20.98	96.00	0.219	21.28	96.00	0.222	463.51	463.51	(24+25)-IV-1	20	Parz.	Parz.
FLN	20.97	96.00	0.218	21.25	96.00	0.221	463.51	463.51	(24+25)-IV-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	144.52	--	1523.88	378.04	378.04	56.46	0.00	463.51	143.85	13.78	0.00	2.6
Des	56.86	--	1523.88	339.88	339.88	55.01	0.00	463.51	143.85	12.58	0.00	6.0

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.27

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	56.46	326.62	144.52	1523.88	0.27
Des.	55.01	326.62	56.86	1523.88	0.20

Trave di fondazione: 9010 [25,30], Pilastrate [25,30] Sez. R: By=50.00 cm Bz=100.00 cm L=440.01 cm Ln=440.13 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	40.69	311.44	24.41	--	10.18	10.18	371.93	371.93	(22+23)-IV-2	20	1.2
44.01	55.00	237.14	11.01	74.30	10.18	10.18	371.93	371.93	(22+23)-IV-2	20	1.2
CAMP	66.87	171.86	--	139.58	10.18	10.18	371.93	371.93	(22+23)-IV-2	20	1.2
396.11	36.37	17.13	28.38	29.85	10.18	10.18	371.93	371.93	5	(22+23)-IV-2	5.7
FLN	7.69	46.98	52.09	--	10.18	10.18	371.93	371.93	5	(22+23)-IV-2	6.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.40	96.00	0.202	19.83	96.00	0.207	371.93	371.93	(22+23)-IV-2	20	Parz.	Parz.
44.01	19.40	96.00	0.202	19.83	96.00	0.207	371.93	371.93	(22+23)-IV-2	20	Parz.	Parz.
CAMP	19.40	96.00	0.202	19.83	96.00	0.207	371.93	371.93	(22+23)-IV-2	20	Parz.	Parz.
396.11	19.40	96.00	0.202	19.37	96.00	0.202	371.93	371.93	5	(22+23)-IV-2	Parz.	Parz.
FLN	19.39	96.00	0.202	19.37	96.00	0.202	371.93	371.93	5	(22+23)-IV-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	181.12	--	1523.88	339.88	339.88	17.42	0.00	371.93	151.00	10.85	0.00	1.9
Cen	99.09	--	1523.88	272.45	272.45	--	--	--	--	8.06	--	2.7
Des	75.96	--	1523.88	339.88	339.88	17.49	0.00	371.93	151.00	10.86	0.00	4.5

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.17

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	17.42	326.62	181.12	1523.88	0.17
Des.	17.49	326.62	75.96	1523.88	0.10

Trave di fondazione: 9011 [23,26], Pilastrate [23,26] Sez. R: By=50.00 cm Bz=100.00 cm L=142.97 cm Ln=188.74 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	487.37	--	--	10.18	15.27	371.91	554.79	1	20	1.1
18.87	--	450.99	--	36.38	10.18	15.27	371.91	554.79	1	20	1.1
CAMP	-0.25	329.88	6.57	157.49	10.18	15.27	371.91	554.79	(24+25)-VI-2	20	1.1
169.86	3.64	248.17	2.68	129.32	10.18	15.27	371.91	554.79	(24+25)-VI-2	20	1.5
FLN	6.32	234.58	--	114.53	10.18	15.27	371.91	554.79	(24+25)-VI-2	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	--	--	--	24.22	96.00	0.252	371.91	554.79	1	20	--	Parz.
18.87	--	--	--	24.22	96.00	0.252	371.91	554.79	1	20	--	Parz.
CAMP	18.42	96.00	0.192	24.22	96.00	0.252	371.91	554.79	(24+25)-VI-2	20	Parz.	Parz.
169.86	18.42	96.00	0.192	24.00	96.00	0.250	371.91	554.79	(24+25)-VI-2	20	Parz.	Parz.
FLN	18.42	96.00	0.192	23.94	96.00	0.249	371.91	554.79	(24+25)-VI-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: 20

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	199.20	--	1523.88	430.68	430.68	89.31	0.00	554.79	188.74	16.85	0.00	2.2
Des								371.91				

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.41

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	89.31	326.62	199.20	1523.88	0.40
Des.	90.48	326.62	199.20	1523.88	0.41

Trave di fondazione: 9011 [26,31], Pilastrate [26,31] Sez. R: By=50.00 cm Bz=100.00 cm L=439.90 cm Ln=439.90 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	86.71	382.01	--	--	10.18	15.27	371.91	554.79	(24+25)-VI-2	20	1.5
43.99	93.42	286.40	--	95.61	10.18	15.27	371.91	554.79	(24+25)-VI-2	20	1.5
CAMP	95.22	203.44	--	178.57	10.18	15.27	371.91	554.79	(24+25)-VI-2	20	1.5
395.91	71.48	13.95	11.05	39.99	10.18	15.27	371.91	554.79	(22+23)-VI-3	(24+25)-VI-2	4.5
FLN	82.52	53.95	--	--	10.18	15.27	371.91	554.79	(22+23)-VI-3	(24+25)-VI-2	4.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	18.53	96.00	0.193	24.00	96.00	0.250	371.91	554.79	(24+25)-VI-2	20	Parz.	Parz.
43.99	18.54	96.00	0.193	24.00	96.00	0.250	371.91	554.79	(24+25)-VI-2	20	Parz.	Parz.
CAMP	18.54	96.00	0.193	24.00	96.00	0.250	371.91	554.79	(24+25)-VI-2	20	Parz.	Parz.
395.91	18.53	96.00	0.193	23.41	96.00	0.244	371.91	554.79	(22+23)-VI-3	(24+25)-VI-2	Parz.	Parz.
FLN	18.53	96.00	0.193	23.41	96.00	0.244	371.91	554.79	(22+23)-VI-3	(24+25)-VI-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	231.93	--	1523.88	339.88	339.88	30.01	0.00	554.79	151.00	11.43	0.00	1.5
Cen	119.90	--	1523.88	272.45	272.45	--	--	--	--	8.06	--	2.3
Des	86.53	--	1523.88	339.88	339.88	29.85	0.00	371.91	151.00	11.43	0.00	3.9

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.24

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	30.01	326.62	231.93	1523.88	0.24
Des.	29.85	326.62	86.53	1523.88	0.15

Trave di fondazione: 9012 [2,8], Pilastrate [2,8] Sez. R: By=50.00 cm Bz=100.00 cm L=368.36 cm Ln=252.48 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	217.63	169.59	--	--	12.72	10.18	463.46	371.92	(22+23)-I-4	(24+25)-I-1	2.1
25.25	208.39	151.21	9.24	18.38	12.72	10.18	463.46	371.92	(22+23)-I-4	(24+25)-I-1	2.1
CAMP	167.69	99.96	49.94	69.63	12.72	10.18	463.46	371.92	(22+23)-I-4	(24+25)-I-1	2.1
227.23	64.02	27.28	90.85	61.44	12.72	10.18	463.46	371.92	(22+23)-I-4	(24+25)-I-1	3.0
FLN	39.33	81.64	96.62	--	12.72	10.18	463.46	371.92	(22+23)-I-4	6	3.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.80	96.00	0.227	19.10	96.00	0.199	463.46	371.92	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
25.25	21.80	96.00	0.227	19.10	96.00	0.199	463.46	371.92	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	21.80	96.00	0.227	19.10	96.00	0.199	463.46	371.92	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
227.23	21.69	96.00	0.226	18.98	96.00	0.198	463.46	371.92	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
FLN	21.66	96.00	0.226	18.97	96.00	0.198	463.46	371.92	(22+23)-I-4	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-III-2 Des=(22+23)-III-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	82.61	--	1523.88	350.01	350.01	27.13	0.00	371.92	126.24	11.60	0.00	4.2
Des	104.58	--	1523.88	350.01	350.01	26.66	0.00	463.46	126.24	11.58	0.00	3.3

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	27.13	326.62	82.61	1523.88	0.14
Des.	26.66	326.62	104.58	1523.88	0.15

Trave di fondazione: 9012 [8,13], Pilastrate [8,13] Sez. R: By=50.00 cm Bz=100.00 cm L=327.82 cm Ln=327.82 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	77.09	103.64	--	--	12.72	10.18	463.46	371.92	(24+25)-VIII-4	21	3.6
32.78	77.92	98.70	--	5.63	12.72	10.18	463.46	371.92	(22+23)-VIII-4	6	3.6
CAMP	82.68	121.51	11.25	17.66	12.72	10.18	463.46	371.92	(22+23)-VIII-1	6	2.7
295.03	89.84	129.68	4.08	9.49	12.72	10.18	463.46	371.92	(22+23)-VIII-1	6	2.7
FLN	93.92	139.17	--	--	12.72	10.18	463.46	371.92	(22+23)-VIII-1	6	2.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.56	96.00	0.225	19.00	96.00	0.198	463.46	371.92	(24+25)-VIII-4	21	Parz.	Parz.
32.78	21.56	96.00	0.225	19.00	96.00	0.198	463.46	371.92	(22+23)-VIII-4	6	Parz.	Parz.
CAMP	21.59	96.00	0.225	19.05	96.00	0.198	463.46	371.92	(22+23)-VIII-1	6	Parz.	Parz.
295.03	21.59	96.00	0.225	19.05	96.00	0.198	463.46	371.92	(22+23)-VIII-1	6	Parz.	Parz.
FLN	21.59	96.00	0.225	19.05	96.00	0.198	463.46	371.92	(22+23)-VIII-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-1 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	88.59	--	1523.88	339.88	339.88	26.49	0.00	371.92	163.91	11.27	0.00	3.8
Des	105.10	--	1523.88	339.88	339.88	26.22	0.00	463.46	163.91	11.26	0.00	3.2

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	26.49	326.62	88.59	1523.88	0.14
Des.	26.22	326.62	105.10	1523.88	0.15

Trave di fondazione: 9012 [13,16], Pilastrate [13,16] Sez. R: By=50.00 cm Bz=100.00 cm L=329.87 cm Ln=329.87 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	60.51	209.67	--	--	12.72	12.72	463.51	463.51	(22+23)-III-3	20	2.2
32.99	62.10	193.17	--	16.49	12.72	12.72	463.51	463.51	(22+23)-III-3	20	2.2
CAMP	42.73	231.49	18.94	66.28	12.72	12.72	463.51	463.51	(22+23)-III-3	20	1.6
296.88	-74.12	261.28	90.61	36.48	12.72	12.72	463.51	463.51	(22+23)-IV-3	20	1.6
FLN	--	297.77	--	--	12.72	12.72	463.51	463.51	1	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.06	96.00	0.219	21.30	96.00	0.222	463.51	463.51	(22+23)-III-3	20	Parz.	Parz.
32.99	21.06	96.00	0.219	21.30	96.00	0.222	463.51	463.51	(22+23)-III-3	20	Parz.	Parz.
CAMP	21.06	96.00	0.219	21.45	96.00	0.223	463.51	463.51	(22+23)-III-3	20	Parz.	Parz.
296.88	21.00	96.00	0.219	21.45	96.00	0.223	463.51	463.51	(22+23)-IV-3	20	Parz.	Parz.
FLN	--	--	--	21.45	96.00	0.223	463.51	463.51	1	20	--	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-III-2 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	68.24	--	1523.88	339.88	339.88	37.75	0.00	463.51	164.93	11.79	0.00	5.0
Des	145.95	--	1523.88	339.88	339.88	37.56	0.00	463.51	164.93	11.78	0.00	2.3

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.21

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	37.75	326.62	68.24	1523.88	0.16
Des.	37.56	326.62	145.95	1523.88	0.21

Trave di fondazione: 9012 [16,23], Pilastrate [16,23] Sez. R: By=50.00 cm Bz=100.00 cm L=532.52 cm Ln=532.52 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-19.12	395.14	45.52	--	10.18	12.72	371.92	463.46	(24+25)-VIII-4	20	1.2
53.25	7.82	310.81	28.06	84.33	10.18	12.72	371.92	463.46	(24+25)-VIII-4	20	1.2
CAMP	67.23	240.97	--	154.17	10.18	12.72	371.92	463.46	(22+23)-VII-1	20	1.2
479.27	37.11	194.61	29.88	63.60	10.18	12.72	371.92	463.46	(22+23)-VII-1	20	1.8
FLN	10.63	258.21	49.57	--	10.18	12.72	371.92	463.46	(24+25)-VII-1	20	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	18.88	96.00	0.197	22.14	96.00	0.231	371.92	463.46	(24+25)-VIII-4	20	Parz.	Parz.
53.25	18.90	96.00	0.197	22.14	96.00	0.231	371.92	463.46	(24+25)-VIII-4	20	Parz.	Parz.
CAMP	18.94	96.00	0.197	22.14	96.00	0.231	371.92	463.46	(22+23)-VII-1	20	Parz.	Parz.
479.27	18.94	96.00	0.197	21.88	96.00	0.228	371.92	463.46	(22+23)-VII-1	20	Parz.	Parz.
FLN	18.93	96.00	0.197	21.88	96.00	0.228	371.92	463.46	(24+25)-VII-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=4 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	188.22	--	1523.88	339.88	339.88	17.00	0.00	463.46	151.00	10.84	0.00	1.8
Cen	93.52	--	1523.88	262.34	262.34	--	--	--	--	7.76	--	2.8
Des	164.72	--	1523.88	339.88	339.88	17.02	0.00	371.92	151.00	10.84	0.00	2.1

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.17

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	17.00	326.62	188.22	1523.88	0.17
Des.	17.02	326.62	164.72	1523.88	0.16

Trave di fondazione: 9013 [3,9], Pilastrate [3,9] Sez. R: By=50.00 cm Bz=100.00 cm L=327.85 cm Ln=327.85 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	94.83	57.28	--	22.07	12.72	10.18	463.46	371.92	(24+25)-I-4	6	4.7
32.79	88.69	61.30	6.14	29.37	12.72	10.18	463.46	371.92	(24+25)-I-4	6	4.1
CAMP	66.95	152.69	27.88	79.37	12.72	10.18	463.46	371.92	(24+25)-I-4	20	1.6
295.07	34.04	189.43	--	42.64	12.72	10.18	463.46	371.92	(24+25)-VII-1	20	1.6
FLN	29.76	232.07	--	--	12.72	10.18	463.46	371.92	(24+25)-VII-1	20	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.59	96.00	0.225	18.96	96.00	0.198	463.46	371.92	(24+25)-I-4	6	Parz.	Parz.
32.79	21.59	96.00	0.225	18.98	96.00	0.198	463.46	371.92	(24+25)-I-4	6	Parz.	Parz.
CAMP	21.59	96.00	0.225	19.20	96.00	0.200	463.46	371.92	(24+25)-I-4	20	Parz.	Parz.
295.07	21.49	96.00	0.224	19.20	96.00	0.200	463.46	371.92	(24+25)-VII-1	20	Parz.	Parz.
FLN	21.48	96.00	0.224	19.20	96.00	0.200	463.46	371.92	(24+25)-VII-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-I-1 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	75.05	--	1523.88	339.88	339.88	10.54	0.00	371.92	163.93	10.54	0.00	4.5
Des	139.47	--	1523.88	339.88	339.88	10.24	0.00	463.46	163.93	10.52	0.00	2.4

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.12

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	10.54	326.62	75.05	1523.88	0.08
Des.	10.24	326.62	139.47	1523.88	0.12

Trave di fondazione: 9013 [9,14], Pilastrate [9,14] Sez. R: By=50.00 cm Bz=100.00 cm L=329.87 cm Ln=329.87 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-41.31	370.81	48.69	--	12.72	12.72	463.51	463.51	(22+23)-VIII-4	20	1.2
32.99	-20.83	316.05	33.04	54.76	12.72	12.72	463.51	463.51	(22+23)-VIII-4	20	1.2
CAMP	13.59	225.30	--	145.51	12.72	12.72	463.51	463.51	(22+23)-IV-2	20	1.2
296.88	-22.94	85.21	35.57	62.46	12.72	12.72	463.51	463.51	(22+23)-IV-2	6	3.1
FLN	-44.46	112.82	52.77	13.64	12.72	12.72	463.51	463.51	(22+23)-IV-2	20	3.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	20.98	96.00	0.219	21.58	96.00	0.225	463.51	463.51	(22+23)-VIII-4	20	Parz.	Parz.
32.99	20.99	96.00	0.219	21.58	96.00	0.225	463.51	463.51	(22+23)-VIII-4	20	Parz.	Parz.
CAMP	20.99	96.00	0.219	21.58	96.00	0.225	463.51	463.51	(22+23)-IV-2	20	Parz.	Parz.
296.88	20.99	96.00	0.219	21.20	96.00	0.221	463.51	463.51	(22+23)-IV-2	6	Parz.	Parz.
FLN	20.98	96.00	0.219	21.17	96.00	0.220	463.51	463.51	(22+23)-IV-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	175.36	--	1523.88	339.88	339.88	32.44	0.00	463.51	164.93	11.55	0.00	1.9
Des	99.23	--	1523.88	339.88	339.88	31.42	0.00	463.51	164.93	11.50	0.00	3.4

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.21

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	32.44	326.62	175.36	1523.88	0.21

	TEd	TRcd	VEd	VRcd	ρ
Des.	31.42	326.62	99.23	1523.88	0.16

Trave di fondazione: 9013 [14,17], Pilastrate [14,17] Sez. R: By=50.00 cm Bz=100.00 cm L=532.52 cm Ln=532.52 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-6.76	383.84	52.76	--	10.18	12.72	371.92	463.46	(24+25)-VII-4	20	1.2
53.25	17.89	299.88	40.71	83.97	10.18	12.72	371.92	463.46	(22+23)-VII-4	20	1.2
CAMP	66.94	230.78	--	153.07	10.18	12.72	371.92	463.46	5	20	1.2
479.27	10.01	194.64	38.84	65.20	10.18	12.72	371.92	463.46	(22+23)-VI-1	20	1.8
FLN	-21.85	259.83	59.10	--	10.18	12.72	371.92	463.46	(24+25)-VI-1	20	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	18.91	96.00	0.197	22.12	96.00	0.230	371.92	463.46	(24+25)-VII-4	20	Parz.	Parz.
53.25	18.93	96.00	0.197	22.12	96.00	0.230	371.92	463.46	(22+23)-VII-4	20	Parz.	Parz.
CAMP	18.94	96.00	0.197	22.12	96.00	0.230	371.92	463.46	5	20	Parz.	Parz.
479.27	18.92	96.00	0.197	21.88	96.00	0.228	371.92	463.46	(22+23)-VI-1	20	Parz.	Parz.
FLN	18.90	96.00	0.197	21.88	96.00	0.228	371.92	463.46	(24+25)-VI-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=4 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	191.99	--	1523.88	339.88	339.88	24.61	0.00	463.46	151.00	11.18	0.00	1.8
Cen	93.81	--	1523.88	262.33	262.33	--	--	--	--	7.76	--	2.8
Des	169.73	--	1523.88	339.88	339.88	24.97	0.00	371.92	151.00	11.20	0.00	2.0

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.20

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	24.61	326.62	191.99	1523.88	0.20
Des.	24.97	326.62	169.73	1523.88	0.19

Trave di fondazione: 9014 [17,23], Pilastrate [17,23] Sez. R: By=50.00 cm Bz=100.00 cm L=310.00 cm Ln=310.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	481.01	--	--	10.18	15.27	371.91	554.79	1	20	1.2
31.00	--	431.14	--	49.87	10.18	15.27	371.91	554.79	1	20	1.2
CAMP	16.45	353.31	12.18	127.70	10.18	15.27	371.91	554.79	(24+25)-VI-3	20	1.2
279.00	25.04	297.14	3.59	16.38	10.18	15.27	371.91	554.79	(24+25)-VI-3	20	1.8
FLN	28.63	313.52	--	--	10.18	15.27	371.91	554.79	(24+25)-VI-3	20	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	--	--	--	24.21	96.00	0.252	371.91	554.79	1	20	--	Parz.
31.00	--	--	--	24.21	96.00	0.252	371.91	554.79	1	20	--	Parz.
CAMP	18.45	96.00	0.192	24.21	96.00	0.252	371.91	554.79	(24+25)-VI-3	20	Parz.	Parz.
279.00	18.45	96.00	0.192	23.87	96.00	0.249	371.91	554.79	(24+25)-VI-3	20	Parz.	Parz.
FLN	18.45	96.00	0.192	23.87	96.00	0.249	371.91	554.79	(24+25)-VI-	20	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
									3			

Verifica a taglio: cot(θ) =1.000 Comb: 20

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	172.56	--	1523.88	339.89	339.89	12.06	0.00	554.79	310.00	10.61	0.00	2.0
Des								371.91				

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	12.06	326.62	172.56	1523.88	0.15
Des.	12.69	326.62	172.56	1523.88	0.15

Trave di fondazione: 9015 [14,16], Pilastrate [14,16] Sez. R: By=50.00 cm Bz=100.00 cm L=310.00 cm Ln=310.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-58.56	203.96	67.96	--	10.18	10.18	371.93	371.93	(22+23)-III-3	20	1.8
31.00	-33.81	166.03	52.53	37.92	10.18	10.18	371.93	371.93	(22+23)-III-3	20	1.8
CAMP	29.37	109.00	--	94.96	10.18	10.18	371.93	371.93	(22+23)-IV-3	20	1.8
279.00	19.32	85.05	--	17.41	10.18	10.18	371.93	371.93	(24+25)-IV-3	20	3.6
FLN	-19.10	102.47	36.70	--	10.18	10.18	371.93	371.93	(22+23)-I-4	20	3.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.31	96.00	0.201	19.64	96.00	0.205	371.93	371.93	(22+23)-III-3	20	Parz.	Parz.
31.00	19.32	96.00	0.201	19.64	96.00	0.205	371.93	371.93	(22+23)-III-3	20	Parz.	Parz.
CAMP	19.34	96.00	0.201	19.64	96.00	0.205	371.93	371.93	(22+23)-IV-3	20	Parz.	Parz.
279.00	19.32	96.00	0.201	19.46	96.00	0.203	371.93	371.93	(24+25)-IV-3	20	Parz.	Parz.
FLN	19.32	96.00	0.201	19.46	96.00	0.203	371.93	371.93	(22+23)-I-4	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=4 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	146.44	--	1523.88	339.88	339.88	8.44	0.00	371.93	155.00	10.44	0.00	2.3
Des	86.86	--	1523.88	339.88	339.88	8.91	0.00	371.93	155.00	10.46	0.00	3.9

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.12

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	8.44	326.62	146.44	1523.88	0.12
Des.	8.91	326.62	86.86	1523.88	0.08

Trave di fondazione: 9016 [9,13], Pilastrate [9,13] Sez. R: By=50.00 cm Bz=100.00 cm L=310.56 cm Ln=310.56 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	2.67	-12.60	31.78	85.23	10.18	10.18	371.93	371.93	(22+23)-VI-2	6	5.1
31.06	17.11	9.64	17.60	91.14	10.18	10.18	371.93	371.93	(22+23)-VI-2	6	3.7
CAMP	41.90	218.15	--	100.81	10.18	10.18	371.93	371.93	(22+23)-IV-2	20	1.2
279.51	-12.07	266.29	47.05	52.67	10.18	10.18	371.93	371.93	(22+23)-IV-2	20	1.2

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
FLN	-33.11	318.96	58.96	--	10.18	10.18	371.93	371.93	(22+23)-IV-2	20	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.35	96.00	0.202	19.41	96.00	0.202	371.93	371.93	(22+23)-VI-2	6	Parz.	Parz.
31.06	19.35	96.00	0.202	19.46	96.00	0.203	371.93	371.93	(22+23)-VI-2	6	Parz.	Parz.
CAMP	19.36	96.00	0.202	19.85	96.00	0.207	371.93	371.93	(22+23)-IV-2	20	Parz.	Parz.
279.51	19.35	96.00	0.202	19.85	96.00	0.207	371.93	371.93	(22+23)-IV-2	20	Parz.	Parz.
FLN	19.33	96.00	0.201	19.85	96.00	0.207	371.93	371.93	(22+23)-IV-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=20 Des=20

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	101.81	--	1523.88	339.88	339.88	10.10	0.00	371.93	155.28	10.52	0.00	3.3
Des	176.80	--	1523.88	339.88	339.88	10.74	0.00	371.93	155.28	10.55	0.00	1.9

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	10.10	326.62	101.81	1523.88	0.10
Des.	10.74	326.62	176.80	1523.88	0.15

Trave di fondazione: 9017 [3,8], Pilastrate [3,8] Sez. R: By=50.00 cm Bz=100.00 cm L=305.05 cm Ln=305.05 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	90.33	68.54	--	--	10.18	10.18	371.93	371.93	(22+23)-III-2	6	4.1
30.50	77.73	66.21	12.60	8.22	10.18	10.18	371.93	371.93	(22+23)-III-2	6	4.1
CAMP	46.60	92.24	43.72	36.86	10.18	10.18	371.93	371.93	(22+23)-III-2	20	2.9
274.54	72.94	109.60	5.32	19.50	10.18	10.18	371.93	371.93	(24+25)-III-3	20	2.9
FLN	78.25	129.10	--	--	10.18	10.18	371.93	371.93	(24+25)-III-3	20	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.44	96.00	0.202	19.40	96.00	0.202	371.93	371.93	(22+23)-III-2	6	Parz.	Parz.
30.50	19.44	96.00	0.202	19.41	96.00	0.202	371.93	371.93	(22+23)-III-2	6	Parz.	Parz.
CAMP	19.44	96.00	0.202	19.50	96.00	0.203	371.93	371.93	(22+23)-III-2	20	Parz.	Parz.
274.54	19.42	96.00	0.202	19.50	96.00	0.203	371.93	371.93	(24+25)-III-3	20	Parz.	Parz.
FLN	19.42	96.00	0.202	19.50	96.00	0.203	371.93	371.93	(24+25)-III-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=(24+25)-III-3 Des=(22+23)-III-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	69.11	--	1523.88	339.88	339.88	12.84	0.00	371.93	152.52	10.64	0.00	4.9
Des	92.72	--	1523.88	339.88	339.88	11.98	0.00	371.93	152.52	10.60	0.00	3.7

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.10

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	12.84	326.62	69.11	1523.88	0.08
Des.	11.98	326.62	92.72	1523.88	0.10

Trave di fondazione: 9018 [4,14], Pilastrate [4,14] Sez. R: By=50.00 cm Bz=100.00 cm L=461.53 cm Ln=472.02 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	4.28	96.52	83.64	--	10.18	10.18	371.93	371.93	(22+23)-VIII-4	20	3.9
47.20	23.23	43.81	89.43	52.72	10.18	10.18	371.93	371.93	5	20	3.3
CAMP	128.22	103.58	--	146.76	10.18	10.18	371.93	371.93	5	20	1.5
424.82	-20.84	169.72	115.14	80.62	10.18	10.18	371.93	371.93	5	20	1.5
FLN	-11.27	250.34	70.27	--	10.18	10.18	371.93	371.93	(22+23)-III-3	20	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.44	96.00	0.202	19.45	96.00	0.203	371.93	371.93	(22+23)-VIII-4	20	Parz.	Parz.
47.20	19.48	96.00	0.203	19.45	96.00	0.203	371.93	371.93	5	20	Parz.	Parz.
CAMP	19.50	96.00	0.203	19.72	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.
424.82	19.45	96.00	0.203	19.72	96.00	0.205	371.93	371.93	5	20	Parz.	Parz.
FLN	19.39	96.00	0.202	19.72	96.00	0.205	371.93	371.93	(22+23)-III-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=20 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	157.75	--	1523.88	339.88	339.88	11.32	0.00	371.93	151.00	10.57	0.00	2.2
Cen	64.76	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.0
Des	196.10	--	1523.88	339.88	339.88	10.37	0.00	371.93	151.00	10.53	0.00	1.7

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.16

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	11.32	326.62	157.75	1523.88	0.14
Des.	10.37	326.62	196.10	1523.88	0.16

Trave di fondazione: 9019 [5,10], Pilastrate [5,10] Sez. R: By=50.00 cm Bz=100.00 cm L=378.19 cm Ln=377.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	-2.97	41.96	51.92	13.13	10.18	10.18	371.93	371.93	(22+23)-I-2	6	6.8
37.70	16.18	42.49	36.30	24.82	10.18	10.18	371.93	371.93	(22+23)-V-2	6	5.5
CAMP	64.68	182.38	--	139.10	10.18	10.18	371.93	371.93	(22+23)-VI-2	20	1.2
339.30	-43.77	246.78	78.09	74.71	10.18	10.18	371.93	371.93	(22+23)-III-2	20	1.2
FLN	-83.08	321.49	98.55	--	10.18	10.18	371.93	371.93	(22+23)-III-2	20	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.37	96.00	0.202	19.38	96.00	0.202	371.93	371.93	(22+23)-I-2	6	Parz.	Parz.
37.70	19.38	96.00	0.202	19.40	96.00	0.202	371.93	371.93	(22+23)-V-2	6	Parz.	Parz.
CAMP	19.40	96.00	0.202	19.85	96.00	0.207	371.93	371.93	(22+23)-VI-2	20	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
339.30	19.35	96.00	0.202	19.85	96.00	0.207	371.93	371.93	(22+23)-III-2	20	Parz.	Parz.
FLN	19.32	96.00	0.201	19.85	96.00	0.207	371.93	371.93	(22+23)-III-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Des=1.000 Comb: Sin=5 Des=4

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	100.79	--	1523.88	339.88	339.88	37.48	0.00	371.93	188.50	11.78	0.00	3.4
Des	227.39	--	1523.88	339.88	339.88	38.95	0.00	371.93	188.50	11.84	0.00	1.5

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.27

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	37.48	326.62	100.79	1523.88	0.18
Des.	38.95	326.62	227.39	1523.88	0.27

Trave di fondazione: 9019 [10,18], Pilastrate [10,18] Sez. R: By=50.00 cm Bz=100.00 cm L=469.90 cm Ln=469.90 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	62.02	255.95	61.84	--	10.18	10.18	371.93	371.93	(22+23)-VI-2	20	1.5
46.99	96.91	166.78	35.72	89.17	10.18	10.18	371.93	371.93	(22+23)-VI-2	20	1.5
CAMP	161.04	93.16	--	162.79	10.18	10.18	371.93	371.93	5	20	1.5
422.91	43.05	30.09	100.60	66.62	10.18	10.18	371.93	371.93	5	(22+23)-IV-2	2.6
FLN	-31.69	96.71	142.41	--	10.18	10.18	371.93	371.93	5	(22+23)-IV-2	3.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.50	96.00	0.203	19.73	96.00	0.206	371.93	371.93	(22+23)-VI-2	20	Parz.	Parz.
46.99	19.51	96.00	0.203	19.73	96.00	0.206	371.93	371.93	(22+23)-VI-2	20	Parz.	Parz.
CAMP	19.56	96.00	0.204	19.73	96.00	0.206	371.93	371.93	5	20	Parz.	Parz.
422.91	19.53	96.00	0.203	19.45	96.00	0.203	371.93	371.93	5	(22+23)-IV-2	Parz.	Parz.
FLN	19.47	96.00	0.203	19.45	96.00	0.203	371.93	371.93	5	(22+23)-IV-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=20 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	217.53	--	1523.88	339.88	339.88	26.21	0.00	371.93	151.00	11.26	0.00	1.6
Cen	76.52	--	1523.88	267.24	267.24	--	--	--	--	7.90	--	3.5
Des	179.04	--	1523.88	339.88	339.88	24.19	0.00	371.93	151.00	11.17	0.00	1.9

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.22

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	26.21	326.62	217.53	1523.88	0.22
Des.	24.19	326.62	179.04	1523.88	0.19

Trave di fondazione: 9020 [6,11], Pilastrate [6,11] Sez. R: By=50.00 cm Bz=100.00 cm L=377.00 cm Ln=377.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	20.70	78.04	53.07	--	12.72	12.72	463.51	463.51	(22+23)-VI-2	20	5.9
37.70	46.50	50.56	31.60	27.48	12.72	12.72	463.51	463.51	(22+23)-VI-2	20	5.9
CAMP	78.54	98.63	--	82.29	12.72	12.72	463.51	463.51	(22+23)-VI-2	20	2.6
339.30	-10.42	136.22	72.34	44.70	12.72	12.72	463.51	463.51	(22+23)-VI-2	20	2.6
FLN	-46.04	180.92	89.86	--	12.72	12.72	463.51	463.51	(22+23)-VI-2	20	2.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.08	96.00	0.220	21.09	96.00	0.220	463.51	463.51	(22+23)-VI-2	20	Parz.	Parz.
37.70	21.09	96.00	0.220	21.09	96.00	0.220	463.51	463.51	(22+23)-VI-2	20	Parz.	Parz.
CAMP	21.09	96.00	0.220	21.25	96.00	0.221	463.51	463.51	(22+23)-VI-2	20	Parz.	Parz.
339.30	21.06	96.00	0.219	21.25	96.00	0.221	463.51	463.51	(22+23)-VI-2	20	Parz.	Parz.
FLN	21.04	96.00	0.219	21.25	96.00	0.221	463.51	463.51	(22+23)-VI-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=4 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	102.78	--	1523.88	339.88	339.88	3.10	0.00	463.51	151.00	10.20	0.00	3.3
Cen	31.02	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	8.4
Des	148.63	--	1523.88	339.88	339.88	2.31	0.00	463.51	151.00	10.16	0.00	2.3

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.10

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	3.10	326.62	102.78	1523.88	0.08
Des.	2.31	326.62	148.63	1523.88	0.10

Trave di fondazione: 9020 [11,19], Pilastrate [11,19] Sez. R: By=50.00 cm Bz=100.00 cm L=469.90 cm Ln=469.90 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	33.63	182.40	31.27	--	12.72	12.72	463.51	463.51	(22+23)-VI-4	20	2.5
46.99	53.15	144.04	12.50	38.36	12.72	12.72	463.51	463.51	(22+23)-VI-4	20	2.5
CAMP	75.17	166.07	--	100.13	12.72	12.72	463.51	463.51	(22+23)-V-3	20	1.7
422.91	41.45	210.71	31.10	55.48	12.72	12.72	463.51	463.51	(22+23)-V-3	20	1.7
FLN	14.78	266.20	48.83	--	12.72	12.72	463.51	463.51	(22+23)-V-3	20	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.07	96.00	0.219	21.26	96.00	0.221	463.51	463.51	(22+23)-VI-4	20	Parz.	Parz.
46.99	21.07	96.00	0.219	21.26	96.00	0.221	463.51	463.51	(22+23)-VI-4	20	Parz.	Parz.
CAMP	21.09	96.00	0.220	21.39	96.00	0.223	463.51	463.51	(22+23)-V-3	20	Parz.	Parz.
422.91	21.08	96.00	0.220	21.39	96.00	0.223	463.51	463.51	(22+23)-V-3	20	Parz.	Parz.
FLN	21.07	96.00	0.219	21.39	96.00	0.223	463.51	463.51	(22+23)-V-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=5 Cen=(22+23)-VI-2 Des=5

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	134.12	--	1523.88	339.88	339.88	11.22	0.00	463.51	151.00	10.57	0.00	2.5
Cen	64.55	--	1523.88	267.24	267.24	--	--	--	--	7.90	--	4.1
Des	157.89	--	1523.88	339.88	339.88	12.48	0.00	463.51	151.00	10.63	0.00	2.2

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.14

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	11.22	326.62	134.12	1523.88	0.12
Des.	12.48	326.62	157.89	1523.88	0.14

Trave di fondazione: 9020 [19,27], Pilastrate [19,27] Sez. R: By=50.00 cm Bz=100.00 cm L=414.09 cm Ln=413.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	22.21	308.64	38.30	--	10.18	10.18	371.93	371.93	(24+25)-V-3	20	1.2
41.30	12.82	243.79	56.84	64.86	10.18	10.18	371.93	371.93	(24+25)-VI-3	20	1.2
CAMP	93.56	185.14	--	123.50	10.18	10.18	371.93	371.93	(22+23)-VI-1	20	1.2
371.70	68.60	15.93	21.83	22.79	10.18	10.18	371.93	371.93	(22+23)-VI-3	(24+25)-V-4	4.1
FLN	48.82	38.72	36.37	--	10.18	10.18	371.93	371.93	(22+23)-II-3	(24+25)-V-4	4.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.39	96.00	0.202	19.83	96.00	0.207	371.93	371.93	(24+25)-V-3	20	Parz.	Parz.
41.30	19.40	96.00	0.202	19.83	96.00	0.207	371.93	371.93	(24+25)-VI-3	20	Parz.	Parz.
CAMP	19.44	96.00	0.203	19.83	96.00	0.207	371.93	371.93	(22+23)-VI-1	20	Parz.	Parz.
371.70	19.44	96.00	0.202	19.35	96.00	0.202	371.93	371.93	(22+23)-VI-3	(24+25)-V-4	Parz.	Parz.
FLN	19.43	96.00	0.202	19.35	96.00	0.202	371.93	371.93	(22+23)-II-3	(24+25)-V-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-V-3

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	164.52	--	1523.88	339.88	339.88	39.87	0.00	371.93	151.00	11.89	0.00	2.1
Cen	103.93	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	2.5
Des	77.76	--	1523.88	339.88	339.88	40.25	0.00	371.93	151.00	11.90	0.00	4.4

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.23

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	39.87	326.62	164.52	1523.88	0.23
Des.	40.25	326.62	77.76	1523.88	0.17

Trave di fondazione: 9021 [7,12], Pilastrate [7,12] Sez. R: By=50.00 cm Bz=100.00 cm L=377.00 cm Ln=377.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	26.68	90.55	34.64	--	12.72	12.72	463.51	463.51	(22+23)-VIII-2	20	5.1
37.70	67.48	66.43	--	24.11	12.72	12.72	463.51	463.51	(22+23)-II-4	20	5.1
CAMP	71.60	72.18	--	48.70	12.72	12.72	463.51	463.51	(22+23)-VI-2	20	3.8
339.30	28.88	94.18	24.61	26.70	12.72	12.72	463.51	463.51	(22+23)-III-2	20	3.8
FLN	12.54	120.88	36.38	--	12.72	12.72	463.51	463.51	(22+23)-III-2	20	3.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.06	96.00	0.219	21.11	96.00	0.220	463.51	463.51	(22+23)-VIII-2	20	Parz.	Parz.
37.70	21.07	96.00	0.220	21.11	96.00	0.220	463.51	463.51	(22+23)-II-4	20	Parz.	Parz.
CAMP	21.08	96.00	0.220	21.16	96.00	0.220	463.51	463.51	(22+23)-VI-2	20	Parz.	Parz.
339.30	21.05	96.00	0.219	21.16	96.00	0.220	463.51	463.51	(22+23)-III-2	20	Parz.	Parz.
FLN	21.04	96.00	0.219	21.16	96.00	0.220	463.51	463.51	(22+23)-III-2	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-I-1 Cen=(24+25)-II-4 Des=(22+23)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	79.05	--	1523.88	339.88	339.88	20.45	0.00	463.51	151.00	10.99	0.00	4.3
Cen	33.17	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	7.9
Des	82.15	--	1523.88	339.88	339.88	19.32	0.00	463.51	151.00	10.94	0.00	4.1

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.11

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	20.45	326.62	79.05	1523.88	0.11
Des.	19.32	326.62	82.15	1523.88	0.11

Trave di fondazione: 9021 [12,20], Pilastrate [12,20] Sez. R: By=50.00 cm Bz=100.00 cm L=469.90 cm Ln=469.90 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	117.32	216.39	--	--	12.72	12.72	463.51	463.51	(24+25)-VI-4	20	2.1
46.99	94.21	183.23	23.11	33.16	12.72	12.72	463.51	463.51	(24+25)-VI-4	20	2.1
CAMP	83.33	156.98	33.99	59.40	12.72	12.72	463.51	463.51	(24+25)-VI-4	20	2.1
422.91	96.33	154.26	6.73	25.19	12.72	12.72	463.51	463.51	(24+25)-II-1	20	2.6
FLN	103.06	179.45	--	--	12.72	12.72	463.51	463.51	(24+25)-II-1	20	2.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	21.15	96.00	0.220	21.31	96.00	0.222	463.51	463.51	(24+25)-VI-4	20	Parz.	Parz.
46.99	21.15	96.00	0.220	21.31	96.00	0.222	463.51	463.51	(24+25)-VI-4	20	Parz.	Parz.
CAMP	21.15	96.00	0.220	21.31	96.00	0.222	463.51	463.51	(24+25)-VI-4	20	Parz.	Parz.
422.91	21.13	96.00	0.220	21.25	96.00	0.221	463.51	463.51	(24+25)-II-1	20	Parz.	Parz.
FLN	21.13	96.00	0.220	21.25	96.00	0.221	463.51	463.51	(24+25)-II-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-II-1 Cen=(22+23)-VI-4 Des=(22+23)-VI-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	104.75	--	1523.88	339.88	339.88	5.00	0.00	463.51	151.00	10.28	0.00	3.2
Cen	67.66	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	3.9
Des	104.13	--	1523.88	339.88	339.88	4.64	0.00	463.51	151.00	10.27	0.00	3.3

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.08

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	5.00	326.62	104.75	1523.88	0.08
Des.	4.64	326.62	104.13	1523.88	0.08

Trave di fondazione: 9021 [20,28], Pilastrate [20,28] Sez. R: By=50.00 cm Bz=100.00 cm L=413.00 cm Ln=413.00 cm Terreno=Terreno Milazzo Criterio : Fondazioni - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	79.70	179.68	--	--	10.18	10.18	371.93	371.93	(22+23)-VI-2	6	2.1
41.30	75.62	146.30	4.08	33.39	10.18	10.18	371.93	371.93	(22+23)-VI-2	6	2.1
CAMP	86.93	115.54	--	64.15	10.18	10.18	371.93	371.93	(22+23)-VI-3	6	2.1
371.70	86.63	66.29	--	30.31	10.18	10.18	371.93	371.93	(22+23)-VI-3	(22+23)-VI-2	3.9
FLN	82.70	96.60	--	--	10.18	10.18	371.93	371.93	(24+25)-VI-3	(22+23)-VI-2	3.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	19.42	96.00	0.202	19.59	96.00	0.204	371.93	371.93	(22+23)-VI-2	6	Parz.	Parz.
41.30	19.42	96.00	0.202	19.59	96.00	0.204	371.93	371.93	(22+23)-VI-2	6	Parz.	Parz.
CAMP	19.43	96.00	0.202	19.59	96.00	0.204	371.93	371.93	(22+23)-VI-3	6	Parz.	Parz.
371.70	19.43	96.00	0.202	19.45	96.00	0.203	371.93	371.93	(22+23)-VI-3	(22+23)-VI-2	Parz.	Parz.
FLN	19.43	96.00	0.202	19.45	96.00	0.203	371.93	371.93	(24+25)-VI-3	(22+23)-VI-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=20 Cen=20 Des=(22+23)-V-2

Sez	Td	VRdns	VRcd	VRsd	VRd	Mt	Tpl	Mr	Dx	Staffe	F.Par.	CS
	kN	kN	kN	kN	kN	kN*m	kN	kN*m	cm	cmq/m	cmq	
Sin	114.64	--	1523.88	339.88	339.88	24.62	0.00	371.93	151.00	11.19	0.00	3.0
Cen	62.11	--	1523.88	261.45	261.45	--	--	--	--	7.73	--	4.2
Des	91.68	--	1523.88	339.88	339.88	25.72	0.00	371.93	151.00	11.24	0.00	3.7

Verifica a torsione bielle compresse ρmax=TEd/TRcd+VEd/VRcd=0.15

	TEd	TRcd	VEd	VRcd	ρ
	kN*m	kN*m	kN	kN	
Sin.	24.62	326.62	114.64	1523.88	0.15
Des.	25.72	326.62	91.68	1523.88	0.14

Verifica dei Pilastri

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Simbologia

L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore

Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica
B[cm]: Larghezza
H[cm]: Altezza

Aspigoli	Area di ferro negli spigoli
Afy	Area di ferro sul lato Y
Afz	Area di ferro sul lato Z
Zona	Punto di verifica
1/N	Distanza dall'inizio della lunghezza netta
Piede	Inizio lunghezza netta
Testa	Fine lunghezza netta
Comb	Combinazione di carico: quando Comb non è sismica è individuata dal codice [(+/-)C], quando è sismica è individuata dal codice [(+/-)(Cx+Cy) Cm Sc], (+/-) rappresenta la eventuale traslazione del diagramma del momento dovuta al taglio, come specificato nel criterio di verifica [positiva (+) o negativa (-)]
- C	Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx	Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy	Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm	Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc	Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1)	Sc = + SismaZ*fz + SismaX*fx + SismaY*fy
2)	Sc = + SismaZ*fz + SismaX*fx - SismaY*fy
3)	Sc = + SismaZ*fz - SismaX*fx + SismaY*fy
4)	Sc = + SismaZ*fz - SismaX*fx - SismaY*fy.
5)	Sc = - SismaZ*fz + SismaX*fx + SismaY*fy
6)	Sc = - SismaZ*fz + SismaX*fx - SismaY*fy
7)	Sc = - SismaZ*fz - SismaX*fx + SismaY*fy
8)	Sc = - SismaZ*fz - SismaX*fx - SismaY*fy.

Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).

N [kN]	Sforzo Normale
N*y [kN]	Sforzo Normale x Omega2
N*z [kN]	Sforzo Normale x Omega3
My [kN*m]	Momento flettente dir Y
M*y [kN*m]	Momento flettente dir Y x cy
cy [kN*m]	Coefficiente moltiplicativo momento flettente dir Y per verifica a carico di punta
cz [kN*m]	Coefficiente moltiplicativo momento flettente dir Z per verifica a carico di punta
Mz [kN*m]	Momento flettente dir Z
M*z [kN*m]	Momento flettente dir Z x cz
εcmax	Deformazione massima cls (1)
εfmax	Deformazione massima acciaio (1)
εcMy	Deformazione massima cls int direzione Y per pressoflessione retta (1)
εfMy	Deformazione massima acciaio int direzione Y per pressoflessione retta (1)
εcMz	Deformazione massima cls int direzione Z per pressoflessione retta (1)
εfMz	Deformazione massima acciaio int direzione Z per pressoflessione retta (1)
ΣMrtY	Somma dei momenti resistenti delle travi in direzione Y(2)
ΣMrtZ	Somma dei momenti resistenti delle travi in direzione Z(2)
ΣMyRich.	Momento resistente richiesto direzione Y per rispettare la gerarchia(2)
ΣMzRich.	Momento resistente richiesto direzione Z per rispettare la gerarchia(2)
T [kN]	Valore del taglio
Dir[Y-Z]	Direzione della componente di taglio
VRdns [kN]	Resistenza a taglio in assenza di armature
VRdns [kN]	Resistenza a taglio in assenza di armature

VRcd [kN]	Resistenza taglio-compressione calcestruzzo
VRsd [kN]	Resistenza taglio-trazione acciaio
VRd [kN]	Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kN]	Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
Ast/m [cmq]	Armatura staffe
Min.Norm.	Valore minimo di norma dell' area delle staffe
cot(θ)	cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
Fatt.Ampl.Sisma	Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
Cs	Coefficiente di sicurezza definito dal rapporto |Fr|/|Fd| (Fr=punto sul dominio di resistenza ottenuto aumentando proporzionalmente Fd,Fd=azione), quando richiesto dal criterio di verifica
ζ_E	Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto(valore stampato quando richiesto dal criterio di verifica)

Verifiche duttilità (quando richieste):

Zona	Sezione di verifica dell'elemento
Comb.	Combinazione di verifica
Nmax [kN]	Sforzo Normale massimo
Dir	Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kN*m]	Momento di snervamento corrispondente a Nmax
MrU [kN*m]	Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
ϕy[1/m]	Curvatura allo snervamento (ϕy= MrU/Mry * ϕ'y)
ϕu[1/m]	Curvatura allo corrispondente a MrU
μ	Capacita in duttilità della sezione
F.Conf	Fattore di confinamento adottato (= fck,c/fck)
μd	Richiesta in duttilità della sezione
Cs	Livello di sicurezza (Cs=μ/μd)

Note Verifica pilastri:

([1]) le deformazioni sono stampate a meno del fattore 10^{-3}

([2]) I momenti resistenti richiesti sono quelli dovuti alla ripartizione della somma dei momenti resistenti delle travi quando nella tabella dei momenti appare '--' significa che la gerarchia in quella direzione non è applicabile a seconda che il pilastro sia al piano terra o all'ultimo piano, oppure, la combinazione corrente non è sismica, oppure, la combinazione è sismica ma la sua direzione non è nella direzione del pilastro considerata. Un valore nullo dei momenti resistenti è relativo a piede o testa di pilastri in fondazione o copertura

Pilastro: 2 [2,102] Sez. R: By=125.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 12.06	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 12.06	Afz = 2.01

ν_{max}=N/(fcd*A)=0.03 <= 0.55 [Comb. (22+23)-VII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-141.34	-110.42	343.62	189.55	818.90	189.55	818.90	1.5
Testa	(22+23)-IV-2	-92.48	-65.26	-40.01	183.98	800.71	183.98	800.71	3.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-4	810.96	826.21	484.81	--	1182.58	1182.58	1182.58	25.13	1.100	2.4
Z	(22+23)-VII-4	187.11	191.79	112.20	--	744.53	586.39	586.39	25.13	2.500	5.2

Pilastro: 3 [3,103] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -

Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.054 <= 0.55 [Comb. (22+23)-VIII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-III-3	-126.42	-17.22	-277.44	129.60	364.24	129.60	364.24	1.3
Testa	(22+23)-III-3	-100.08	11.59	191.35	126.65	358.13	126.65	358.13	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-4	371.95	377.99	222.08	--	698.31	698.31	698.31	16.76	1.547	3.1
Z	(22+23)-VIII-4	133.34	136.25	79.83	--	487.89	390.92	390.92	16.76	2.500	4.9

Pilastro: 4 [4,104] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -
Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.108 <= 0.55 [Comb. (22+23)-IV-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-III-3	-277.42	-14.92	-259.37	146.20	398.59	146.20	398.59	1.6
Testa	6	-161.22	-31.04	141.61	133.49	372.26	133.49	372.26	2.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-2	412.71	418.41	246.12	--	723.13	723.13	723.13	16.76	1.602	2.9
Z	(22+23)-IV-2	153.03	155.79	91.45	--	512.78	390.92	390.92	16.76	2.500	4.3

Pilastro: 4 [104,204] Sez. R: By=80.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri -
Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.049 <= 0.55 [Comb. (22+23)-IV-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-99.75	-61.41	105.73	126.61	358.06	126.61	358.06	1.9
Testa	(22+23)-IV-2	-144.41	-59.66	-31.57	131.61	368.39	131.61	368.39	2.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-2	368.39	373.57	257.21	--	695.89	695.89	695.89	16.76	1.542	2.7
Z	(22+23)-IV-2	131.61	134.12	92.12	--	485.51	390.92	390.92	16.76	2.500	4.2

Pilastro: 5 [5,105] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -

Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.149 <= 0.55 [Comb. (22+23)-II-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-I-1	-202.37	-12.92	121.14	135.71	269.41	135.71	269.41	2.4
Testa	20	-442.05	-19.54	52.16	158.58	302.14	158.58	302.14	4.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-II-4	293.02	295.77	174.35	--	437.30	437.30	437.30	9.14	2.405	2.5
Z	(22+23)-II-4	151.93	153.63	90.49	--	398.98	213.23	213.23	9.14	2.500	2.4

Pilastro: 5 [105,205] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri -
Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.066 <= 0.55 [Comb. (22+23)-II-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-I-4	-150.94	22.83	-104.52	130.18	261.30	130.18	261.30	2.4
Testa	(24+25)-I-1	-77.65	8.15	-127.27	122.15	249.47	122.15	249.47	2.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-II-4	261.45	264.13	182.20	--	418.33	418.33	418.33	9.14	2.300	2.3
Z	(22+23)-II-4	130.28	132.11	90.96	--	370.10	213.23	213.23	9.14	2.500	2.3

Pilastro: 6 [6,106] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -
Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.113 <= 0.55 [Comb. (22+23)-IV-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-343.48	-53.50	85.05	150.25	290.52	150.25	290.52	2.2
Testa	(22+23)-III-2	-264.75	-7.22	-88.89	142.25	278.97	142.25	278.97	3.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-2	279.66	282.61	166.50	--	429.14	429.14	429.14	9.14	2.360	2.6
Z	(22+23)-IV-2	142.73	144.76	85.13	--	386.40	213.23	213.23	9.14	2.500	2.5

Pilastro: 6 [106,206] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri -

Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.044 <= 0.55 [Comb. (22+23)-III-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-I-1	-102.31	-16.24	110.82	124.87	253.48	124.87	253.48	2.3
Testa	(22+23)-II-1	-54.97	42.55	-78.34	119.63	245.76	119.63	245.76	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-III-2	252.50	255.24	176.02	--	413.18	413.18	413.18	9.14	2.272	2.3
Z	(22+23)-III-2	124.21	126.06	86.76	--	362.48	213.23	213.23	9.14	2.500	2.5

Pilastro: 7 [7,107] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -
Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.038 <= 0.55 [Comb. (22+23)-VI-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-II-1	-66.85	-69.59	113.66	122.90	350.40	122.90	350.40	1.6
Testa	(24+25)-II-1	-34.35	55.51	-55.99	119.21	342.82	119.21	342.82	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VI-2	359.32	365.41	214.61	--	690.66	690.66	690.66	16.76	1.530	3.2
Z	(22+23)-VI-2	127.22	130.17	76.22	--	480.39	390.92	390.92	16.76	2.500	5.1

Pilastro: 8 [8,108] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -
Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01

ν_{max}=N/(fcd*A)=0.057 <= 0.55 [Comb. (22+23)-III-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-IV-2	-90.97	22.63	88.80	105.65	226.82	105.65	226.82	2.3
Testa	(24+25)-VIII-4	-85.70	-37.28	-36.70	105.07	225.76	105.07	225.76	2.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-III-3	233.55	237.32	139.44	--	450.02	450.02	450.02	11.17	2.025	3.2
Z	(22+23)-III-3	109.40	111.55	65.43	--	366.62	260.62	260.62	11.17	2.500	4.0

Pilastro: 9 [9,109] Sez. R: By=30.00 cm Bz=70.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri -

Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.085 <= 0.55 [Comb. (22+23)-VIII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VIII-4	-252.32	157.42	17.67	334.48	142.28	334.48	142.28	2.3
Testa	6	-85.65	-113.83	50.14	302.23	124.05	302.23	124.05	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-4	139.82	142.28	83.54	--	439.16	293.19	293.19	12.57	2.500	3.5
Z	(22+23)-VIII-4	330.12	334.48	196.81	--	562.57	562.57	562.57	12.57	1.912	2.9

Pilastro: 9 [109,209] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.051 <= 0.55 [Comb. (22+23)-I-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-68.39	-75.31	25.91	298.81	122.12	298.81	122.12	3.2
Testa	20	-144.03	-25.63	56.63	313.70	130.54	313.70	130.54	2.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-I-4	129.35	131.52	90.44	--	425.77	293.19	293.19	12.57	2.500	3.2
Z	(22+23)-I-4	311.60	315.44	217.38	--	551.54	551.54	551.54	12.57	1.874	2.5

Pilastro: 10 [10,110] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.155 <= 0.55 [Comb. (22+23)-III-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-531.05	-77.39	50.29	288.46	146.41	288.46	146.41	2.2
Testa	(22+23)-IV-2	-313.24	-83.11	-14.08	260.93	129.18	260.93	129.18	3.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-III-3	135.09	136.75	80.50	--	400.97	260.62	260.62	11.17	2.500	3.2
Z	(22+23)-III-3	269.16	271.72	160.17	--	475.52	475.52	475.52	11.17	2.139	3.0

Pilastro: 10 [110,210] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.077 <= 0.55 [Comb. (22+23)-III-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VI-4	-184.60	119.18	-11.94	243.47	115.84	243.47	115.84	2.2
Testa	(22+23)-VI-4	-167.73	-142.30	11.99	241.15	114.03	241.15	114.03	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-III-3	115.25	117.05	80.53	--	373.83	260.62	260.62	11.17	2.500	3.2
Z	(22+23)-III-3	242.71	245.03	169.08	--	455.48	455.48	455.48	11.17	2.049	2.7

Pilastro: 11 [11,111] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.172 <= 0.55 [Comb. (22+23)-I-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-I-1	-438.97	-20.05	110.89	158.34	301.86	158.34	301.86	2.7
Testa	6	-144.35	-30.20	62.63	129.47	260.25	129.47	260.25	3.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-I-1	300.08	301.86	178.25	--	442.39	442.39	442.39	9.14	2.433	2.5
Z	(22+23)-I-1	156.79	158.34	93.32	--	406.94	213.23	213.23	9.14	2.500	2.3

Pilastro: 11 [111,211] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.071 <= 0.55 [Comb. (22+23)-I-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-II-4	-134.42	69.29	-10.14	128.39	258.66	128.39	258.66	2.1
Testa	(24+25)-II-4	-117.55	-74.46	8.33	126.54	255.94	126.54	255.94	1.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-I-1	263.68	266.34	183.74	--	419.62	419.62	419.62	9.14	2.307	2.3
Z	(22+23)-I-1	131.80	133.61	92.01	--	372.02	213.23	213.23	9.14	2.500	2.3

Pilastro: 12 [12,112] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.066 <= 0.55 [Comb. (22+23)-I-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-II-1	-146.58	-200.93	17.37	237.65	111.75	237.65	111.75	1.2
Testa	(24+25)-II-1	-126.83	155.85	-19.82	233.89	109.59	233.89	109.59	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-I-1	112.13	114.27	67.04	--	370.06	260.62	260.62	11.17	2.500	3.9
Z	(22+23)-I-1	238.32	241.45	142.07	--	452.63	452.63	452.63	11.17	2.037	3.2

Pilastro: 13 [13,113] Sez. R: By=30.00 cm Bz=70.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.13 <= 0.55 [Comb. (22+23)-VII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VIII-4	-372.88	171.99	29.64	356.52	154.82	356.52	154.82	2.1
Testa	6	-215.99	-122.44	47.77	327.59	138.39	327.59	138.39	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-4	153.78	156.11	91.77	--	457.42	293.19	293.19	12.57	2.500	3.2
Z	(22+23)-VII-4	354.69	358.76	211.27	--	577.28	577.28	577.28	12.57	1.962	2.7

Pilastro: 13 [113,213] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.053 <= 0.55 [Comb. (22+23)-VII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-227.13	-74.15	48.07	329.71	139.59	329.71	139.59	2.7
Testa	(22+23)-IV-2	-104.52	-70.84	-45.80	305.95	126.16	305.95	126.16	2.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-4	129.80	131.97	90.75	--	426.33	293.19	293.19	12.57	2.500	3.2
Z	(22+23)-VII-4	312.40	316.23	217.92	--	552.00	552.00	552.00	12.57	1.876	2.5

Pilastro: 14 [14,37] Sez. R: By=30.00 cm Bz=60.00 cm L=80.00 cm Ln=80.00 cm Criterio: Pilastri tozzi - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.172 <= 0.55 [Comb. (22+23)-III-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
Piede	(22+23)-VIII-4	-381.35	152.41	23.25	269.90	135.57	269.90	135.57	1.8
Testa	20	-508.84	-38.07	19.25	285.83	145.37	285.83	145.37	4.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-2	--	--	65.16	--	404.41	260.62	260.62	11.17	2.500	4.0
Z	(22+23)-VII-1	--	--	423.81	--	479.98	479.98	479.98	11.17	2.160	1.1

Pilastro: 14 [37,114] Sez. R: By=30.00 cm Bz=60.00 cm L=359.00 cm Ln=359.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.156 <= 0.55 [Comb. (22+23)-VII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-131.53	-44.20	30.09	234.80	110.11	234.80	110.11	3.4
Testa	6	-115.38	-76.29	40.55	231.67	108.34	231.67	108.34	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-1	135.63	136.98	98.71	--	401.59	260.62	260.62	11.17	2.500	2.6
Z	(22+23)-VII-1	269.98	272.06	196.28	--	475.96	475.96	475.96	11.17	2.141	2.4

Pilastro: 14 [114,214] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.076 <= 0.55 [Comb. (22+23)-V-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VII-4	-131.74	86.48	-18.33	234.84	110.13	234.84	110.13	2.7
Testa	20	-181.05	-118.84	41.72	242.98	115.46	242.98	115.46	1.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-V-1	115.18	116.99	80.49	--	373.74	260.62	260.62	11.17	2.500	3.2
Z	(22+23)-V-1	242.63	244.95	169.03	--	455.42	455.42	455.42	11.17	2.049	2.7

Pilastro: 15 [15,115] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.066 <= 0.55 [Comb. (22+23)-III-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-IV-3	-133.55	-146.98	-20.97	235.18	110.33	235.18	110.33	1.6
Testa	(22+23)-IV-3	-125.41	109.71	31.23	233.62	109.44	233.62	109.44	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-III-4	112.04	114.17	66.99	--	369.94	260.62	260.62	11.17	2.500	3.9
Z	(22+23)-III-4	238.16	241.33	141.99	--	452.54	452.54	452.54	11.17	2.036	3.2

Pilastro: 16 [16,116] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.125 <= 0.55 [Comb. (22+23)-IV-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-VIII-4	-185.53	99.82	19.94	266.77	133.91	266.77	133.91	2.7
Testa	6	-98.75	-80.28	22.49	252.90	124.48	252.90	124.48	2.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-3	145.80	147.80	86.94	--	390.49	213.23	213.23	9.14	2.500	2.5
Z	(22+23)-IV-3	284.11	286.99	169.12	--	431.81	431.81	431.81	9.14	2.375	2.6

Pilastro: 16 [116,216] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.052 <= 0.55 [Comb. (22+23)-VIII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-47.95	-30.62	51.33	244.60	118.85	244.60	118.85	2.3
Testa	20	-122.18	-120.40	8.05	256.69	127.05	256.69	127.05	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-1	126.37	128.22	88.26	--	365.18	213.23	213.23	9.14	2.500	2.4
Z	(22+23)-VIII-1	255.69	258.41	178.22	--	415.01	415.01	415.01	9.14	2.282	2.3

Pilastro: 17 [17,35] Sez. R: By=30.00 cm Bz=70.00 cm L=267.00 cm Ln=267.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.108 <= 0.55 [Comb. (22+23)-V-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-II-2	-233.44	191.39	40.45	330.91	140.26	330.91	140.26	1.6
Testa	6	-161.32	-70.25	37.80	317.06	132.44	317.06	132.44	3.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-V-3	148.12	149.57	144.94	--	449.28	293.19	293.19	12.57	2.500	2.0
Z	(22+23)-V-3	344.76	347.32	336.97	--	570.76	570.76	570.76	12.57	1.939	1.7

Pilastro: 17 [35,117] Sez. R: By=30.00 cm Bz=70.00 cm L=172.00 cm Ln=172.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.106 <= 0.55 [Comb. (22+23)-V-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-138.24	-119.40	35.94	312.57	129.90	312.57	129.90	2.2
Testa	6	-129.21	-100.32	47.83	310.80	128.90	310.80	128.90	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-V-3	147.97	148.91	224.39	--	448.75	293.19	293.19	12.57	2.500	1.3
Z	(22+23)-V-3	344.51	346.17	522.02	--	570.34	570.34	570.34	12.57	1.938	1.1

Pilastro: 17 [117,217] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.045 <= 0.55 [Comb. (22+23)-V-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-188.20	-119.95	46.48	322.26	135.37	322.26	135.37	2.1
Testa	(22+23)-V-2	-71.44	-74.58	-52.63	299.42	122.46	299.42	122.46	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-V-3	127.27	129.45	88.99	--	423.19	293.19	293.19	12.57	2.500	3.3
Z	(22+23)-V-3	307.91	311.77	214.82	--	549.39	549.39	549.39	12.57	1.867	2.6

Pilastro: 18 [18,118] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01

ν_{max}=N/(fcd*A)=0.127 <= 0.55 [Comb. (22+23)-VII-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-V-2	-322.56	-6.25	127.39	130.11	262.17	130.11	262.17	2.4
Testa	6	-79.98	-41.88	67.89	104.43	224.59	104.43	224.59	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-2	259.57	262.20	154.51	--	468.27	468.27	468.27	11.17	2.107	3.0
Z	(22+23)-VII-2	128.15	130.13	76.48	--	391.02	260.62	260.62	11.17	2.500	3.4

Pilastro: 18 [118,218] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01

ν_{max}=N/(fcd*A)=0.054 <= 0.55 [Comb. (22+23)-V-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VI-3	-97.12	-51.21	-75.20	106.33	228.06	106.33	228.06	1.8
Testa	(22+23)-VI-3	-80.24	57.49	75.94	104.46	224.65	104.46	224.65	1.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-V-2	232.74	235.99	162.49	--	449.43	449.43	449.43	11.17	2.022	2.8
Z	(22+23)-V-2	108.94	110.79	76.17	--	365.86	260.62	260.62	11.17	2.500	3.4

Pilastro: 19 [19,119] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

ν_{max}=N/(fcd*A)=0.153 <= 0.55 [Comb. (22+23)-VII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-V-1	-389.06	-28.61	116.12	172.41	317.30	172.41	317.30	2.5
Testa	6	-146.85	-36.92	65.97	147.71	288.33	147.71	288.33	3.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-1	315.05	317.32	187.26	--	426.54	357.20	357.20	7.18	2.500	1.9
Z	(22+23)-VII-1	170.75	172.43	101.62	--	400.12	167.54	167.54	7.18	2.500	1.6

Pilastro: 19 [119,219] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

ν_{max}=N/(fcd*A)=0.053 <= 0.55 [Comb. (22+23)-V-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-II-1	-127.15	-69.84	11.15	145.57	285.89	145.57	285.89	2.3
Testa	(22+23)-VI-1	-110.46	72.46	-21.53	143.75	283.55	143.75	283.55	2.1

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-V-1	285.02	287.11	198.34	--	389.91	357.20	357.20	7.18	2.500	1.8
Z	(22+23)-V-1	144.81	146.65	101.04	--	365.75	167.54	167.54	7.18	2.500	1.7

Pilastro: 20 [20,120] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.065 <= 0.55 [Comb. (22+23)-VII-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-VI-4	-138.31	197.60	6.36	236.09	110.85	236.09	110.85	1.2
Testa	(24+25)-VI-4	-118.56	-162.12	-11.87	232.29	108.69	232.29	108.69	1.4

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-2	111.66	113.80	66.77	--	369.47	260.62	260.62	11.17	2.500	3.9
Z	(22+23)-VII-2	237.51	240.85	141.66	--	452.18	452.18	452.18	11.17	2.034	3.2

Pilastro: 21 [21,121] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.062 <= 0.55 [Comb. (22+23)-VII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-IV-3	-122.97	-145.42	-26.79	233.15	109.17	233.15	109.17	1.5
Testa	(22+23)-IV-3	-103.22	120.27	41.02	229.27	107.00	229.27	107.00	1.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VII-4	110.87	113.01	66.30	--	368.47	260.62	260.62	11.17	2.500	3.9
Z	(22+23)-VII-4	236.13	239.83	140.95	--	451.42	451.42	451.42	11.17	2.031	3.2

Pilastro: 22 [22,122] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.135 <= 0.55 [Comb. (22+23)-IV-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-VIII-1	-203.79	-130.46	13.92	246.11	117.89	246.11	117.89	2.0
Testa	6	-119.24	-68.17	51.25	232.42	108.76	232.42	108.76	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-2	130.25	132.20	77.72	--	393.90	260.62	260.62	11.17	2.500	3.4
Z	(22+23)-IV-2	262.37	264.98	156.16	--	470.38	470.38	470.38	11.17	2.116	3.0

Pilastro: 22 [122,222] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.045 <= 0.55 [Comb. (22+23)-IV-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-157.99	-55.71	46.91	239.78	112.98	239.78	112.98	2.3
Testa	(24+25)-IV-3	-63.36	89.39	7.66	221.17	102.58	221.17	102.58	2.6

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-2	106.53	108.39	74.51	--	362.85	260.62	260.62	11.17	2.500	3.5
Z	(22+23)-IV-2	228.43	231.76	159.53	--	447.13	447.13	447.13	11.17	2.012	2.8

Pilastro: 23 [23,36] Sez. R: By=30.00 cm Bz=70.00 cm L=267.00 cm Ln=267.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.108 <= 0.55 [Comb. (22+23)-VI-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-V-3	-203.09	-160.33	-54.36	325.12	136.99	325.12	136.99	1.6
Testa	(22+23)-VII-4	-227.13	26.35	65.34	329.71	139.59	329.71	139.59	2.5

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VI-2	148.23	149.68	145.05	--	449.42	293.19	293.19	12.57	2.500	2.0
Z	(22+23)-VI-2	344.96	347.52	337.16	--	570.88	570.88	570.88	12.57	1.940	1.7

Pilastro: 23 [36,123] Sez. R: By=30.00 cm Bz=70.00 cm L=172.00 cm Ln=172.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.111 <= 0.55 [Comb. (22+23)-VI-2]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-296.45	-62.30	51.40	342.70	146.95	342.70	146.95	2.9
Testa	(22+23)-VI-3	-27.46	48.00	-48.42	290.67	117.51	290.67	117.51	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VI-2	149.52	150.46	226.73	--	450.79	293.19	293.19	12.57	2.500	1.3
Z	(22+23)-VI-2	347.23	348.87	526.13	--	571.98	571.98	571.98	12.57	1.944	1.1

Pilastro: 23 [123,223] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.049 <= 0.55 [Comb. (22+23)-VIII-4]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VIII-1	-82.62	-40.51	58.13	301.63	123.72	301.63	123.72	2.2
Testa	(22+23)-VIII-1	-62.94	64.61	-57.89	297.73	121.51	297.73	121.51	2.0

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-4	128.56	130.73	89.89	--	424.79	293.19	293.19	12.57	2.500	3.3
Z	(22+23)-VIII-4	310.20	314.05	216.41	--	550.72	550.72	550.72	12.57	1.871	2.5

Pilastro: 24 [24,124] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

ν_{max}=N/(fcd*A)=0.064 <= 0.55 [Comb. (22+23)-IV-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-IV-3	-163.19	-138.33	-22.34	240.53	113.54	240.53	113.54	1.7
Testa	(22+23)-IV-3	-143.43	119.20	32.85	237.06	111.40	237.06	111.40	1.7

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-3	111.40	113.54	66.61	--	369.14	260.62	260.62	11.17	2.500	3.9
Z	(22+23)-IV-3	237.06	240.53	141.43	--	451.94	451.94	451.94	11.17	2.033	3.2

Pilastro: 25 [25,125] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04

ν_{max}=N/(fcd*A)=0.187 <= 0.55 [Comb. (22+23)-IV-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-IV-3	-476.07	-136.37	-17.80	327.03	179.23	327.03	179.23	2.4
Testa	6	-156.27	-67.55	42.66	289.49	148.74	289.49	148.74	2.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-3	177.77	179.23	105.72	--	412.03	167.54	167.54	7.18	2.500	1.6
Z	(22+23)-IV-3	324.86	327.03	193.04	--	439.24	357.20	357.20	7.18	2.500	1.9

Pilastro: 25 [125,225] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04

ν_{max}=N/(fcd*A)=0.059 <= 0.55 [Comb. (22+23)-IV-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-II-3	-142.87	-64.35	-41.93	287.83	147.28	287.83	147.28	2.9
Testa	(22+23)-II-3	-125.99	71.75	53.02	285.75	145.44	285.75	145.44	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-IV-3	146.45	148.28	102.17	--	367.81	167.54	167.54	7.18	2.500	1.6
Z	(22+23)-IV-3	286.88	288.97	199.63	--	392.10	357.20	357.20	7.18	2.500	1.8

Pilastro: 26 [26,126] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.162 <= 0.55 [Comb. (22+23)-VIII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-II-3	-404.95	-146.24	-19.58	298.78	155.63	298.78	155.63	2.1
Testa	6	-49.36	-64.68	46.36	244.83	119.01	244.83	119.01	2.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-1	154.64	156.26	92.07	--	403.34	213.23	213.23	9.14	2.500	2.3
Z	(22+23)-VIII-1	297.42	299.49	176.76	--	440.10	440.10	440.10	9.14	2.420	2.5

Pilastro: 26 [126,226] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
Testa	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

ν_{max}=N/(fcd*A)=0.064 <= 0.55 [Comb. (22+23)-VIII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-VI-2	-35.32	77.54	41.65	242.52	117.44	242.52	117.44	2.1
Testa	6	18.79	-81.00	44.23	233.56	111.35	233.56	111.35	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-1	129.73	131.55	90.58	--	369.40	213.23	213.23	9.14	2.500	2.4
Z	(22+23)-VIII-1	260.63	263.32	181.64	--	417.86	417.86	417.86	9.14	2.298	2.3

Pilastro: 27 [27,127] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.039 <= 0.55 [Comb. (22+23)-VI-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	20	-147.53	-25.21	186.99	131.96	369.11	131.96	369.11	2.0
Testa	6	-48.08	-55.81	5.32	120.77	346.03	120.77	346.03	2.3

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VI-3	359.51	365.61	214.73	--	690.78	690.78	690.78	16.76	1.530	3.2
Z	(22+23)-VI-3	127.32	130.27	76.28	--	480.51	390.92	390.92	16.76	2.500	5.1

Pilastro: 28 [28,128] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.038 <= 0.55 [Comb. (22+23)-VI-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-VI-2	-72.49	66.79	103.82	123.54	351.72	123.54	351.72	1.7
Testa	6	-6.61	-56.86	78.33	116.04	335.96	116.04	335.96	1.9

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VI-1	359.40	365.50	214.66	--	690.71	690.71	690.71	16.76	1.530	3.2
Z	(22+23)-VI-1	127.26	130.21	76.25	--	480.44	390.92	390.92	16.76	2.500	5.1

Pilastro: 29 [29,129] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.039 <= 0.55 [Comb. (22+23)-VIII-3]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	6	-69.35	-15.39	190.68	123.18	350.99	123.18	350.99	1.8
Testa	6	-43.01	-56.47	-2.40	120.19	344.84	120.19	344.84	2.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-3	359.93	366.02	214.97	--	691.03	691.03	691.03	16.76	1.531	3.2
Z	(22+23)-VIII-3	127.52	130.47	76.40	--	480.75	390.92	390.92	16.76	2.500	5.1

Pilastro: 30 [30,130] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.055 <= 0.55 [Comb. (22+23)-VIII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(24+25)-V-2	-161.30	-9.03	223.77	133.49	372.28	133.49	372.28	1.8
Testa	(22+23)-V-2	-148.72	14.12	-144.61	132.09	369.38	132.09	369.38	2.8

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-1	372.28	378.31	222.27	--	698.51	698.51	698.51	16.76	1.547	3.1
Z	(22+23)-VIII-1	133.49	136.41	79.93	--	488.08	390.92	390.92	16.76	2.500	4.9

Pilastro: 31 [31,131] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm Criterio: Pilastri - Verifica a presso-flessione deviata: **Verificato**

Piede	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
Testa	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

ν_{max}=N/(fcd*A)=0.042 <= 0.55 [Comb. (22+23)-VIII-1]

Zona	C.	N	My	Mz	Mry+	Mrz+	Mry-	Mrz-	CS
		kN	kN*m	kN*m	kN*m	kN*m	kN*m	kN*m	
Piede	(22+23)-II-3	-129.41	-69.02	-150.53	129.94	364.93	129.94	364.93	1.6
Testa	(22+23)-II-3	-103.07	64.28	24.42	126.98	358.83	126.98	358.83	2.2

Verifica a taglio

Dir	C.	MrSup	MrInf	T	Vrdns	Vrcd	Vrsd	Vrd	Ast/m	cot(θ)	Cs
		kN*m	kN*m	kN	kN	kN	kN	kN	cmq/m		
Y	(22+23)-VIII-1	362.03	368.11	216.21	--	692.30	692.30	692.30	16.76	1.534	3.2
Z	(22+23)-VIII-1	128.53	131.48	77.00	--	481.99	390.92	390.92	16.76	2.500	5.1

Verifica delle travi

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Simbologia:
Terreno Nome della stratigrafia per travi Winkler

L [cm] Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
By[cm]: Larghezza (asse locale y)
Bz[cm]: Larghezza (asse locale z)
Sez. T: Sezione a T (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. L: Sezione ad L (rovescia e non)
Ba[cm]: Larghezza base inferiore
Ha[cm]: Altezza inferiore
Bs[cm]: Larghezza superiore
Hs[cm]: Altezza superiore
Sez. C: Sezione circolare
R[cm]: Raggio
Sez. G: Sezione generica
B[cm]: Larghezza
H[cm]: Altezza
Fatt.Ampl.Sisma Fattore moltiplicativo di gruppo per le azioni sismiche (solo se diverso da 1.0)
X [cm] Punto di verifica
ILN Inizio luce netta
CAMP Punto di massimo momento sia superiore che inferiore ad esclusione degli estremi
FLN Fine luce netta
M- [kN*m] Momento negativo massimo di calcolo([1])
N- [kN] Sforzo normale corrispondente ad M-
M+ [kN*m] Momento positivo massimo di calcolo([1])
N+ [kN] Sforzo normale corrispondente ad M+
ΔM- [kN*m] Incremento di M- per la traslazione del diagramma del momento a causa del taglio
ΔM+ [kN*m] Incremento di M+ per la traslazione del diagramma del momento a causa del taglio
Afs [cmq] Area di ferro superiore
Afi [cmq] Area di ferro inferiore
εsc- Deformazione nel cls per effetto di M-:N-([4])
εsc+ Deformazione nel cls per effetto di M+:N+([4])
εsf- Deformazione nell'acciaio per effetto di M-:N-([4])
εsf+ Deformazione nell'acciaio per effetto di M+:N+([4])
C- Combinazione di carico generatore di M-:N-
C+ Combinazione di carico generatore di M+:N+
x- [cm] Profondità asse neutro per la combinazione C-([5])
d- [cm] Altezza utile della sezione per la combinazione C-([6])
x+ [cm] Profondità asse neutro per la combinazione C+([5])
d+ [cm] Altezza utile della sezione per la combinazione C+([6])
Mr- [kN*m] Momento resistente superiore
Mr+ [kN*m] Momento resistente inferiore
Stato- Stato della sezione per la combinazione C-([7])
Stato+ Stato della sezione per la combinazione C+([7])
Comb Combinazione di carico: quando Comb non è sismica è individuata dal codice [C], quando è sismica è individuata dal codice [(Cx+Cy) Cm Sc].
- C Individua la Combinazione di Carico non sismica (1, 2, ecc. come da scenario);
- Cx Individua la Combinazione di Carico sismica in direzione x (SismaX, come da scenario);
- Cy Individua la Combinazione di Carico sismica in direzione y (SismaY, come da scenario);
- Cm Individua la Combinazione spostamento masse (I, II, III, IV, V, ecc. come da Combinazioni Sisma in Spostamento masse impalcato);
- Sc Individua la sottocombinazione ottenuta mediante la permutazione dei segni (1, 2, 3, 4, 5, 6, 7, 8):
1) Sc = + SismaZ*fz + SismaX*fx + SismaY*fy
2) Sc = + SismaZ*fz + SismaX*fx - SismaY*fy
3) Sc = + SismaZ*fz - SismaX*fx + SismaY*fy
4) Sc = + SismaZ*fz - SismaX*fx - SismaY*fy.

5) Sc = - SismaZ*fz + SismaX*fx + SismaY*fy
6) Sc = - SismaZ*fz + SismaX*fx - SismaY*fy
7) Sc = - SismaZ*fz - SismaX*fx + SismaY*fy
8) Sc = - SismaZ*fz - SismaX*fx - SismaY*fy.

Le ultime quattro sono assenti quando non è richiesto il contributo del sisma in direzione verticale. Le combinazioni delle azioni sismiche così ottenute vengono combinate con i carichi verticali (come da scenario).

Sez — Sezione di verifica [Sinistra/Destra]
Td [kN] — Taglio di verifica([2])
VRdns [kN] — Resistenza a taglio in assenza di armature
VRcd [kN] — Resistenza taglio-compressione calcestruzzo
VRsd [kN] — Resistenza taglio-trazione acciaio
VRd [kN] — Resistenza a taglio =min(VRcd,VRsd)
VRd,f [kN] — Resistenza a taglio dovuta alla resistenza a trazione del calcestruzzo ad alte prestazioni (quando presente)(cfr. eq 4.2 CNR204/2006), oppure resistenza rinforzo del composito (quando presente)(cfr. eq 4.19 CNR200/2013), oppure resistenza rinforzo della camicia in acciaio (quando presente)(cfr. eq C8.7.4.5 Circolare NTC)
Mt [kN*m] — Momento torcente
Tpl [kN] — Taglio dovuto ai momenti resistenti alle estremità della trave
Mr [kN*m] — Momento resistente (ultimo) utilizzato per il calcolo di Tpl quando richiesto
Dx [cm] — Distanza dall'estremo da armare con staffe
Staffe [cmq] — Area delle staffe
cot(θ) — cot(θ) secondo il punto 4.1.2.3.5 delle Norme Tecniche
F.Par. [cmq] — Area armatura longitudinale di parete([3])
Cs — Coefficiente di sicurezza definito dal rapporto Fr/Fd (Fr=resistenza,Fd=azione)
ζ_E — Livello di sicurezza sismico definito come rapporto tra l'accelerazione sopportabile e l'accelerazione di progetto, quando richiesto dal criterio di verifica

Simbologia verifica travi collegamento:

Comb — Combinazione più gravosa
Nsd [kN] — Azione verticale negli elementi collegati, nella combinazione specificata
α — Coefficiente in funzione della classe di terreno (NTC 7.2.5.1)
a/g — Punto di aggancio dello spettro di accelerazione [a/g=Sa(0)]
N — Sforzo normale di verifica N=α*Nsd*a/g
Af [cmq] — Area di ferro complessiva nella sezione
NRd C [kN] — Resistenza a compressione della sezione
NRd T [kN] — Resistenza a trazione della sezione

Verifiche duttilità (quando richieste):

Zona — Sezione di verifica dell'elemento
Comb. — Combinazione di verifica
Nmax [kN] — Sforzo Normale massimo
Dir — Direzione di flessione (pilastri=Y o Z, travi =Z, pareti= ortogonale alla base)
Mry [kN*m] — Momento di snervamento corrispondente a Nmax
MrU [kN*m] — Momento ultimo (resistente) corrispondente a Nmax sulla sezione depurata del calcestruzzo non confinato, considerando il confinamento
ϕy[1/m] — Curvatura allo snervamento (ϕy= MrU/Mry * ϕ'y)
ϕu[1/m] — Curvatura allo corrispondente a MrU
μ — Capacita in duttilità della sezione
F.Conf — Fattore di confinamento adottato (= fck,c/fck)
μd — Richiesta in duttilità della sezione
Cs — Livello di sicurezza (Cs=μ/μd)

Note Verifica travi:

([1]) il valore del momento di verifica è dato da M +ΔM
([2]) Td è il valore di verifica a taglio esso è calcolato in funzione della somma tra taglio da carichi verticali il valore di Tpl ovvero quando la trave è tozza amplificando il taglio di calcolo dovuto al sisma per il fattore di comportamento
([3]) armatura necessaria per la sola verifica a torsione
([4]) le deformazioni sono stampate a meno del fattore 10^{-3}
([5]) distanza tra la fibra di cls compressa piu' lontata e l'asse neutro in direzione ortogonale all'asse neutro
([6]) distanza tra le fibre sollecitate piu' lontane dall'asse neutro: nel caso di sezione parzializzata le due fibre

sono quella di cls compresso e quella dell'acciaio teso piu lontane da n-n, mentre nel caso di sezione completamente compressa le due fibre sono le due di cls compresso piu lontane da n-n

([7]) Indica lo stato della sezione se: completamente compressa (Compr.),completamente tesa (Tesa), parzializzata (Parz.)

Trave: 101 [129,130], Pilastrate [29,30] Sez. R: By=30.00 cm Bz=50.00 cm L=534.50 cm Ln=534.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	110.98	25.43	--	10.90	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	1.5
53.45	71.63	34.87	38.51	7.76	10.05	6.03	171.20	104.01	(22+23)-V-3	(22+23)-V-2	1.6
CAMP	38.03	85.39	32.88	--	10.05	6.03	171.20	104.01	(22+23)-V-3	20	1.2
481.05	70.97	56.52	39.57	4.47	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.5
FLN	111.40	48.81	--	7.55	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.04	46.50	0.345	11.56	46.50	0.249	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
53.45	16.04	46.50	0.345	11.58	46.50	0.249	171.20	104.01	(22+23)-V-3	(22+23)-V-2	Parz.	Parz.
CAMP	15.81	46.50	0.340	11.75	46.50	0.253	171.20	104.01	(22+23)-V-3	20	Parz.	Parz.
481.05	16.04	46.50	0.345	11.65	46.50	0.251	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.
FLN	16.05	46.50	0.345	11.63	46.50	0.250	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	115.94	--	442.88	175.61	175.61	61.79	104.01	75.00	10.72	1.5
Cen	95.77	--	442.88	97.32	97.32	--	--	--	5.94	1.0
Des	118.28	--	442.88	175.61	175.61	61.79	171.20	75.00	10.72	1.5

Trave: 101 [130,131], Pilastrate [30,31] Sez. R: By=30.00 cm Bz=50.00 cm L=614.50 cm Ln=614.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	126.90	-11.96	--	17.44	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	1.3
61.45	80.50	8.52	39.50	12.77	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	1.4
CAMP	40.21	101.24	34.30	--	10.05	6.03	171.20	104.01	(22+23)-V-3	20	1.0
553.05	67.37	50.69	36.81	24.16	10.05	6.03	171.20	104.01	(22+23)-V-2	20	1.4
FLN	110.61	62.68	--	6.80	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.14	46.50	0.347	11.45	46.50	0.246	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
61.45	16.10	46.50	0.346	11.51	46.50	0.247	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
CAMP	15.83	46.50	0.340	10.70	46.50	0.230	171.20	104.01	(22+23)-V-3	20	Parz.	Parz.
553.05	16.00	46.50	0.344	11.71	46.50	0.252	171.20	104.01	(22+23)-V-2	20	Parz.	Parz.
FLN	16.04	46.50	0.345	11.68	46.50	0.251	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Sin	111.48	--	442.88	175.61	175.61	53.74	104.01	75.00	10.72	1.6
Cen	91.35	--	442.88	91.91	91.91	--	--	--	5.61	1.0
Des	113.59	--	442.88	175.61	175.61	53.74	171.20	75.00	10.72	1.5

Trave: 102 [124,125], Pilastrate [24,25] Sez. R: By=30.00 cm Bz=50.00 cm L=544.50 cm Ln=544.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	61.42	0.69	--	19.22	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	2.8
54.45	26.90	0.52	33.17	37.07	10.05	6.03	171.20	104.01	(22+23)-V-3	20	2.8
CAMP	17.42	89.58	32.78	--	10.05	6.03	171.20	104.01	(22+23)-V-2	20	1.2
490.05	46.09	35.83	57.27	8.12	10.05	6.03	171.20	104.01	5	6	1.7
FLN	105.70	23.79	--	11.57	10.05	6.03	171.20	104.01	5	6	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.75	46.50	0.339	11.50	46.50	0.247	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
54.45	15.75	46.50	0.339	11.57	46.50	0.249	171.20	104.01	(22+23)-V-3	20	Parz.	Parz.
CAMP	15.69	46.50	0.337	11.76	46.50	0.253	171.20	104.01	(22+23)-V-2	20	Parz.	Parz.
490.05	16.00	46.50	0.344	11.59	46.50	0.249	171.20	104.01	5	6	Parz.	Parz.
FLN	16.01	46.50	0.344	11.56	46.50	0.249	171.20	104.01	5	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	122.35	--	442.88	175.61	175.61	60.65	104.01	75.00	10.72	1.4
Cen	100.30	--	442.88	103.88	103.88	--	--	--	6.34	1.0
Des	126.49	--	442.88	175.61	175.61	60.65	171.20	75.00	10.72	1.4

Trave: 102 [125,126], Pilastrate [25,26] Sez. R: By=30.00 cm Bz=50.00 cm L=604.50 cm Ln=604.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	163.80	5.02	--	15.26	20.11	8.04	327.78	137.84	5	6	2.0
60.45	86.79	22.65	66.64	12.79	20.11	8.04	327.78	137.84	5	6	2.1
CAMP	24.13	109.84	54.23	--	10.05	8.04	171.47	137.84	5	20	1.3
544.05	49.36	28.45	38.27	35.11	10.05	8.04	171.47	137.84	(22+23)-V-2	20	2.0
FLN	93.58	28.03	--	11.04	10.05	8.04	171.47	137.84	(22+23)-V-2	6	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	20.77	46.50	0.447	11.29	46.50	0.243	327.78	137.84	5	6	Parz.	Parz.
60.45	20.71	46.50	0.445	11.32	46.50	0.243	327.78	137.84	5	6	Parz.	Parz.
CAMP	15.30	46.50	0.329	13.51	46.50	0.291	171.47	137.84	5	20	Parz.	Parz.
544.05	15.34	46.50	0.330	13.32	46.50	0.286	171.47	137.84	(22+23)-V-2	20	Parz.	Parz.
FLN	15.37	46.50	0.331	13.22	46.50	0.284	171.47	137.84	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Sin	167.11	--	442.88	182.92	182.92	92.43	327.78	75.00	11.17	1.1
Cen	139.56	--	442.88	150.23	150.23	--	--	--	9.17	1.1
Des	165.60	--	442.88	182.92	182.92	92.43	137.84	75.00	11.17	1.1

Trave: 103 [121,122], Pilastrate [21,22] Sez. R: By=30.00 cm Bz=50.00 cm L=574.50 cm Ln=574.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	74.23	-12.71	--	24.00	10.05	8.04	171.47	137.84	1	(24+25)-V-2	2.3
57.45	13.40	-5.43	55.36	42.41	10.05	8.04	171.47	137.84	5	20	2.5
CAMP	3.11	109.85	31.91	--	10.05	8.04	171.47	137.84	(22+23)-V-2	1	1.3
517.05	38.16	19.35	38.91	36.77	10.05	8.04	171.47	137.84	(22+23)-V-2	20	2.2
FLN	81.34	17.19	--	13.06	10.05	8.04	171.47	137.84	5	6	2.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.28	46.50	0.329	13.12	46.50	0.282	171.47	137.84	1	(24+25)-V-2	Parz.	Parz.
57.45	15.25	46.50	0.328	13.22	46.50	0.284	171.47	137.84	5	20	Parz.	Parz.
CAMP	15.10	46.50	0.325	13.51	46.50	0.291	171.47	137.84	(22+23)-V-2	1	Parz.	Parz.
517.05	15.29	46.50	0.329	13.29	46.50	0.286	171.47	137.84	(22+23)-V-2	20	Parz.	Parz.
FLN	15.31	46.50	0.329	13.19	46.50	0.284	171.47	137.84	5	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	131.46	--	442.88	175.61	175.61	64.61	137.84	75.00	10.72	1.3
Cen	107.39	--	442.88	109.75	109.75	--	--	--	6.70	1.0
Des	131.52	--	442.88	175.61	175.61	64.61	171.47	75.00	10.72	1.3

Trave: 104 [115,113], Pilastrate [15,13] Sez. R: By=30.00 cm Bz=50.00 cm L=531.07 cm Ln=577.87 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	57.89	-0.12	--	15.96	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	3.0
57.79	25.81	-1.24	29.04	32.25	10.05	6.03	171.20	104.01	(22+23)-III-3	20	3.1
CAMP	14.46	84.47	25.17	--	10.05	6.03	171.20	104.01	(22+23)-III-2	20	1.2
520.08	42.26	26.78	29.79	24.54	10.05	6.03	171.20	104.01	(22+23)-III-2	20	2.0
FLN	75.17	33.75	--	7.78	10.05	6.03	171.20	104.01	(22+23)-III-2	6	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.73	46.50	0.338	11.49	46.50	0.247	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
57.79	15.72	46.50	0.338	11.54	46.50	0.248	171.20	104.01	(22+23)-III-3	20	Parz.	Parz.
CAMP	15.64	46.50	0.336	11.74	46.50	0.253	171.20	104.01	(22+23)-III-2	20	Parz.	Parz.
520.08	15.81	46.50	0.340	11.62	46.50	0.250	171.20	104.01	(22+23)-III-2	20	Parz.	Parz.
FLN	15.83	46.50	0.340	11.58	46.50	0.249	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	107.27	--	442.88	175.61	175.61	57.15	104.01	75.00	10.72	1.6
Cen	88.25	--	442.88	91.46	91.46	--	--	--	5.59	1.0
Des	104.26	--	442.88	175.61	175.61	57.15	171.20	75.00	10.72	1.7

Trave: 105 [102,108], Pilastrate [2,8] Sez. R: By=30.00 cm Bz=50.00 cm L=368.36 cm Ln=252.48 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	44.32	54.68	--	--	10.05	8.04	171.47	137.84	(24+25)-V-4	(22+23)-V-1	2.5
25.25	37.23	49.49	7.09	5.19	10.05	8.04	171.47	137.84	(24+25)-V-4	(22+23)-V-1	2.5
CAMP	30.68	48.13	13.64	12.64	10.05	8.04	171.47	137.84	(24+25)-V-4	6	2.3
227.23	20.94	54.74	12.81	6.03	10.05	8.04	171.47	137.84	(22+23)-I-1	6	2.3
FLN	33.75	60.77	--	--	10.05	8.04	171.47	137.84	(22+23)-I-1	6	2.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.14	46.50	0.326	13.28	46.50	0.286	171.47	137.84	(24+25)-V-4	(22+23)-V-1	Parz.	Parz.
25.25	15.14	46.50	0.326	13.28	46.50	0.286	171.47	137.84	(24+25)-V-4	(22+23)-V-1	Parz.	Parz.
CAMP	15.14	46.50	0.326	13.31	46.50	0.286	171.47	137.84	(24+25)-V-4	6	Parz.	Parz.
227.23	15.09	46.50	0.325	13.31	46.50	0.286	171.47	137.84	(22+23)-I-1	6	Parz.	Parz.
FLN	15.09	46.50	0.325	13.31	46.50	0.286	171.47	137.84	(22+23)-I-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	161.46	--	442.88	175.61	175.61	147.01	137.84	75.00	10.72	1.1
Cen	154.18	--	442.88	164.63	164.63	--	--	--	10.05	1.1
Des	165.69	--	442.88	182.92	182.92	147.01	171.47	75.00	11.17	1.1

Trave: 105 [108,113], Pilastrate [8,13] Sez. R: By=30.00 cm Bz=50.00 cm L=327.82 cm Ln=327.82 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	69.97	18.13	--	12.48	10.05	8.04	171.47	137.84	(22+23)-VIII-4	6	2.5
32.78	46.70	26.30	23.28	10.91	10.05	8.04	171.47	137.84	(22+23)-VIII-4	6	2.5
CAMP	25.28	70.25	35.28	--	10.05	8.04	171.47	137.84	(22+23)-VIII-4	20	2.0
295.03	40.23	64.61	15.04	5.00	10.05	8.04	171.47	137.84	(24+25)-VIII-1	20	2.0
FLN	55.27	68.46	--	--	10.05	8.04	171.47	137.84	(24+25)-VIII-1	(22+23)-VIII-4	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.26	46.50	0.328	13.19	46.50	0.284	171.47	137.84	(22+23)-VIII-4	6	Parz.	Parz.
32.78	15.26	46.50	0.328	13.22	46.50	0.284	171.47	137.84	(22+23)-VIII-4	6	Parz.	Parz.
CAMP	15.21	46.50	0.327	13.35	46.50	0.287	171.47	137.84	(22+23)-VIII-4	20	Parz.	Parz.
295.03	15.19	46.50	0.327	13.34	46.50	0.287	171.47	137.84	(24+25)-VIII-1	20	Parz.	Parz.
FLN	15.19	46.50	0.327	13.34	46.50	0.287	171.47	137.84	(24+25)-	(22+23)-	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
									VIII-1	VIII-4		

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	144.11	--	442.88	175.61	175.61	113.23	137.84	75.00	10.72	1.2
Cen	126.93	--	442.88	137.19	137.19	--	--	--	8.38	1.1
Des	147.64	--	442.88	175.61	175.61	113.23	171.47	75.00	10.72	1.2

Trave: 105 [113,116], Pilastrate [13,16] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	111.24	37.76	--	--	10.05	8.04	171.47	137.84	(22+23)-VII-4	(24+25)-VII-1	1.5
32.99	85.20	33.26	26.04	4.50	10.05	8.04	171.47	137.84	(22+23)-VII-4	(24+25)-VII-1	1.5
CAMP	59.97	55.07	40.49	18.68	10.05	8.04	171.47	137.84	(22+23)-VII-4	(22+23)-VII-4	1.7
296.88	52.91	67.59	18.53	10.52	10.05	8.04	171.47	137.84	(24+25)-VII-1	(22+23)-VII-4	1.8
FLN	71.44	78.10	--	--	10.05	8.04	171.47	137.84	(24+25)-VII-1	(22+23)-VII-4	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.46	46.50	0.333	13.22	46.50	0.284	171.47	137.84	(22+23)-VII-4	(24+25)-VII-1	Parz.	Parz.
32.99	15.46	46.50	0.333	13.22	46.50	0.284	171.47	137.84	(22+23)-VII-4	(24+25)-VII-1	Parz.	Parz.
CAMP	15.41	46.50	0.331	13.36	46.50	0.287	171.47	137.84	(22+23)-VII-4	(22+23)-VII-4	Parz.	Parz.
296.88	15.27	46.50	0.328	13.38	46.50	0.288	171.47	137.84	(24+25)-VII-1	(22+23)-VII-4	Parz.	Parz.
FLN	15.27	46.50	0.328	13.38	46.50	0.288	171.47	137.84	(24+25)-VII-1	(22+23)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	134.68	--	442.88	175.61	175.61	112.52	137.84	75.00	10.72	1.3
Cen	124.38	--	442.88	126.64	126.64	--	--	--	7.73	1.0
Des	141.13	--	442.88	175.61	175.61	112.52	171.47	75.00	10.72	1.2

Trave: 105 [116,123], Pilastrate [16,23] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	99.92	7.97	--	12.74	10.05	8.04	171.47	137.84	(22+23)-VII-4	6	1.7
53.25	63.92	20.94	35.37	10.83	10.05	8.04	171.47	137.84	(22+23)-VII-4	6	1.7
CAMP	33.40	86.49	29.97	--	10.05	8.04	171.47	137.84	(22+23)-VII-4	20	1.6
479.27	38.51	36.04	32.82	25.98	10.05	8.04	171.47	137.84	(22+23)-V-2	20	2.2
FLN	71.92	41.68	--	6.78	10.05	8.04	171.47	137.84	(22+23)-V-2	6	2.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
ILN	15.41	46.50	0.331	13.16	46.50	0.283	171.47	137.84	(22+23)-VII-4	6	Parz.	Parz.
53.25	15.40	46.50	0.331	13.20	46.50	0.284	171.47	137.84	(22+23)-VII-4	6	Parz.	Parz.
CAMP	15.23	46.50	0.327	13.41	46.50	0.288	171.47	137.84	(22+23)-VII-4	20	Parz.	Parz.
479.27	15.26	46.50	0.328	13.31	46.50	0.286	171.47	137.84	(22+23)-V-2	20	Parz.	Parz.
FLN	15.27	46.50	0.328	13.26	46.50	0.285	171.47	137.84	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	124.72	--	442.88	175.61	175.61	69.70	137.84	75.00	10.72	1.4
Cen	104.54	--	442.88	112.56	112.56	--	--	--	6.87	1.1
Des	126.76	--	442.88	175.61	175.61	69.70	171.47	75.00	10.72	1.4

Trave: 106 [103,109], Pilastrate [3,9] Sez. R: By=30.00 cm Bz=50.00 cm L=327.85 cm Ln=327.85 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	85.53	29.87	--	--	10.05	6.03	171.20	104.01	(22+23)-V-4	(24+25)-V-1	2.0
32.79	62.68	26.96	22.85	2.91	10.05	6.03	171.20	104.01	(22+23)-V-4	(24+25)-V-1	2.0
CAMP	40.93	57.90	35.36	14.76	10.05	6.03	171.20	104.01	(22+23)-V-4	(22+23)-VII-4	1.4
295.07	44.89	67.93	16.43	7.94	10.05	6.03	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	1.4
FLN	61.33	75.87	--	--	10.05	6.03	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.89	46.50	0.342	11.54	46.50	0.248	171.20	104.01	(22+23)-V-4	(24+25)-V-1	Parz.	Parz.
32.79	15.89	46.50	0.342	11.54	46.50	0.248	171.20	104.01	(22+23)-V-4	(24+25)-V-1	Parz.	Parz.
CAMP	15.84	46.50	0.341	11.70	46.50	0.252	171.20	104.01	(22+23)-V-4	(22+23)-VII-4	Parz.	Parz.
295.07	15.75	46.50	0.339	11.71	46.50	0.252	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	Parz.	Parz.
FLN	15.75	46.50	0.339	11.71	46.50	0.252	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	122.24	--	442.88	175.61	175.61	100.73	104.01	75.00	10.72	1.4
Cen	111.68	--	442.88	117.59	117.59	--	--	--	7.18	1.1
Des	128.85	--	442.88	175.61	175.61	100.73	171.20	75.00	10.72	1.4

Trave: 106 [109,114], Pilastrate [9,14] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	103.01	22.58	--	11.02	10.05	6.03	171.20	104.01	(22+23)-VII-4	6	1.7
32.99	77.59	29.82	25.43	9.63	10.05	6.03	171.20	104.01	(22+23)-VII-4	6	1.7
CAMP	53.86	64.44	38.63	--	10.05	6.03	171.20	104.01	(22+23)-VII-4	20	1.6
296.88	41.27	58.53	15.88	9.49	10.05	6.03	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	1.5
FLN	57.16	68.02	--	--	10.05	6.03	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.99	46.50	0.344	11.55	46.50	0.248	171.20	104.01	(22+23)-VII-4	6	Parz.	Parz.
32.99	15.99	46.50	0.344	11.57	46.50	0.249	171.20	104.01	(22+23)-VII-4	6	Parz.	Parz.
CAMP	15.93	46.50	0.343	11.67	46.50	0.251	171.20	104.01	(22+23)-VII-4	20	Parz.	Parz.
296.88	15.73	46.50	0.338	11.68	46.50	0.251	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	Parz.	Parz.
FLN	15.73	46.50	0.338	11.68	46.50	0.251	171.20	104.01	(24+25)-VII-1	(22+23)-VII-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	127.47	--	442.88	175.61	175.61	100.12	104.01	75.00	10.72	1.4
Cen	111.74	--	442.88	119.88	119.88	--	--	--	7.32	1.1
Des	125.25	--	442.88	175.61	175.61	100.12	171.20	75.00	10.72	1.4

Trave: 106 [114,117], Pilastrate [14,17] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	115.00	7.75	--	13.41	10.05	6.03	171.20	104.01	(22+23)-VIII-4	6	1.5
53.25	71.68	21.40	42.55	11.31	10.05	6.03	171.20	104.01	(22+23)-VIII-4	6	1.5
CAMP	34.47	89.23	36.55	--	10.05	6.03	171.20	104.01	(22+23)-VIII-4	20	1.2
479.27	51.42	39.15	33.99	25.03	10.05	6.03	171.20	104.01	(22+23)-VI-1	20	1.6
FLN	86.02	37.99	--	6.92	10.05	6.03	171.20	104.01	(22+23)-VI-1	6	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.07	46.50	0.346	11.51	46.50	0.247	171.20	104.01	(22+23)-VIII-4	6	Parz.	Parz.
53.25	16.06	46.50	0.345	11.55	46.50	0.248	171.20	104.01	(22+23)-VIII-4	6	Parz.	Parz.
CAMP	15.81	46.50	0.340	11.76	46.50	0.253	171.20	104.01	(22+23)-VIII-4	20	Parz.	Parz.
479.27	15.89	46.50	0.342	11.66	46.50	0.251	171.20	104.01	(22+23)-VI-1	20	Parz.	Parz.
FLN	15.89	46.50	0.342	11.59	46.50	0.249	171.20	104.01	(22+23)-VI-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	120.19	--	442.88	175.61	175.61	62.02	104.01	75.00	10.72	1.5
Cen	98.76	--	442.88	102.89	102.89	--	--	--	6.28	1.0
Des	117.85	--	442.88	175.61	175.61	62.02	171.20	75.00	10.72	1.5

Trave: 107 [102,103], Pilastrate [2,3] Sez. R: By=30.00 cm Bz=50.00 cm L=514.30 cm Ln=514.30 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	81.40	19.16	--	4.76	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	2.1
51.43	58.15	23.88	23.25	2.36	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	2.1
CAMP	37.43	67.74	21.12	--	10.05	6.03	171.20	104.01	(22+23)-I-4	20	1.5
462.87	35.92	52.52	22.87	10.44	10.05	6.03	171.20	104.01	(22+23)-I-1	20	1.7
FLN	58.79	54.85	--	3.21	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.87	46.50	0.341	11.52	46.50	0.248	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
51.43	15.87	46.50	0.341	11.52	46.50	0.248	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.74	46.50	0.338	11.68	46.50	0.251	171.20	104.01	(22+23)-I-4	20	Parz.	Parz.
462.87	15.74	46.50	0.338	11.66	46.50	0.251	171.20	104.01	(22+23)-I-1	20	Parz.	Parz.
FLN	15.74	46.50	0.338	11.64	46.50	0.250	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	92.74	--	442.88	175.61	175.61	64.21	104.01	75.00	10.72	1.9
Cen	83.14	--	442.88	89.44	89.44	--	--	--	5.46	1.1
Des	97.45	--	442.88	175.61	175.61	64.21	171.20	75.00	10.72	1.8

Trave: 107 [103,104], Pilastrate [3,4] Sez. R: By=30.00 cm Bz=50.00 cm L=463.50 cm Ln=463.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	123.94	23.89	--	--	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.4
46.35	89.30	25.50	34.64	--	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.4
CAMP	57.42	70.34	36.33	10.87	10.05	6.03	171.20	104.01	(22+23)-I-4	(22+23)-I-4	1.3
417.15	60.00	80.36	23.97	6.62	10.05	6.03	171.20	104.01	(24+25)-I-1	(22+23)-I-4	1.2
FLN	83.98	86.98	--	--	10.05	12.06	171.64	205.22	(24+25)-I-1	(22+23)-I-4	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.12	46.50	0.347	11.52	46.50	0.248	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
46.35	16.12	46.50	0.347	11.52	46.50	0.248	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.94	46.50	0.343	11.73	46.50	0.252	171.20	104.01	(22+23)-I-4	(22+23)-I-4	Parz.	Parz.
417.15	15.88	46.50	0.342	11.75	46.50	0.253	171.20	104.01	(24+25)-I-1	(22+23)-I-4	Parz.	Parz.
FLN	14.34	46.50	0.308	16.06	46.50	0.345	171.64	205.22	(24+25)-I-1	(22+23)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	129.44	--	442.88	175.61	175.61	97.45	171.20	75.00	10.72	1.4
Cen	117.70	--	442.88	126.91	126.91	--	--	--	7.75	1.1
Des	132.38	--	442.88	175.61	175.61	97.45	205.22	75.00	10.72	1.3

Trave: 107 [104,105], Pilastrate [4,5] Sez. R: By=30.00 cm Bz=50.00 cm L=590.40 cm Ln=590.40 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	144.11	9.29	--	15.57	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.2
59.04	94.35	26.86	44.10	9.96	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.2
CAMP	51.84	92.87	37.66	--	10.05	6.03	171.20	104.01	(22+23)-I-4	20	1.1
531.36	77.30	43.04	42.97	6.99	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.4
FLN	125.80	32.23	--	9.59	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.26	46.50	0.350	11.52	46.50	0.248	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
59.04	16.22	46.50	0.349	11.56	46.50	0.249	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.91	46.50	0.342	11.78	46.50	0.253	171.20	104.01	(22+23)-I-4	20	Parz.	Parz.
531.36	16.10	46.50	0.346	11.61	46.50	0.250	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.
FLN	16.14	46.50	0.347	11.58	46.50	0.249	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	120.27	--	442.88	175.61	175.61	55.94	104.01	75.00	10.72	1.5
Cen	96.32	--	442.88	98.65	98.65	--	--	--	6.02	1.0
Des	122.60	--	442.88	175.61	175.61	55.94	171.20	75.00	10.72	1.4

Trave: 107 [105,106], Pilastrate [5,6] Sez. R: By=30.00 cm Bz=50.00 cm L=397.00 cm Ln=397.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	98.96	76.68	--	--	10.05	12.06	171.64	205.22	(22+23)-I-4	(24+25)-I-1	1.7
39.70	69.99	69.45	28.97	7.23	10.05	12.06	171.64	205.22	(22+23)-I-4	(24+25)-I-1	1.7
CAMP	58.17	59.48	41.44	12.26	10.05	6.03	171.20	104.01	(22+23)-I-1	(24+25)-I-1	1.4
357.30	88.86	51.24	33.82	2.81	10.05	6.03	171.20	104.01	(22+23)-I-1	(24+25)-I-4	1.4
FLN	122.69	54.05	--	--	10.05	6.03	171.20	104.01	(22+23)-I-1	(24+25)-I-4	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	14.39	46.50	0.309	16.01	46.50	0.344	171.64	205.22	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
39.70	14.39	46.50	0.309	16.01	46.50	0.344	171.64	205.22	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.97	46.50	0.344	11.69	46.50	0.251	171.20	104.01	(22+23)-I-1	(24+25)-I-1	Parz.	Parz.
357.30	16.12	46.50	0.347	11.63	46.50	0.250	171.20	104.01	(22+23)-I-1	(24+25)-I-4	Parz.	Parz.
FLN	16.12	46.50	0.347	11.63	46.50	0.250	171.20	104.01	(22+23)-I-1	(24+25)-I-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	153.19	--	442.88	175.61	175.61	113.78	205.22	75.00	10.72	1.1
Cen	137.42	--	442.88	149.66	149.66	--	--	--	9.14	1.1
Des	153.19	--	442.88	175.61	175.61	113.78	171.20	75.00	10.72	1.1

Trave: 107 [106,107], Pilastrate [6,7] Sez. R: By=30.00 cm Bz=50.00 cm L=530.00 cm Ln=530.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	72.61	35.30	--	--	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	2.4
53.00	48.35	36.24	23.94	--	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	2.4
CAMP	45.02	70.33	24.70	--	10.05	6.03	171.20	104.01	(22+23)-I-1	20	1.5
477.00	70.04	67.99	27.98	0.57	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.5
FLN	98.39	65.41	--	2.55	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.82	46.50	0.340	11.56	46.50	0.249	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
53.00	15.81	46.50	0.340	11.56	46.50	0.249	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.80	46.50	0.340	11.69	46.50	0.251	171.20	104.01	(22+23)-I-1	20	Parz.	Parz.
477.00	15.96	46.50	0.343	11.68	46.50	0.251	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.
FLN	15.97	46.50	0.343	11.68	46.50	0.251	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	93.64	--	442.88	175.61	175.61	62.31	104.01	75.00	10.72	1.9
Cen	81.42	--	442.88	82.32	82.32	--	--	--	5.03	1.0
Des	93.64	--	442.88	175.61	175.61	62.31	171.20	75.00	10.72	1.9

Trave: 108 [107,112], Pilastrate [7,12] Sez. R: By=30.00 cm Bz=50.00 cm L=377.00 cm Ln=377.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	74.21	58.80	--	--	10.05	6.03	171.20	104.01	(22+23)-II-4	(24+25)-II-1	1.8
37.70	48.58	55.19	25.63	3.61	10.05	6.03	171.20	104.01	(22+23)-II-4	(24+25)-II-1	1.8
CAMP	53.92	57.88	41.64	--	10.05	6.03	171.20	104.01	(22+23)-II-1	20	1.8
339.30	83.08	47.78	32.19	0.46	10.05	6.03	171.20	104.01	(22+23)-II-1	6	1.5
FLN	115.27	45.57	--	2.51	10.05	6.03	171.20	104.01	(22+23)-II-1	6	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.82	46.50	0.340	11.64	46.50	0.250	171.20	104.01	(22+23)-II-4	(24+25)-II-1	Parz.	Parz.
37.70	15.82	46.50	0.340	11.64	46.50	0.250	171.20	104.01	(22+23)-II-4	(24+25)-II-1	Parz.	Parz.
CAMP	15.95	46.50	0.343	11.64	46.50	0.250	171.20	104.01	(22+23)-II-1	20	Parz.	Parz.
339.30	16.07	46.50	0.346	11.60	46.50	0.250	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.
FLN	16.07	46.50	0.346	11.60	46.50	0.250	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	129.42	--	442.88	175.61	175.61	87.60	104.01	75.00	10.72	1.4
Cen	114.50	--	442.88	118.30	118.30	--	--	--	7.22	1.0
Des	129.42	--	442.88	175.61	175.61	87.60	171.20	75.00	10.72	1.4

Trave: 108 [112,120], Pilastrate [12,20] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	111.83	36.46	--	7.35	10.05	6.03	171.20	104.01	(22+23)-II-4	(22+23)-II-1	1.5
46.99	75.00	43.55	36.84	1.61	10.05	6.03	171.20	104.01	(22+23)-II-4	(22+23)-VI-1	1.5
CAMP	53.52	73.69	39.22	--	10.05	6.03	171.20	104.01	(22+23)-II-1	20	1.4
422.91	88.34	42.99	38.75	7.13	10.05	6.03	171.20	104.01	(22+23)-II-1	6	1.3
FLN	127.09	34.59	--	9.15	10.05	6.03	171.20	104.01	(22+23)-II-1	6	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.05	46.50	0.345	11.59	46.50	0.249	171.20	104.01	(22+23)-II-4	(22+23)-II-1	Parz.	Parz.
46.99	16.05	46.50	0.345	11.59	46.50	0.249	171.20	104.01	(22+23)-II-4	(22+23)-VI-1	Parz.	Parz.
CAMP	15.93	46.50	0.343	11.70	46.50	0.252	171.20	104.01	(22+23)-II-1	20	Parz.	Parz.
422.91	16.15	46.50	0.347	11.61	46.50	0.250	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.
FLN	16.15	46.50	0.347	11.59	46.50	0.249	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	125.86	--	442.88	175.61	175.61	70.28	104.01	75.00	10.72	1.4
Cen	104.12	--	442.88	109.75	109.75	--	--	--	6.70	1.1
Des	120.45	--	442.88	175.61	175.61	70.28	171.20	75.00	10.72	1.5

Trave: 108 [120,128], Pilastrate [20,28] Sez. R: By=30.00 cm Bz=50.00 cm L=413.00 cm Ln=413.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	110.18	42.74	--	5.26	10.05	6.03	171.20	104.01	(22+23)-VI-2	(22+23)-VI-3	1.6
41.30	76.49	49.05	33.69	--	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	1.6
CAMP	46.70	78.50	38.77	--	10.05	6.03	171.20	104.01	(22+23)-VI-2	20	1.3
371.70	53.16	57.29	29.86	14.86	10.05	6.03	171.20	104.01	(22+23)-VI-3	20	1.4
FLN	83.01	38.89	--	21.85	10.05	6.03	171.20	104.01	(22+23)-VI-3	20	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.04	46.50	0.345	11.60	46.50	0.250	171.20	104.01	(22+23)-VI-2	(22+23)-VI-3	Parz.	Parz.
41.30	16.04	46.50	0.345	11.61	46.50	0.250	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.
CAMP	15.89	46.50	0.342	11.72	46.50	0.252	171.20	104.01	(22+23)-VI-2	20	Parz.	Parz.
371.70	15.88	46.50	0.341	11.70	46.50	0.252	171.20	104.01	(22+23)-VI-3	20	Parz.	Parz.
FLN	15.88	46.50	0.341	11.65	46.50	0.251	171.20	104.01	(22+23)-VI-3	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	127.19	--	442.88	175.61	175.61	79.96	104.01	75.00	10.72	1.4
Cen	108.43	--	442.88	113.05	113.05	--	--	--	6.90	1.0
Des	124.53	--	442.88	175.61	175.61	79.96	171.20	75.00	10.72	1.4

Trave: 109 [106,111], Pilastrate [6,11] Sez. R: By=30.00 cm Bz=50.00 cm L=377.00 cm Ln=377.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	90.60	53.15	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-4	(24+25)-VI-1	1.9
37.70	59.18	32.18	31.43	27.02	10.05	6.03	171.20	104.01	(22+23)-VI-4	20	1.8
CAMP	46.04	73.16	52.23	--	10.05	6.03	171.20	104.01	(22+23)-II-1	20	1.4
339.30	82.35	25.20	41.05	10.56	10.05	6.03	171.20	104.01	(22+23)-II-1	6	1.4
FLN	123.41	15.43	--	12.96	10.05	6.03	171.20	104.01	(22+23)-II-1	6	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.92	46.50	0.342	11.62	46.50	0.250	171.20	104.01	(22+23)-VI-4	(24+25)-VI-1	Parz.	Parz.
37.70	15.92	46.50	0.342	11.65	46.50	0.250	171.20	104.01	(22+23)-VI-4	20	Parz.	Parz.
CAMP	15.96	46.50	0.343	11.70	46.50	0.252	171.20	104.01	(22+23)-II-1	20	Parz.	Parz.
339.30	16.12	46.50	0.347	11.56	46.50	0.249	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.
FLN	16.12	46.50	0.347	11.53	46.50	0.248	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	153.64	--	442.88	175.61	175.61	87.60	104.01	75.00	10.72	1.1
Cen	130.58	--	442.88	138.01	138.01	--	--	--	8.43	1.1
Des	153.64	--	442.88	175.61	175.61	87.60	171.20	75.00	10.72	1.1

Trave: 109 [111,119], Pilastrate [11,19] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	107.18	13.10	--	16.21	10.05	6.03	171.20	104.01	(22+23)-VI-4	6	1.6
46.99	60.93	4.82	46.25	46.02	10.05	6.03	171.20	104.01	(22+23)-VI-4	20	1.6
CAMP	34.87	100.05	46.95	--	10.05	6.03	171.20	104.01	(22+23)-VI-3	20	1.0
422.91	76.35	14.10	48.24	30.15	10.05	6.03	171.20	104.01	(22+23)-VI-3	21	1.4
FLN	124.59	18.19	--	14.13	10.05	6.03	171.20	104.01	(22+23)-VI-3	6	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.02	46.50	0.344	11.54	46.50	0.248	171.20	104.01	(22+23)-VI-4	6	Parz.	Parz.
46.99	16.02	46.50	0.344	11.61	46.50	0.250	171.20	104.01	(22+23)-VI-4	20	Parz.	Parz.
CAMP	15.87	46.50	0.341	11.81	46.50	0.254	171.20	104.01	(22+23)-VI-3	20	Parz.	Parz.
422.91	16.13	46.50	0.347	11.59	46.50	0.249	171.20	104.01	(22+23)-VI-3	21	Parz.	Parz.
FLN	16.13	46.50	0.347	11.55	46.50	0.248	171.20	104.01	(22+23)-VI-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
Sin	159.19	--	442.88	175.61	175.61	70.28	104.01	75.00	10.72	1.1
Cen	124.22	--	442.88	126.64	126.64	--	--	--	7.73	1.0
Des	151.33	--	442.88	175.61	175.61	70.28	171.20	75.00	10.72	1.2

Trave: 110 [119,127], Pilastrate [19,27] Sez. R: By=30.00 cm Bz=50.00 cm L=414.09 cm Ln=410.83 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	81.56	14.11	--	8.55	10.05	6.03	171.20	104.01	(22+23)-II-4	(24+25)-II-1	2.1
41.08	53.18	0.02	28.37	32.76	10.05	6.03	171.20	104.01	(22+23)-II-4	20	2.1
CAMP	28.69	76.55	32.25	--	10.05	6.03	171.20	104.01	(22+23)-II-4	20	1.4
369.74	45.21	52.42	25.13	16.08	10.05	6.03	171.20	104.01	(22+23)-VI-1	20	1.5
FLN	70.34	54.27	--	4.21	10.05	6.03	171.20	104.01	(22+23)-VI-1	6	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.87	46.50	0.341	11.51	46.50	0.248	171.20	104.01	(22+23)-II-4	(24+25)-II-1	Parz.	Parz.
41.08	15.87	46.50	0.341	11.55	46.50	0.248	171.20	104.01	(22+23)-II-4	20	Parz.	Parz.
CAMP	15.75	46.50	0.339	11.71	46.50	0.252	171.20	104.01	(22+23)-II-4	20	Parz.	Parz.
369.74	15.80	46.50	0.340	11.68	46.50	0.251	171.20	104.01	(22+23)-VI-1	20	Parz.	Parz.
FLN	15.80	46.50	0.340	11.64	46.50	0.250	171.20	104.01	(22+23)-VI-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	127.38	--	442.88	175.61	175.61	80.39	104.01	75.00	10.72	1.4
Cen	108.70	--	442.88	113.06	113.06	--	--	--	6.90	1.0
Des	124.84	--	442.88	175.61	175.61	80.39	171.20	75.00	10.72	1.4

Trave: 111 [102,115], Pilastrate [2,15] Sez. R: By=30.00 cm Bz=50.00 cm L=481.60 cm Ln=481.60 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	76.89	33.23	--	3.44	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	2.2
48.16	50.84	35.64	26.05	1.70	10.05	6.03	171.20	104.01	(22+23)-IV-2	(22+23)-IV-3	2.2
CAMP	33.70	68.09	31.50	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.5
433.44	62.28	36.26	33.83	12.75	10.05	6.03	171.20	104.01	(22+23)-IV-3	21	1.8
FLN	96.11	35.90	--	7.94	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.84	46.50	0.341	11.56	46.50	0.249	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
48.16	15.84	46.50	0.341	11.56	46.50	0.249	171.20	104.01	(22+23)-IV-2	(22+23)-IV-3	Parz.	Parz.
CAMP	15.77	46.50	0.339	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
433.44	15.95	46.50	0.343	11.61	46.50	0.250	171.20	104.01	(22+23)-IV-3	21	Parz.	Parz.
FLN	15.95	46.50	0.343	11.59	46.50	0.249	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	107.93	--	442.88	175.61	175.61	68.57	104.01	75.00	10.72	1.6
Cen	95.95	--	442.88	96.84	96.84	--	--	--	5.91	1.0
Des	116.04	--	442.88	175.61	175.61	68.57	171.20	75.00	10.72	1.5

Trave: 111 [115,121], Pilastrate [15,21] Sez. R: By=30.00 cm Bz=50.00 cm L=430.70 cm Ln=430.70 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	73.75	46.02	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	2.3
43.07	52.37	43.77	21.37	2.26	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	2.3
CAMP	36.68	58.42	26.56	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.8
387.63	58.12	53.09	23.84	0.73	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.9
FLN	81.96	50.77	--	2.51	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.82	46.50	0.340	11.60	46.50	0.249	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
43.07	15.82	46.50	0.340	11.60	46.50	0.249	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
CAMP	15.76	46.50	0.339	11.64	46.50	0.250	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
387.63	15.87	46.50	0.341	11.62	46.50	0.250	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.
FLN	15.87	46.50	0.341	11.62	46.50	0.250	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	105.68	--	442.88	175.61	175.61	76.68	104.01	75.00	10.72	1.7
Cen	94.11	--	442.88	96.97	96.97	--	--	--	5.92	1.0
Des	104.88	--	442.88	175.61	175.61	76.68	171.20	75.00	10.72	1.7

Trave: 111 [121,124], Pilastrate [21,24] Sez. R: By=30.00 cm Bz=50.00 cm L=287.70 cm Ln=287.70 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	67.77	59.36	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	1.8
28.77	50.36	50.48	17.41	8.88	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	1.8
CAMP	40.37	62.51	32.66	6.33	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.5
258.93	57.83	66.28	18.57	3.12	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.5
FLN	76.40	69.41	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.79	46.50	0.340	11.65	46.50	0.250	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
28.77	15.79	46.50	0.340	11.65	46.50	0.250	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
CAMP	15.82	46.50	0.340	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-	6	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
									3			
258.93	15.84	46.50	0.341	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.
FLN	15.84	46.50	0.341	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	134.15	--	442.88	175.61	175.61	114.79	104.01	75.00	10.72	1.3
Cen	122.53	--	442.88	131.51	131.51	--	--	--	8.03	1.1
Des	134.15	--	442.88	175.61	175.61	114.79	171.20	75.00	10.72	1.3

Trave: 111 [124,129], Pilastrate [24,29] Sez. R: By=30.00 cm Bz=50.00 cm L=439.90 cm Ln=439.90 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	69.96	14.92	--	4.35	10.05	6.03	171.20	104.01	(22+23)-VIII-4	(24+25)-VIII-1	2.4
43.99	47.97	11.38	21.99	13.30	10.05	6.03	171.20	104.01	(22+23)-VIII-4	6	2.4
CAMP	28.51	67.54	23.63	--	10.05	6.03	171.20	104.01	(22+23)-VIII-4	20	1.5
395.91	34.50	59.77	18.19	6.19	10.05	6.03	171.20	104.01	(22+23)-VIII-1	20	1.6
FLN	52.69	50.22	--	10.66	10.05	6.03	171.20	104.01	(22+23)-VIII-1	20	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.80	46.50	0.340	11.50	46.50	0.247	171.20	104.01	(22+23)-VIII-4	(24+25)-VIII-1	Parz.	Parz.
43.99	15.80	46.50	0.340	11.52	46.50	0.248	171.20	104.01	(22+23)-VIII-4	6	Parz.	Parz.
CAMP	15.70	46.50	0.338	11.68	46.50	0.251	171.20	104.01	(22+23)-VIII-4	20	Parz.	Parz.
395.91	15.71	46.50	0.338	11.67	46.50	0.251	171.20	104.01	(22+23)-VIII-1	20	Parz.	Parz.
FLN	15.71	46.50	0.338	11.65	46.50	0.251	171.20	104.01	(22+23)-VIII-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	103.98	--	442.88	175.61	175.61	75.07	104.01	75.00	10.72	1.7
Cen	92.92	--	442.88	98.83	98.83	--	--	--	6.03	1.1
Des	103.98	--	442.88	175.61	175.61	75.07	171.20	75.00	10.72	1.7

Trave: 112 [113,122], Pilastrate [13,22] Sez. R: By=30.00 cm Bz=50.00 cm L=466.53 cm Ln=461.17 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	86.35	33.30	--	5.17	10.05	6.03	171.20	104.01	(22+23)-IV-2	(22+23)-IV-3	2.0
46.12	57.20	17.46	29.15	24.78	10.05	6.03	171.20	104.01	(22+23)-IV-2	20	2.0
CAMP	39.45	72.67	35.68	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.4
415.05	70.23	41.96	36.47	4.96	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.6
FLN	106.70	35.28	--	7.30	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.89	46.50	0.342	11.57	46.50	0.249	171.20	104.01	(22+23)-IV-2	(22+23)-IV-3	Parz.	Parz.
46.12	15.89	46.50	0.342	11.58	46.50	0.249	171.20	104.01	(22+23)-IV-2	20	Parz.	Parz.
CAMP	15.83	46.50	0.340	11.70	46.50	0.252	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
415.05	16.02	46.50	0.344	11.60	46.50	0.249	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.
FLN	16.02	46.50	0.344	11.58	46.50	0.249	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	115.15	--	442.88	175.61	175.61	71.61	104.01	75.00	10.72	1.5
Cen	101.92	--	442.88	104.43	104.43	--	--	--	6.38	1.0
Des	126.17	--	442.88	175.61	175.61	71.61	171.20	75.00	10.72	1.4

Trave: 112 [122,125], Pilastrate [22,25] Sez. R: By=30.00 cm Bz=50.00 cm L=289.26 cm Ln=287.70 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	103.78	86.67	--	--	10.05	6.03	171.20	104.01	(22+23)-VIII-4	(24+25)-VIII-1	1.2
28.77	74.85	75.67	28.93	11.00	10.05	6.03	171.20	104.01	(22+23)-VIII-4	(24+25)-VIII-1	1.2
CAMP	64.09	62.55	57.57	22.12	10.05	6.03	171.20	104.01	(22+23)-IV-3	(24+25)-VIII-1	1.2
258.93	94.56	66.39	33.12	7.20	10.05	6.03	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	1.3
FLN	127.67	73.59	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.00	46.50	0.344	11.75	46.50	0.253	171.20	104.01	(22+23)-VIII-4	(24+25)-VIII-1	Parz.	Parz.
28.77	16.00	46.50	0.344	11.75	46.50	0.253	171.20	104.01	(22+23)-VIII-4	(24+25)-VIII-1	Parz.	Parz.
CAMP	16.11	46.50	0.346	11.74	46.50	0.253	171.20	104.01	(22+23)-IV-3	(24+25)-VIII-1	Parz.	Parz.
258.93	16.15	46.50	0.347	11.70	46.50	0.252	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.
FLN	16.15	46.50	0.347	11.70	46.50	0.252	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	159.01	--	442.88	175.61	175.61	114.79	104.01	75.00	10.72	1.1
Cen	133.34	--	442.88	137.19	137.19	--	--	--	8.38	1.0
Des	160.56	--	442.88	175.61	175.61	114.79	171.20	75.00	10.72	1.1

Trave: 112 [125,130], Pilastrate [25,30] Sez. R: By=60.00 cm Bz=25.00 cm L=440.01 cm Ln=440.13 cm Criterio : Travi spessore - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
ILN	36.66	3.51	--	4.46	22.12	12.06	173.53	96.99	(22+23)-IV-2	6	4.7
44.01	23.09	11.27	7.81	3.87	22.12	12.06	173.53	96.99	(22+23)-IV-2	6	5.6
CAMP	12.89	39.36	6.89	--	12.06	12.06	96.94	96.94	(22+23)-VIII-1	20	2.5
396.11	24.87	27.37	8.06	1.56	12.06	12.06	96.94	96.94	(22+23)-VIII-1	6	2.9
FLN	38.89	23.46	--	2.25	12.06	12.06	96.94	96.94	(22+23)-VIII-1	6	2.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	9.93	22.50	0.441	6.84	22.50	0.304	173.53	96.99	(22+23)-IV-2	6	Parz.	Parz.
44.01	9.91	22.50	0.440	6.85	22.50	0.304	173.53	96.99	(22+23)-IV-2	6	Parz.	Parz.
CAMP	7.71	22.50	0.343	7.79	22.50	0.346	96.94	96.94	(22+23)-VIII-1	20	Parz.	Parz.
396.11	7.76	22.50	0.345	7.74	22.50	0.344	96.94	96.94	(22+23)-VIII-1	6	Parz.	Parz.
FLN	7.78	22.50	0.346	7.73	22.50	0.344	96.94	96.94	(22+23)-VIII-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	96.62	--	428.59	297.40	297.40	73.74	173.53	37.50	37.53	3.1
Cen	94.12	--	428.59	99.57	99.57	--	--	--	12.57	1.1
Des	97.50	--	428.59	297.40	297.40	73.74	96.94	37.50	37.53	3.1

Trave: 113 [123,126], Pilastrate [23,26] Sez. R: By=30.00 cm Bz=50.00 cm L=142.97 cm Ln=165.76 cm Criterio : Travi tozze - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	95.27	111.09	--	--	10.05	8.04	171.47	137.84	(24+25)-VI-2	(22+23)-VI-3	1.2
16.58	75.00	91.76	20.27	19.33	10.05	8.04	171.47	137.84	(24+25)-VI-2	(22+23)-VI-3	1.2
CAMP	74.99	50.46	52.77	60.63	10.05	8.04	171.47	137.84	(22+23)-VIII-1	(22+23)-VI-3	1.2
149.18	100.92	62.14	26.84	12.60	10.05	8.04	171.47	137.84	(22+23)-VIII-1	(24+25)-VIII-4	1.3
FLN	127.76	74.73	--	--	10.05	8.04	171.47	137.84	(22+23)-VIII-1	(24+25)-VIII-4	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.38	46.50	0.331	13.52	46.50	0.291	171.47	137.84	(24+25)-VI-2	(22+23)-VI-3	Parz.	Parz.
16.58	15.38	46.50	0.331	13.52	46.50	0.291	171.47	137.84	(24+25)-VI-2	(22+23)-VI-3	Parz.	Parz.
CAMP	15.55	46.50	0.334	13.52	46.50	0.291	171.47	137.84	(22+23)-VIII-1	(22+23)-VI-3	Parz.	Parz.
149.18	15.55	46.50	0.334	13.36	46.50	0.287	171.47	137.84	(22+23)-VIII-1	(24+25)-VIII-4	Parz.	Parz.
FLN	15.55	46.50	0.334	13.36	46.50	0.287	171.47	137.84	(22+23)-VIII-1	(24+25)-VIII-4	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	251.88	--	442.88	276.90	276.90	223.92	137.84	165.76	16.91	1.1
Des							171.47			

Trave: 113 [126,131], Pilastrate [26,31] Sez. R: By=30.00 cm Bz=50.00 cm L=439.90 cm Ln=439.90 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	67.18	52.32	--	--	10.05	8.04	171.47	137.84	(22+23)-VIII-4	(24+25)-VIII-1	2.6
43.99	46.35	50.02	20.83	2.30	10.05	8.04	171.47	137.84	(22+23)-VIII-4	(24+25)-VIII-1	2.6
CAMP	30.43	67.12	26.65	--	10.05	8.04	171.47	137.84	(22+23)-VIII-1	20	2.1
395.91	52.43	41.77	24.53	13.71	10.05	8.04	171.47	137.84	(22+23)-VIII-1	20	2.2
FLN	76.96	49.64	--	3.87	10.05	8.04	171.47	137.84	(22+23)-VIII-1	6	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.24	46.50	0.328	13.27	46.50	0.285	171.47	137.84	(22+23)-VIII-4	(24+25)-VIII-1	Parz.	Parz.
43.99	15.24	46.50	0.328	13.27	46.50	0.285	171.47	137.84	(22+23)-VIII-4	(24+25)-VIII-1	Parz.	Parz.
CAMP	15.20	46.50	0.327	13.33	46.50	0.287	171.47	137.84	(22+23)-VIII-1	20	Parz.	Parz.
395.91	15.29	46.50	0.329	13.29	46.50	0.286	171.47	137.84	(22+23)-VIII-1	20	Parz.	Parz.
FLN	15.29	46.50	0.329	13.28	46.50	0.286	171.47	137.84	(22+23)-VIII-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	112.20	--	442.88	175.61	175.61	84.38	137.84	75.00	10.72	1.6
Cen	102.32	--	442.88	102.89	102.89	--	--	--	6.28	1.0
Des	113.18	--	442.88	175.61	175.61	84.38	171.47	75.00	10.72	1.6

Trave: 114 [116,114], Pilastrate [16,14] Sez. R: By=30.00 cm Bz=50.00 cm L=310.00 cm Ln=310.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	61.42	44.01	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	2.4
31.00	49.34	36.62	12.07	7.39	10.05	6.03	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	2.4
CAMP	37.79	28.74	19.86	12.96	10.05	6.03	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	2.5
279.00	42.42	27.90	12.31	7.17	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	3.0
FLN	54.73	35.07	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	3.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.75	46.50	0.339	11.59	46.50	0.249	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.
31.00	15.75	46.50	0.339	11.59	46.50	0.249	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.
CAMP	15.73	46.50	0.338	11.58	46.50	0.249	171.20	104.01	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.
279.00	15.72	46.50	0.338	11.56	46.50	0.249	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
FLN	15.72	46.50	0.338	11.56	46.50	0.249	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	115.28	--	442.88	175.61	175.61	106.53	104.01	75.00	10.72	1.5
Cen	110.21	--	442.88	117.59	117.59	--	--	--	7.18	1.1
Des	115.28	--	442.88	175.61	175.61	106.53	171.20	75.00	10.72	1.5

Trave: 115 [113,109], Pilastrate [13,9] Sez. R: By=60.00 cm Bz=25.00 cm L=310.56 cm Ln=310.56 cm
Criterio : Travi spessore - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	44.60	18.30	--	1.81	12.06	12.06	96.94	96.94	(22+23)-IV-3	6	2.2
31.06	31.12	20.52	10.98	1.45	12.06	12.06	96.94	96.94	(22+23)-IV-3	6	2.3
CAMP	19.09	31.12	9.81	--	12.06	12.06	96.94	96.94	(22+23)-IV-3	20	3.1
279.51	20.16	19.89	7.70	4.90	12.06	12.06	96.94	96.94	(22+23)-IV-2	20	3.5
FLN	29.60	22.22	--	--	12.06	12.06	96.94	96.94	(22+23)-IV-2	(24+25)-IV-3	3.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	7.81	22.50	0.347	7.71	22.50	0.343	96.94	96.94	(22+23)-IV-3	6	Parz.	Parz.
31.06	7.80	22.50	0.347	7.72	22.50	0.343	96.94	96.94	(22+23)-IV-3	6	Parz.	Parz.
CAMP	7.74	22.50	0.344	7.75	22.50	0.345	96.94	96.94	(22+23)-IV-3	20	Parz.	Parz.
279.51	7.74	22.50	0.344	7.73	22.50	0.343	96.94	96.94	(22+23)-IV-2	20	Parz.	Parz.
FLN	7.75	22.50	0.344	7.72	22.50	0.343	96.94	96.94	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	98.95	--	428.59	297.40	297.40	74.91	96.94	37.50	37.53	3.0
Cen	89.91	--	428.59	93.72	93.72	--	--	--	11.83	1.0
Des	98.91	--	428.59	297.40	297.40	74.91	96.94	37.50	37.53	3.0

Trave: 116 [108,103], Pilastrate [8,3] Sez. R: By=30.00 cm Bz=50.00 cm L=305.05 cm Ln=305.05 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	96.91	52.50	--	--	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	1.8
30.50	76.09	45.24	20.82	7.26	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	1.8
CAMP	55.90	50.95	35.07	26.35	10.05	6.03	171.20	104.01	(22+23)-III-3	(22+23)-III-3	1.3
274.54	35.57	66.53	12.69	15.06	10.05	6.03	171.20	104.01	(24+25)-III-2	(22+23)-III-3	1.3
FLN	48.26	81.59	--	--	10.05	6.03	171.20	104.01	(24+25)-III-2	(22+23)-III-3	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.96	46.50	0.343	11.62	46.50	0.250	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
30.50	15.96	46.50	0.343	11.62	46.50	0.250	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
CAMP	15.92	46.50	0.342	11.72	46.50	0.252	171.20	104.01	(22+23)-III-3	(22+23)-III-3	Parz.	Parz.
274.5	15.68	46.50	0.337	11.73	46.50	0.252	171.20	104.01	(24+25)-III-	(22+23)-III-	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
4									2	3		
FLN	15.68	46.50	0.337	11.73	46.50	0.252	171.20	104.01	(24+25)-III-2	(22+23)-III-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	118.71	--	442.88	175.61	175.61	108.26	104.01	75.00	10.72	1.5
Cen	112.70	--	442.88	117.59	117.59	--	--	--	7.18	1.0
Des	117.99	--	442.88	175.61	175.61	108.26	171.20	75.00	10.72	1.5

Trave: 117 [117,118], Pilastrate [17,18] Sez. R: By=30.00 cm Bz=50.00 cm L=179.02 cm Ln=201.49 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	125.73	87.55	--	--	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	1.2
20.15	99.97	71.67	25.76	15.88	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	1.2
CAMP	75.15	54.66	50.58	36.51	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-3	1.1
181.34	86.35	73.19	23.46	17.98	10.05	6.03	171.20	104.01	(22+23)-V-2	(24+25)-V-3	1.1
FLN	109.81	91.17	--	--	10.05	6.03	171.20	104.01	(22+23)-V-2	(24+25)-V-3	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.14	46.50	0.347	11.76	46.50	0.253	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
20.15	16.14	46.50	0.347	11.76	46.50	0.253	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
CAMP	16.14	46.50	0.347	11.77	46.50	0.253	171.20	104.01	(22+23)-V-3	(24+25)-V-3	Parz.	Parz.
181.34	16.04	46.50	0.345	11.77	46.50	0.253	171.20	104.01	(22+23)-V-2	(24+25)-V-3	Parz.	Parz.
FLN	16.04	46.50	0.345	11.77	46.50	0.253	171.20	104.01	(22+23)-V-2	(24+25)-V-3	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	187.24	--	442.88	205.79	205.79	163.91	104.01	201.49	12.57	1.1
Des							171.20			

Trave: 117 [118,119], Pilastrate [18,19] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	85.69	56.06	--	--	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	1.9
42.70	56.61	40.20	29.08	17.77	10.05	6.03	171.20	104.01	(22+23)-V-3	20	1.8
CAMP	58.60	70.05	38.89	--	10.05	6.03	171.20	104.01	(22+23)-V-2	20	1.5
384.30	89.65	43.09	34.83	--	10.05	6.03	171.20	104.01	(22+23)-V-2	(24+25)-V-3	1.4
FLN	124.48	35.57	--	5.15	10.05	6.03	171.20	104.01	(22+23)-V-2	(22+23)-V-3	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.89	46.50	0.342	11.63	46.50	0.250	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
42.70	15.89	46.50	0.342	11.64	46.50	0.250	171.20	104.01	(22+23)-V-3	20	Parz.	Parz.
CAMP	15.96	46.50	0.343	11.69	46.50	0.251	171.20	104.01	(22+23)-V-2	20	Parz.	Parz.
384.3	16.13	46.50	0.347	11.59	46.50	0.249	171.20	104.01	(22+23)-V-2	(24+25)-V-3	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
0												
FLN	16.13	46.50	0.347	11.58	46.50	0.249	171.20	104.01	(22+23)-V-2	(22+23)-V-3	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	120.97	--	442.88	175.61	175.61	77.34	104.01	75.00	10.72	1.5
Cen	103.96	--	442.88	109.75	109.75	--	--	--	6.70	1.1
Des	121.65	--	442.88	175.61	175.61	77.34	171.20	75.00	10.72	1.4

Trave: 117 [119,120], Pilastrate [19,20] Sez. R: By=60.00 cm Bz=25.00 cm L=530.00 cm Ln=530.00 cm Criterio : Travi spessore - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	37.34	0.59	--	4.50	24.13	14.07	189.27	112.72	(22+23)-V-3	6	5.1
53.00	22.22	10.01	7.22	3.79	24.13	14.07	189.27	112.72	(22+23)-V-3	6	6.4
CAMP	9.42	41.63	6.11	--	14.07	14.07	112.63	112.63	(22+23)-V-3	20	2.7
477.00	19.76	24.52	7.15	2.06	14.07	14.07	112.63	112.63	(22+23)-V-2	6	4.2
FLN	34.74	18.57	--	2.84	14.07	14.07	112.63	112.63	(22+23)-V-2	6	3.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	10.06	22.50	0.447	7.17	22.50	0.319	189.27	112.72	(22+23)-V-3	6	Parz.	Parz.
53.00	10.03	22.50	0.446	7.19	22.50	0.320	189.27	112.72	(22+23)-V-3	6	Parz.	Parz.
CAMP	8.01	22.50	0.356	8.11	22.50	0.360	112.63	112.63	(22+23)-V-3	20	Parz.	Parz.
477.00	8.05	22.50	0.358	8.05	22.50	0.358	112.63	112.63	(22+23)-V-2	6	Parz.	Parz.
FLN	8.08	22.50	0.359	8.03	22.50	0.357	112.63	112.63	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	92.47	--	428.59	297.40	297.40	68.35	189.27	37.50	37.53	3.2
Cen	89.33	--	428.59	93.72	93.72	--	--	--	11.83	1.0
Des	93.25	--	428.59	297.40	297.40	68.35	112.63	37.50	37.53	3.2

Trave: 118 [127,128], Pilastrate [27,28] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=500.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	66.69	29.26	--	3.23	10.05	6.03	171.20	104.01	(22+23)-V-3	(22+23)-V-2	2.6
50.00	44.38	32.79	22.31	--	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	2.6
CAMP	32.41	73.00	22.98	3.27	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.4
450.00	54.24	76.21	24.90	1.40	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.3
FLN	79.13	77.61	--	--	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.78	46.50	0.339	11.55	46.50	0.248	171.20	104.01	(22+23)-V-3	(22+23)-V-2	Parz.	Parz.
50.00	15.78	46.50	0.339	11.55	46.50	0.248	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
CAMP	15.72	46.50	0.338	11.71	46.50	0.252	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
450.00	15.85	46.50	0.341	11.72	46.50	0.252	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.
FLN	15.85	46.50	0.341	11.72	46.50	0.252	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	96.83	--	442.88	175.61	175.61	66.05	104.01	75.00	10.72	1.8
Cen	84.89	--	442.88	86.65	86.65	--	--	--	5.29	1.0
Des	96.83	--	442.88	175.61	175.61	66.05	171.20	75.00	10.72	1.8

Trave: 119 [110,111], Pilastrate [10,11] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	54.10	54.02	--	--	10.05	6.03	171.20	104.01	(24+25)-III-3	(22+23)-III-2	1.9
42.70	37.67	47.87	16.43	6.15	10.05	6.03	171.20	104.01	(24+25)-III-3	(22+23)-III-2	1.9
CAMP	43.14	53.57	24.90	--	10.05	6.03	171.20	104.01	(22+23)-III-2	20	1.9
384.30	63.14	43.46	21.75	2.39	10.05	6.03	171.20	104.01	(22+23)-III-2	6	2.0
FLN	84.89	40.19	--	3.75	10.05	6.03	171.20	104.01	(22+23)-III-2	6	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.71	46.50	0.338	11.63	46.50	0.250	171.20	104.01	(24+25)-III-3	(22+23)-III-2	Parz.	Parz.
42.70	15.71	46.50	0.338	11.63	46.50	0.250	171.20	104.01	(24+25)-III-3	(22+23)-III-2	Parz.	Parz.
CAMP	15.79	46.50	0.340	11.62	46.50	0.250	171.20	104.01	(22+23)-III-2	20	Parz.	Parz.
384.30	15.89	46.50	0.342	11.60	46.50	0.249	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.
FLN	15.89	46.50	0.342	11.59	46.50	0.249	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	96.64	--	442.88	175.61	175.61	77.34	104.01	75.00	10.72	1.8
Cen	89.67	--	442.88	93.31	93.31	--	--	--	5.70	1.0
Des	97.80	--	442.88	175.61	175.61	77.34	171.20	75.00	10.72	1.8

Trave: 119 [111,112], Pilastrate [11,12] Sez. R: By=30.00 cm Bz=50.00 cm L=530.00 cm Ln=530.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	63.97	25.70	--	3.26	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	2.7
53.00	44.30	15.20	19.42	16.97	10.05	6.03	171.20	104.01	(22+23)-III-3	20	2.7
CAMP	27.12	62.95	16.96	--	10.05	6.03	171.20	104.01	(22+23)-III-3	20	1.7
477.00	32.17	45.73	19.01	9.44	10.05	6.03	171.20	104.01	(22+23)-III-2	20	1.9
FLN	51.43	48.02	--	3.64	10.05	6.03	171.20	104.01	(22+23)-III-2	6	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.77	46.50	0.339	11.53	46.50	0.248	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
53.00	15.77	46.50	0.339	11.55	46.50	0.248	171.20	104.01	(22+23)-III-3	20	Parz.	Parz.
CAMP	15.66	46.50	0.337	11.66	46.50	0.251	171.20	104.01	(22+23)-III-3	20	Parz.	Parz.
477.00	15.70	46.50	0.338	11.63	46.50	0.250	171.20	104.01	(22+23)-III-2	20	Parz.	Parz.
FLN	15.70	46.50	0.338	11.62	46.50	0.250	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	85.94	--	442.88	175.61	175.61	62.31	104.01	75.00	10.72	2.0
Cen	77.20	--	442.88	79.48	79.48	--	--	--	4.85	1.0
Des	85.94	--	442.88	175.61	175.61	62.31	171.20	75.00	10.72	2.0

Trave: 120 [105,110], Pilastrate [5,10] Sez. R: By=30.00 cm Bz=50.00 cm L=378.19 cm Ln=379.38 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	83.37	49.53	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-4	(24+25)-VI-1	2.1
37.94	53.24	31.24	30.13	23.66	10.05	6.03	171.20	104.01	(22+23)-VI-4	20	1.9
CAMP	59.66	68.01	48.77	--	10.05	6.03	171.20	104.01	(22+23)-VI-1	20	1.5
341.44	93.85	29.55	38.47	9.98	10.05	6.03	171.20	104.01	(22+23)-VI-1	6	1.3
FLN	132.32	23.82	--	9.14	10.05	6.03	171.20	104.01	(22+23)-VI-1	(24+25)-VI-4	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.88	46.50	0.341	11.61	46.50	0.250	171.20	104.01	(22+23)-VI-4	(24+25)-VI-1	Parz.	Parz.
37.94	15.88	46.50	0.341	11.63	46.50	0.250	171.20	104.01	(22+23)-VI-4	20	Parz.	Parz.
CAMP	16.03	46.50	0.345	11.68	46.50	0.251	171.20	104.01	(22+23)-VI-1	20	Parz.	Parz.
341.44	16.18	46.50	0.348	11.57	46.50	0.249	171.20	104.01	(22+23)-VI-1	6	Parz.	Parz.
FLN	16.18	46.50	0.348	11.55	46.50	0.248	171.20	104.01	(22+23)-VI-1	(24+25)-VI-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	141.81	--	442.88	175.61	175.61	87.05	104.01	75.00	10.72	1.2
Cen	123.74	--	442.88	132.20	132.20	--	--	--	8.07	1.1
Des	145.11	--	442.88	175.61	175.61	87.05	171.20	75.00	10.72	1.2

Trave: 120 [110,118], Pilastrate [10,18] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	135.24	40.83	--	11.77	10.05	6.03	171.20	104.01	(22+23)-VI-4	(24+25)-VI-1	1.3

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
46.99	88.19	49.78	47.05	7.44	10.05	6.03	171.20	104.01	(22+23)-VI-4	(22+23)-VI-1	1.3
CAMP	48.21	87.40	45.30	--	10.05	6.03	171.20	104.01	(22+23)-VI-4	20	1.2
422.91	75.09	47.46	41.23	3.58	10.05	6.03	171.20	104.01	(22+23)-VI-1	(22+23)-VI-4	1.5
FLN	116.33	42.45	--	6.39	10.05	6.03	171.20	104.01	(22+23)-VI-1	(24+25)-VI-4	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.20	46.50	0.348	11.62	46.50	0.250	171.20	104.01	(22+23)-VI-4	(24+25)-VI-1	Parz.	Parz.
46.99	16.20	46.50	0.348	11.64	46.50	0.250	171.20	104.01	(22+23)-VI-4	(22+23)-VI-1	Parz.	Parz.
CAMP	15.94	46.50	0.343	11.76	46.50	0.253	171.20	104.01	(22+23)-VI-4	20	Parz.	Parz.
422.91	16.08	46.50	0.346	11.61	46.50	0.250	171.20	104.01	(22+23)-VI-1	(22+23)-VI-4	Parz.	Parz.
FLN	16.08	46.50	0.346	11.61	46.50	0.250	171.20	104.01	(22+23)-VI-1	(24+25)-VI-4	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	140.91	--	442.88	175.61	175.61	70.28	104.01	75.00	10.72	1.2
Cen	110.78	--	442.88	119.26	119.26	--	--	--	7.28	1.1
Des	128.10	--	442.88	175.61	175.61	70.28	171.20	75.00	10.72	1.4

Trave: 121 [104,114], Pilastrate [4,14] Sez. R: By=30.00 cm Bz=50.00 cm L=461.53 cm Ln=503.95 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	89.74	19.27	--	14.56	10.05	6.03	171.20	104.01	(22+23)-IV-2	6	1.9
50.40	53.44	22.34	36.30	32.35	10.05	6.03	171.20	104.01	(22+23)-IV-2	20	1.9
CAMP	23.37	90.58	33.88	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.1
453.56	55.80	34.32	38.17	11.02	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.8
FLN	93.97	20.79	--	13.94	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.91	46.50	0.342	11.55	46.50	0.248	171.20	104.01	(22+23)-IV-2	6	Parz.	Parz.
50.40	15.91	46.50	0.342	11.63	46.50	0.250	171.20	104.01	(22+23)-IV-2	20	Parz.	Parz.
CAMP	15.73	46.50	0.338	11.77	46.50	0.253	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
453.56	15.94	46.50	0.343	11.59	46.50	0.249	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.
FLN	15.94	46.50	0.343	11.55	46.50	0.248	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	125.07	--	442.88	175.61	175.61	65.53	104.01	75.00	10.72	1.4
Cen	103.32	--	442.88	111.43	111.43	--	--	--	6.80	1.1
Des	124.54	--	442.88	175.61	175.61	65.53	171.20	75.00	10.72	1.4

Trave: 122 [36,35], Pilastrate [23,17] Sez. R: By=30.00 cm Bz=50.00 cm L=310.00 cm Ln=310.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	126.80	86.74	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-3	(24+25)-VI-2	1.2
31.00	95.52	74.53	31.28	12.20	10.05	6.03	171.20	104.01	(22+23)-VI-3	(24+25)-VI-2	1.2
CAMP	66.37	63.67	50.65	24.44	10.05	6.03	171.20	104.01	(22+23)-VI-3	(24+25)-VI-3	1.2
279.00	89.88	78.90	29.97	13.40	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	1.1
FLN	119.86	92.30	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	1.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.14	46.50	0.347	11.75	46.50	0.253	171.20	104.01	(22+23)-VI-3	(24+25)-VI-2	Parz.	Parz.
31.00	16.14	46.50	0.347	11.75	46.50	0.253	171.20	104.01	(22+23)-VI-3	(24+25)-VI-2	Parz.	Parz.
CAMP	16.08	46.50	0.346	11.76	46.50	0.253	171.20	104.01	(22+23)-VI-3	(24+25)-VI-3	Parz.	Parz.
279.00	16.10	46.50	0.346	11.78	46.50	0.253	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.
FLN	16.10	46.50	0.346	11.78	46.50	0.253	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	140.94	--	444.22	174.32	174.32	106.53	104.01	310.00	10.64	1.2
Des							171.20			

Trave: 123 [39,116], Pilastrate [--,16] Sez. R: By=30.00 cm Bz=50.00 cm L=398.55 cm Ln=345.39 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	30.46	49.23	--	--	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	2.1
34.54	21.83	50.59	8.63	--	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	2.1
CAMP	14.44	49.13	11.83	1.45	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	2.1
310.86	-2.54	13.19	2.54	15.11	10.05	6.03	171.20	104.01	(24+25)-VII-4	1	3.7
FLN	--	--	--	18.75	10.05	6.03	171.20	104.01	(24+25)-VII-4	1	5.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.59	46.50	0.335	11.61	46.50	0.250	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
34.54	15.59	46.50	0.335	11.61	46.50	0.250	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
CAMP	15.57	46.50	0.335	11.61	46.50	0.250	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
310.86	--	--	--	11.53	46.50	0.248	171.20	104.01	(24+25)-VII-4	1	--	Parz.
FLN	--	--	--	11.50	46.50	0.247	171.20	104.01	(24+25)-VII-4	1	--	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	115.83	--	442.88	175.61	175.61	95.62	104.01	75.00	10.72	1.5
Cen	103.70	--	442.88	109.75	109.75	--	--	--	6.70	1.1
Des	115.83	--	442.88	175.61	175.61	95.62	171.20	75.00	10.72	1.5

Trave: 123 [36,39], Pilastrate [23,--] Sez. R: By=30.00 cm Bz=50.00 cm L=173.00 cm Ln=143.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	--	8.49	20.90	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	5.0
14.30	1.99	6.09	9.39	19.89	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	4.0
CAMP	22.77	40.98	8.15	7.48	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	2.1
128.70	26.72	44.86	4.20	3.60	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	2.1
FLN	30.91	48.46	--	--	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	2.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.48	46.50	0.333	11.51	46.50	0.247	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
14.30	15.49	46.50	0.333	11.52	46.50	0.248	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
CAMP	15.59	46.50	0.335	11.61	46.50	0.250	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
128.70	15.59	46.50	0.335	11.61	46.50	0.250	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
FLN	15.59	46.50	0.335	11.61	46.50	0.250	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	240.60	--	442.88	276.60	276.60	230.95	104.01	143.00	16.89	1.1
Des							171.20			

Trave: 201 [225,226], Pilastrate [25,26] Sez. R: By=30.00 cm Bz=50.00 cm L=604.50 cm Ln=604.50 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	76.35	7.62	--	14.26	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	2.2
60.45	41.61	23.07	30.06	11.37	10.05	6.03	171.20	104.01	(22+23)-V-3	(22+23)-V-2	2.4
CAMP	12.96	85.28	24.80	--	10.05	6.03	171.20	104.01	(22+23)-V-3	20	1.2
544.05	35.25	46.12	27.33	18.00	10.05	6.03	171.20	104.01	(22+23)-V-2	20	1.6
FLN	66.84	47.23	--	4.16	10.05	6.03	171.20	104.01	(22+23)-V-2	6	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato+
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.84	46.50	0.341	11.51	46.50	0.248	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
60.45	15.81	46.50	0.340	11.55	46.50	0.248	171.20	104.01	(22+23)-V-3	(22+23)-V-2	Parz.	Parz.
CAMP	15.63	46.50	0.336	11.75	46.50	0.253	171.20	104.01	(22+23)-V-3	20	Parz.	Parz.
544.05	15.76	46.50	0.339	11.66	46.50	0.251	171.20	104.01	(22+23)-V-2	20	Parz.	Parz.
FLN	15.78	46.50	0.339	11.62	46.50	0.250	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4

Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	102.25	--	442.88	175.61	175.61	54.63	104.01	75.00	10.72	1.7
Cen	82.92	--	442.88	87.64	87.64	--	--	--	5.35	1.1
Des	99.02	--	442.88	175.61	175.61	54.63	171.20	75.00	10.72	1.8

Trave: 202 [213,216], Pilastrate [13,16] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	88.23	41.56	--	--	10.05	6.03	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	1.9
32.99	67.82	38.83	20.41	2.73	10.05	6.03	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	1.9
CAMP	48.57	69.48	31.21	15.09	10.05	6.03	171.20	104.01	(22+23)-VII-4	6	1.2
296.88	35.78	79.37	17.63	8.85	10.05	6.03	171.20	104.01	(22+23)-VII-1	6	1.2
FLN	53.41	88.23	--	--	10.05	6.03	171.20	104.01	(22+23)-VII-1	6	1.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.91	46.50	0.342	11.58	46.50	0.249	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	Parz.	Parz.
32.99	15.91	46.50	0.342	11.58	46.50	0.249	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	Parz.	Parz.
CAMP	15.86	46.50	0.341	11.74	46.50	0.253	171.20	104.01	(22+23)-VII-4	6	Parz.	Parz.
296.88	15.71	46.50	0.338	11.76	46.50	0.253	171.20	104.01	(22+23)-VII-1	6	Parz.	Parz.
FLN	15.71	46.50	0.338	11.76	46.50	0.253	171.20	104.01	(22+23)-VII-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	123.48	--	442.88	175.61	175.61	100.12	104.01	75.00	10.72	1.4
Cen	111.67	--	442.88	119.94	119.94	--	--	--	7.32	1.1
Des	128.57	--	442.88	175.61	175.61	100.12	171.20	75.00	10.72	1.4

Trave: 202 [216,223], Pilastrate [16,23] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	97.55	-6.36	--	17.89	10.05	6.03	171.20	104.01	5	6	1.8
53.25	49.23	11.85	47.47	15.65	10.05	6.03	171.20	104.01	5	6	1.8
CAMP	24.10	95.15	29.77	--	10.05	6.03	171.20	104.01	(22+23)-VII-4	20	1.1
479.27	27.36	51.66	30.33	23.98	10.05	6.03	171.20	104.01	(22+23)-VII-1	20	1.4
FLN	58.23	44.97	--	8.79	10.05	6.03	171.20	104.01	(22+23)-VII-1	6	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.96	46.50	0.343	11.47	46.50	0.247	171.20	104.01	5	6	Parz.	Parz.
53.25	15.96	46.50	0.343	11.53	46.50	0.248	171.20	104.01	5	6	Parz.	Parz.
CAMP	15.71	46.50	0.338	11.79	46.50	0.253	171.20	104.01	(22+23)-VII-4	20	Parz.	Parz.
479.27	15.73	46.50	0.338	11.71	46.50	0.252	171.20	104.01	(22+23)-VII-1	20	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
FLN	15.74	46.50	0.338	11.62	46.50	0.250	171.20	104.01	(22+23)-VII-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	113.48	--	442.88	175.61	175.61	62.02	104.01	75.00	10.72	1.5
Cen	96.47	--	442.88	96.84	96.84	--	--	--	5.91	1.0
Des	116.90	--	442.88	175.61	175.61	62.02	171.20	75.00	10.72	1.5

Trave: 203 [213,222], Pilastrate [13,22] Sez. R: By=30.00 cm Bz=50.00 cm L=466.53 cm Ln=461.17 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	72.47	12.71	--	12.66	10.05	6.03	171.20	104.01	(22+23)-VIII-4	6	2.4
46.12	48.02	17.44	24.45	17.75	10.05	6.03	171.20	104.01	(22+23)-VIII-4	21	2.4
CAMP	28.05	75.33	26.92	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.4
415.05	51.31	43.89	27.19	18.74	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.7
FLN	78.50	50.51	--	5.64	10.05	6.03	171.20	104.01	(22+23)-IV-3	6	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.81	46.50	0.340	11.52	46.50	0.248	171.20	104.01	(22+23)-VIII-4	6	Parz.	Parz.
46.12	15.81	46.50	0.340	11.56	46.50	0.249	171.20	104.01	(22+23)-VIII-4	21	Parz.	Parz.
CAMP	15.72	46.50	0.338	11.71	46.50	0.252	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
415.05	15.85	46.50	0.341	11.66	46.50	0.251	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
FLN	15.85	46.50	0.341	11.63	46.50	0.250	171.20	104.01	(22+23)-IV-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	107.85	--	442.88	175.61	175.61	71.61	104.01	75.00	10.72	1.6
Cen	97.15	--	442.88	104.43	104.43	--	--	--	6.38	1.1
Des	114.80	--	442.88	175.61	175.61	71.61	171.20	75.00	10.72	1.5

Trave: 203 [222,225], Pilastrate [22,25] Sez. R: By=30.00 cm Bz=50.00 cm L=289.26 cm Ln=347.70 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	80.60	32.33	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	2.1
34.77	56.64	31.97	23.96	0.35	10.05	6.03	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	2.1
CAMP	34.19	68.57	34.54	--	10.05	6.03	171.20	104.01	(22+23)-IV-2	20	1.5
312.93	54.17	51.35	24.43	13.66	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.6
FLN	78.60	47.36	--	9.53	10.05	6.03	171.20	104.01	(22+23)-IV-3	21	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.86	46.50	0.341	11.55	46.50	0.248	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
34.77	15.86	46.50	0.341	11.55	46.50	0.248	171.20	104.01	(22+23)-IV-2	(24+25)-IV-3	Parz.	Parz.
CAMP	15.79	46.50	0.340	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-2	20	Parz.	Parz.
312.93	15.85	46.50	0.341	11.67	46.50	0.251	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
FLN	15.85	46.50	0.341	11.64	46.50	0.250	171.20	104.01	(22+23)-IV-3	21	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	131.27	--	442.88	175.61	175.61	94.98	104.01	75.00	10.72	1.3
Cen	115.00	--	442.88	119.56	119.56	--	--	--	7.30	1.0
Des	137.69	--	442.88	175.61	175.61	94.98	171.20	75.00	10.72	1.3

Trave: 204 [223,226], Pilastrate [23,26] Sez. R: By=30.00 cm Bz=50.00 cm L=142.97 cm Ln=165.76 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	61.84	47.63	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	2.2
16.58	47.19	38.06	14.65	9.58	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	2.2
CAMP	53.33	60.48	31.68	10.76	10.05	6.03	171.20	104.01	(22+23)-VIII-1	6	1.5
149.18	68.85	66.01	16.17	5.23	10.05	6.03	171.20	104.01	(22+23)-VIII-1	6	1.5
FLN	85.02	71.24	--	--	10.05	6.03	171.20	104.01	(22+23)-VIII-1	6	1.5

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.76	46.50	0.339	11.60	46.50	0.250	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.
16.58	15.76	46.50	0.339	11.60	46.50	0.250	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.
CAMP	15.89	46.50	0.342	11.69	46.50	0.251	171.20	104.01	(22+23)-VIII-1	6	Parz.	Parz.
149.18	15.89	46.50	0.342	11.69	46.50	0.251	171.20	104.01	(22+23)-VIII-1	6	Parz.	Parz.
FLN	15.89	46.50	0.342	11.69	46.50	0.251	171.20	104.01	(22+23)-VIII-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	222.61	--	442.88	235.19	235.19	199.24	104.01	165.76	14.36	1.1
Des							171.20			

Trave: 205 [223,217], Pilastrate [23,17] Sez. R: By=30.00 cm Bz=50.00 cm L=310.00 cm Ln=310.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	91.49	56.85	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-3	6	1.8
31.00	70.01	54.57	21.48	2.28	10.05	6.03	171.20	104.01	(22+23)-VI-3	6	1.8
CAMP	49.93	51.62	34.85	4.52	10.05	6.03	171.20	104.01	(22+23)-VI-3	6	1.9

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
279.00	60.30	49.82	19.36	8.91	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	1.8
FLN	79.66	58.73	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.92	46.50	0.342	11.64	46.50	0.250	171.20	104.01	(22+23)-VI-3	6	Parz.	Parz.
31.00	15.92	46.50	0.342	11.64	46.50	0.250	171.20	104.01	(22+23)-VI-3	6	Parz.	Parz.
CAMP	15.89	46.50	0.342	11.63	46.50	0.250	171.20	104.01	(22+23)-VI-3	6	Parz.	Parz.
279.00	15.86	46.50	0.341	11.64	46.50	0.250	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.
FLN	15.86	46.50	0.341	11.64	46.50	0.250	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	129.68	--	442.88	174.32	174.32	106.53	104.01	310.00	10.64	1.3
Des							171.20			

Trave: 206 [217,218], Pilastrate [17,18] Sez. R: By=30.00 cm Bz=50.00 cm L=179.02 cm Ln=179.02 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	64.64	40.08	--	12.57	10.05	6.03	171.20	104.01	(22+23)-V-3	6	2.0
17.90	49.73	41.70	14.91	14.73	10.05	6.03	171.20	104.01	(22+23)-V-3	21	1.8
CAMP	35.41	68.81	29.22	4.38	10.05	6.03	171.20	104.01	(22+23)-V-3	6	1.4
161.11	47.75	71.14	12.15	2.05	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.4
FLN	59.90	73.19	--	--	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.77	46.50	0.339	11.62	46.50	0.250	171.20	104.01	(22+23)-V-3	6	Parz.	Parz.
17.90	15.77	46.50	0.339	11.63	46.50	0.250	171.20	104.01	(22+23)-V-3	21	Parz.	Parz.
CAMP	15.77	46.50	0.339	11.70	46.50	0.252	171.20	104.01	(22+23)-V-3	6	Parz.	Parz.
161.11	15.75	46.50	0.339	11.70	46.50	0.252	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.
FLN	15.75	46.50	0.339	11.70	46.50	0.252	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	200.57	--	442.88	205.79	205.79	184.48	104.01	179.02	12.57	1.0
Des							171.20			

Trave: 206 [218,219], Pilastrate [18,19] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	69.03	39.41	--	--	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	2.5
42.70	46.02	38.18	23.00	1.23	10.05	6.03	171.20	104.01	(22+23)-V-3	(24+25)-V-2	2.5
CAMP	40.55	63.66	28.03	--	10.05	6.03	171.20	104.01	(22+23)-V-2	20	1.6

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
384.30	62.92	53.68	25.16	0.81	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.9
FLN	88.07	51.24	--	2.68	10.05	6.03	171.20	104.01	(22+23)-V-2	6	1.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.80	46.50	0.340	11.57	46.50	0.249	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
42.70	15.80	46.50	0.340	11.57	46.50	0.249	171.20	104.01	(22+23)-V-3	(24+25)-V-2	Parz.	Parz.
CAMP	15.79	46.50	0.340	11.66	46.50	0.251	171.20	104.01	(22+23)-V-2	20	Parz.	Parz.
384.30	15.90	46.50	0.342	11.63	46.50	0.250	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.
FLN	15.90	46.50	0.342	11.63	46.50	0.250	171.20	104.01	(22+23)-V-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	109.35	--	442.88	175.61	175.61	77.34	104.01	75.00	10.72	1.6
Cen	96.98	--	442.88	106.21	106.21	--	--	--	6.49	1.1
Des	110.02	--	442.88	175.61	175.61	77.34	171.20	75.00	10.72	1.6

Trave: 207 [204,205], Pilastrate [4,5] Sez. R: By=30.00 cm Bz=50.00 cm L=590.40 cm Ln=590.40 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	118.87	17.30	--	11.16	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.4
59.04	79.90	29.89	34.53	6.89	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.5
CAMP	46.29	83.88	29.78	--	10.05	6.03	171.20	104.01	(22+23)-I-4	20	1.2
531.36	57.59	43.03	33.66	20.25	10.05	6.03	171.20	104.01	(22+23)-I-1	20	1.6
FLN	95.58	53.29	--	5.15	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.8

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.09	46.50	0.346	11.53	46.50	0.248	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
59.04	16.06	46.50	0.345	11.56	46.50	0.249	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.84	46.50	0.341	11.74	46.50	0.253	171.20	104.01	(22+23)-I-4	20	Parz.	Parz.
531.36	15.92	46.50	0.342	11.66	46.50	0.251	171.20	104.01	(22+23)-I-1	20	Parz.	Parz.
FLN	15.95	46.50	0.343	11.64	46.50	0.250	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	104.12	--	442.88	175.61	175.61	55.94	104.01	75.00	10.72	1.7
Cen	86.58	--	442.88	87.69	87.69	--	--	--	5.35	1.0
Des	106.38	--	442.88	175.61	175.61	55.94	171.20	75.00	10.72	1.7

Trave: 207 [205,206], Pilastrate [5,6] Sez. R: By=30.00 cm Bz=50.00 cm L=397.00 cm Ln=397.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	73.80	53.88	--	--	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.9
39.70	51.02	48.27	22.78	5.62	10.05	6.03	171.20	104.01	(22+23)-I-4	(24+25)-I-1	1.9
CAMP	48.72	61.60	30.95	2.56	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.6

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
357.30	71.66	63.82	25.21	1.08	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.6
FLN	96.87	64.89	--	--	10.05	6.03	171.20	104.01	(22+23)-I-1	6	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.82	46.50	0.340	11.63	46.50	0.250	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
39.70	15.82	46.50	0.340	11.63	46.50	0.250	171.20	104.01	(22+23)-I-4	(24+25)-I-1	Parz.	Parz.
CAMP	15.86	46.50	0.341	11.66	46.50	0.251	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.
357.30	15.96	46.50	0.343	11.67	46.50	0.251	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.
FLN	15.96	46.50	0.343	11.67	46.50	0.251	171.20	104.01	(22+23)-I-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	111.81	--	442.88	175.61	175.61	83.19	104.01	75.00	10.72	1.6
Cen	100.36	--	442.88	102.89	102.89	--	--	--	6.28	1.0
Des	111.81	--	442.88	175.61	175.61	83.19	171.20	75.00	10.72	1.6

Trave: 208 [209,214], Pilastrate [9,14] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	95.65	30.96	--	--	10.05	6.03	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	1.8
32.99	73.78	30.42	21.87	0.54	10.05	6.03	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	1.8
CAMP	53.37	71.64	33.22	8.95	10.05	6.03	171.20	104.01	(22+23)-VII-4	20	1.3
296.88	27.31	78.14	13.84	4.18	10.05	6.03	171.20	104.01	(24+25)-VII-1	20	1.3
FLN	41.15	82.32	--	--	10.05	6.03	171.20	104.01	(24+25)-VII-1	20	1.3

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.95	46.50	0.343	11.54	46.50	0.248	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	Parz.	Parz.
32.99	15.95	46.50	0.343	11.54	46.50	0.248	171.20	104.01	(22+23)-VII-4	(24+25)-VII-1	Parz.	Parz.
CAMP	15.90	46.50	0.342	11.73	46.50	0.252	171.20	104.01	(22+23)-VII-4	20	Parz.	Parz.
296.88	15.64	46.50	0.336	11.74	46.50	0.252	171.20	104.01	(24+25)-VII-1	20	Parz.	Parz.
FLN	15.64	46.50	0.336	11.74	46.50	0.252	171.20	104.01	(24+25)-VII-1	20	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	123.40	--	442.88	175.61	175.61	100.12	104.01	75.00	10.72	1.4
Cen	110.27	--	442.88	119.88	119.88	--	--	--	7.32	1.1
Des	124.53	--	442.88	175.61	175.61	100.12	171.20	75.00	10.72	1.4

Trave: 208 [214,217], Pilastrate [14,17] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	101.93	-13.39	--	20.73	10.05	6.03	171.20	104.01	5	6	1.7
53.25	49.69	7.71	51.32	18.29	10.05	6.03	171.20	104.01	5	6	1.7
CAMP	23.15	98.09	30.21	--	10.05	6.03	171.20	104.01	(22+23)-VII-4	20	1.1
479.27	32.39	54.89	29.27	23.03	10.05	6.03	171.20	104.01	(22+23)-VI-1	20	1.3
FLN	62.18	56.72	--	6.57	10.05	6.03	171.20	104.01	(22+23)-VI-1	6	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.99	46.50	0.344	11.46	46.50	0.246	171.20	104.01	5	6	Parz.	Parz.
53.25	15.98	46.50	0.344	11.52	46.50	0.248	171.20	104.01	5	6	Parz.	Parz.
CAMP	15.71	46.50	0.338	11.80	46.50	0.254	171.20	104.01	(22+23)-VII-4	20	Parz.	Parz.
479.27	15.75	46.50	0.339	11.72	46.50	0.252	171.20	104.01	(22+23)-VI-1	20	Parz.	Parz.
FLN	15.76	46.50	0.339	11.66	46.50	0.251	171.20	104.01	(22+23)-VI-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	116.52	--	442.88	175.61	175.61	62.02	104.01	75.00	10.72	1.5
Cen	98.52	--	442.88	102.89	102.89	--	--	--	6.28	1.0
Des	114.53	--	442.88	175.61	175.61	62.02	171.20	75.00	10.72	1.5

Trave: 209 [204,209], Pilastrate [4,9] Sez. R: By=30.00 cm Bz=50.00 cm L=322.79 cm Ln=322.79 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	38.91	63.28	--	--	10.05	6.03	171.20	104.01	(24+25)-III-2	(22+23)-III-3	1.6
32.28	27.33	58.94	11.57	4.34	10.05	6.03	171.20	104.01	(24+25)-III-2	(22+23)-III-3	1.6
CAMP	14.94	63.33	28.76	--	10.05	6.03	171.20	104.01	(22+23)-III-3	20	1.6
290.51	32.03	12.73	18.81	22.03	10.05	6.03	171.20	104.01	(22+23)-III-3	20	3.0
FLN	50.84	17.16	--	9.34	10.05	6.03	171.20	104.01	(22+23)-III-3	6	3.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.63	46.50	0.336	11.66	46.50	0.251	171.20	104.01	(24+25)-III-2	(22+23)-III-3	Parz.	Parz.
32.28	15.63	46.50	0.336	11.66	46.50	0.251	171.20	104.01	(24+25)-III-2	(22+23)-III-3	Parz.	Parz.
CAMP	15.66	46.50	0.337	11.66	46.50	0.251	171.20	104.01	(22+23)-III-3	20	Parz.	Parz.
290.51	15.70	46.50	0.338	11.55	46.50	0.248	171.20	104.01	(22+23)-III-3	20	Parz.	Parz.
FLN	15.70	46.50	0.338	11.53	46.50	0.248	171.20	104.01	(22+23)-III-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	126.38	--	442.88	175.61	175.61	102.31	104.01	75.00	10.72	1.4
Cen	112.47	--	442.88	119.47	119.47	--	--	--	7.30	1.1
Des	127.90	--	442.88	175.61	175.61	102.31	171.20	75.00	10.72	1.4

Trave: 209 [209,213], Pilastrate [9,13] Sez. R: By=30.00 cm Bz=50.00 cm L=310.56 cm Ln=310.56 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	34.51	67.69	--	--	10.05	6.03	171.20	104.01	(22+23)-IV-2	6	1.5
31.06	24.44	61.92	10.07	5.77	10.05	6.03	171.20	104.01	(22+23)-IV-2	6	1.5
CAMP	26.96	55.50	15.89	10.37	10.05	6.03	171.20	104.01	(22+23)-III-3	6	1.6
279.51	35.85	16.83	10.22	--	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	3.7
FLN	46.08	16.03	--	--	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	3.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.61	46.50	0.336	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-2	6	Parz.	Parz.
31.06	15.61	46.50	0.336	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-2	6	Parz.	Parz.
CAMP	15.65	46.50	0.337	11.67	46.50	0.251	171.20	104.01	(22+23)-III-3	6	Parz.	Parz.
279.51	15.67	46.50	0.337	11.49	46.50	0.247	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
FLN	15.67	46.50	0.337	11.49	46.50	0.247	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	128.13	--	442.88	175.61	175.61	106.34	104.01	75.00	10.72	1.4
Cen	115.26	--	442.88	117.59	117.59	--	--	--	7.18	1.0
Des	128.13	--	442.88	175.61	175.61	106.34	171.20	75.00	10.72	1.4

Trave: 210 [214,216], Pilastrate [14,16] Sez. R: By=60.00 cm Bz=25.00 cm L=310.00 cm Ln=310.00 cm
Criterio : Travi spessore - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	25.40	33.48	--	--	8.04	8.04	65.52	65.52	(22+23)-III-2	6	2.0
31.00	18.01	32.40	6.03	0.88	8.04	8.04	65.52	65.52	(22+23)-III-2	6	2.0
CAMP	11.40	30.84	5.40	1.27	8.04	8.04	65.52	65.52	(22+23)-III-2	6	2.0
279.00	16.29	10.43	5.21	--	8.04	8.04	65.52	65.52	(22+23)-IV-3	(24+25)-IV-2	3.0
FLN	22.67	10.19	--	--	8.04	8.04	65.52	65.52	(22+23)-IV-3	(24+25)-IV-2	2.9

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	6.89	22.50	0.306	6.93	22.50	0.308	65.52	65.52	(22+23)-III-2	6	Parz.	Parz.
31.00	6.88	22.50	0.306	6.93	22.50	0.308	65.52	65.52	(22+23)-III-2	6	Parz.	Parz.
CAMP	6.84	22.50	0.304	6.92	22.50	0.308	65.52	65.52	(22+23)-III-2	6	Parz.	Parz.
279.00	6.87	22.50	0.305	6.81	22.50	0.303	65.52	65.52	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.
FLN	6.87	22.50	0.305	6.81	22.50	0.303	65.52	65.52	(22+23)-IV-3	(24+25)-IV-2	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4

Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	64.29	--	428.59	297.40	297.40	50.72	65.52	37.50	37.53	4.6
Cen	59.59	--	428.59	91.04	91.04	--	--	--	11.49	1.5
Des	64.29	--	428.59	297.40	297.40	50.72	65.52	37.50	37.53	4.6

Trave: 211 [204,214], Pilastrate [4,14] Sez. R: By=30.00 cm Bz=50.00 cm L=461.53 cm Ln=503.95 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	73.18	-9.59	--	18.78	10.05	6.03	171.20	104.01	1	(24+25)-VI-1	2.3
50.40	25.85	7.18	47.33	16.39	10.05	6.03	171.20	104.01	1	(22+23)-VI-1	2.3
CAMP	12.42	69.40	27.30	--	10.05	6.03	171.20	104.01	(22+23)-IV-3	20	1.5
453.56	31.22	11.86	45.20	28.32	10.05	6.03	171.20	104.01	5	20	2.2
FLN	76.43	22.91	--	8.38	10.05	6.03	171.20	104.01	5	6	2.2

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.82	46.50	0.340	11.46	46.50	0.247	171.20	104.01	1	(24+25)-VI-1	Parz.	Parz.
50.40	15.82	46.50	0.340	11.52	46.50	0.248	171.20	104.01	1	(22+23)-VI-1	Parz.	Parz.
CAMP	15.64	46.50	0.336	11.68	46.50	0.251	171.20	104.01	(22+23)-IV-3	20	Parz.	Parz.
453.56	15.84	46.50	0.341	11.57	46.50	0.249	171.20	104.01	5	20	Parz.	Parz.
FLN	15.84	46.50	0.341	11.54	46.50	0.248	171.20	104.01	5	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	119.60	--	442.88	175.61	175.61	65.53	104.01	75.00	10.72	1.5
Cen	102.18	--	442.88	105.56	105.56	--	--	--	6.45	1.0
Des	121.35	--	442.88	175.61	175.61	65.53	171.20	75.00	10.72	1.4

Trave: 212 [205,210], Pilastrate [5,10] Sez. R: By=30.00 cm Bz=50.00 cm L=378.19 cm Ln=379.38 cm
Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	∆M-	∆M+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	57.06	25.92	--	7.89	10.05	6.03	171.20	104.01	(22+23)-VI-4	(22+23)-VI-1	3.0
37.94	32.43	32.71	24.62	2.22	10.05	6.03	171.20	104.01	(22+23)-VI-4	(22+23)-VI-1	3.0
CAMP	45.63	61.67	42.95	--	10.05	6.03	171.20	104.01	(22+23)-VI-1	20	1.7
341.44	75.58	52.49	34.28	--	10.05	6.03	171.20	104.01	(22+23)-VI-1	6	1.6
FLN	109.87	49.70	--	--	10.05	6.03	171.20	104.01	(22+23)-VI-1	6	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.73	46.50	0.338	11.55	46.50	0.248	171.20	104.01	(22+23)-VI-4	(22+23)-VI-1	Parz.	Parz.
37.94	15.73	46.50	0.338	11.56	46.50	0.249	171.20	104.01	(22+23)-VI-4	(22+23)-VI-1	Parz.	Parz.
CAMP	15.91	46.50	0.342	11.65	46.50	0.251	171.20	104.01	(22+23)-VI-1	20	Parz.	Parz.
341.4	16.04	46.50	0.345	11.62	46.50	0.250	171.20	104.01	(22+23)-VI-	6	Parz.	Parz.

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
4									1			
FLN	16.04	46.50	0.345	11.61	46.50	0.250	171.20	104.01	(22+23)-VI-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	142.58	--	442.88	175.61	175.61	87.05	104.01	75.00	10.72	1.2
Cen	124.28	--	442.88	132.20	132.20	--	--	--	8.07	1.1
Des	145.86	--	442.88	175.61	175.61	87.05	171.20	75.00	10.72	1.2

Trave: 212 [210,218], Pilastrate [10,18] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	108.11	14.96	--	18.41	10.05	6.03	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	1.6
46.99	65.41	30.05	42.70	14.01	10.05	6.03	171.20	104.01	(22+23)-VI-2	(22+23)-VI-3	1.6
CAMP	29.90	94.92	40.35	--	10.05	6.03	171.20	104.01	(22+23)-VI-2	20	1.1
422.91	50.71	41.27	36.18	28.46	10.05	6.03	171.20	104.01	(22+23)-VI-3	20	1.5
FLN	86.90	42.74	--	8.47	10.05	6.03	171.20	104.01	(22+23)-VI-3	6	2.0

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	16.02	46.50	0.345	11.55	46.50	0.248	171.20	104.01	(22+23)-VI-2	(24+25)-VI-3	Parz.	Parz.
46.99	16.02	46.50	0.345	11.59	46.50	0.249	171.20	104.01	(22+23)-VI-2	(22+23)-VI-3	Parz.	Parz.
CAMP	15.80	46.50	0.340	11.79	46.50	0.253	171.20	104.01	(22+23)-VI-2	20	Parz.	Parz.
422.91	15.90	46.50	0.342	11.69	46.50	0.251	171.20	104.01	(22+23)-VI-3	20	Parz.	Parz.
FLN	15.90	46.50	0.342	11.62	46.50	0.250	171.20	104.01	(22+23)-VI-3	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	142.08	--	442.88	175.61	175.61	70.28	104.01	75.00	10.72	1.2
Cen	111.50	--	442.88	119.26	119.26	--	--	--	7.28	1.1
Des	129.02	--	442.88	175.61	175.61	70.28	171.20	75.00	10.72	1.4

Trave: 213 [206,211], Pilastrate [6,11] Sez. R: By=30.00 cm Bz=50.00 cm L=377.00 cm Ln=347.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	48.17	43.73	--	--	10.05	6.03	171.20	104.01	(22+23)-II-4	(24+25)-II-1	2.4
34.70	31.71	44.50	16.46	--	10.05	6.03	171.20	104.01	(22+23)-II-4	(22+23)-II-1	2.3
CAMP	32.19	47.25	35.97	--	10.05	6.03	171.20	104.01	(22+23)-II-1	20	2.2
312.30	55.15	45.40	25.64	--	10.05	6.03	171.20	104.01	(22+23)-II-1	6	2.1
FLN	80.78	44.66	--	--	10.05	6.03	171.20	104.01	(22+23)-II-1	6	2.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.68	46.50	0.337	11.59	46.50	0.249	171.20	104.01	(22+23)-II-4	(24+25)-II-1	Parz.	Parz.
34.70	15.68	46.50	0.337	11.59	46.50	0.249	171.20	104.01	(22+23)-II-4	(22+23)-II-1	Parz.	Parz.
CAMP	15.79	46.50	0.340	11.60	46.50	0.249	171.20	104.01	(22+23)-II-1	20	Parz.	Parz.
312.30	15.86	46.50	0.341	11.59	46.50	0.249	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.
FLN	15.86	46.50	0.341	11.59	46.50	0.249	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	137.65	--	442.88	175.61	175.61	95.17	104.01	75.00	10.72	1.3
Cen	112.54	--	442.88	118.30	118.30	--	--	--	7.22	1.1
Des	135.75	--	442.88	175.61	175.61	95.17	171.20	75.00	10.72	1.3

Trave: 213 [211,219], Pilastrate [11,19] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	78.43	6.91	--	16.21	10.05	6.03	171.20	104.01	(22+23)-II-4	6	2.2
46.99	43.48	6.59	34.96	36.32	10.05	6.03	171.20	104.01	(22+23)-II-4	20	2.2
CAMP	22.44	90.92	31.15	--	10.05	6.03	171.20	104.01	(22+23)-II-1	20	1.1
422.91	49.89	41.88	32.63	26.50	10.05	6.03	171.20	104.01	(22+23)-II-1	20	1.5
FLN	82.52	40.11	--	8.63	10.05	6.03	171.20	104.01	(22+23)-II-1	6	2.1

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.85	46.50	0.341	11.51	46.50	0.248	171.20	104.01	(22+23)-II-4	6	Parz.	Parz.
46.99	15.85	46.50	0.341	11.58	46.50	0.249	171.20	104.01	(22+23)-II-4	20	Parz.	Parz.
CAMP	15.71	46.50	0.338	11.77	46.50	0.253	171.20	104.01	(22+23)-II-1	20	Parz.	Parz.
422.91	15.87	46.50	0.341	11.68	46.50	0.251	171.20	104.01	(22+23)-II-1	20	Parz.	Parz.
FLN	15.87	46.50	0.341	11.61	46.50	0.250	171.20	104.01	(22+23)-II-1	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	128.79	--	442.88	175.61	175.61	70.28	104.01	75.00	10.72	1.4
Cen	105.50	--	442.88	109.75	109.75	--	--	--	6.70	1.0
Des	126.19	--	442.88	175.61	175.61	70.28	171.20	75.00	10.72	1.4

Trave: 214 [210,211], Pilastrate [10,11] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	41.10	35.79	--	--	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	2.9
42.70	26.42	31.85	14.69	3.94	10.05	6.03	171.20	104.01	(22+23)-III-3	(24+25)-III-2	2.9
CAMP	40.61	56.53	21.63	3.92	10.05	6.03	171.20	104.01	(22+23)-III-2	6	1.7
384.30	57.95	59.93	19.07	2.29	10.05	6.03	171.20	104.01	(22+23)-III-2	6	1.7
FLN	77.02	62.22	--	--	10.05	6.03	171.20	104.01	(22+23)-III-2	6	1.7

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.64	46.50	0.336	11.56	46.50	0.249	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
42.70	15.64	46.50	0.336	11.56	46.50	0.249	171.20	104.01	(22+23)-III-3	(24+25)-III-2	Parz.	Parz.
CAMP	15.76	46.50	0.339	11.65	46.50	0.251	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.
384.30	15.84	46.50	0.341	11.66	46.50	0.251	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.
FLN	15.84	46.50	0.341	11.66	46.50	0.251	171.20	104.01	(22+23)-III-2	6	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	96.48	--	442.88	175.61	175.61	77.34	104.01	75.00	10.72	1.8
Cen	89.57	--	442.88	93.31	93.31	--	--	--	5.70	1.0
Des	97.63	--	442.88	175.61	175.61	77.34	171.20	75.00	10.72	1.8

Trave: 8000 [37,38], Pilastrate [14,--] Sez. R: By=30.00 cm Bz=50.00 cm L=405.25 cm Ln=405.25 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	--	--	--	23.60	10.05	6.03	171.20	104.01	11	1	4.4
40.53	-16.26	19.02	16.26	19.34	10.05	6.03	171.20	104.01	11	1	2.7
CAMP	3.13	65.47	11.17	--	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	1.6
364.73	11.38	64.81	10.01	0.47	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	1.6
FLN	21.39	62.17	--	2.83	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	1.6

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	--	--	--	11.52	46.50	0.248	171.20	104.01	11	1	--	Parz.
40.53	--	--	--	11.57	46.50	0.249	171.20	104.01	11	1	--	Parz.
CAMP	15.51	46.50	0.334	11.67	46.50	0.251	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
364.73	15.54	46.50	0.334	11.67	46.50	0.251	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
FLN	15.54	46.50	0.334	11.67	46.50	0.251	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.

Verifica a taglio: cot(θ) Sin=1.000,cot(θ) Cen=1.000,cot(θ) Des=1.000 Comb: Sin=(22+23)-VIII-4 Cen=(22+23)-VIII-4 Des=(22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	105.76	--	442.88	175.61	175.61	81.49	104.01	75.00	10.72	1.7
Cen	96.05	--	442.88	96.84	96.84	--	--	--	5.91	1.0
Des	105.76	--	442.88	175.61	175.61	81.49	171.20	75.00	10.72	1.7

Trave: 8000 [38,35], Pilastrate [--,17] Sez. R: By=30.00 cm Bz=50.00 cm L=173.00 cm Ln=173.00 cm Criterio : Travi alte - Verifica a flessione : **Verificato**

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
cm	kN*m	kN*m	kN*m	kN*m	cmq	cmq	kN*m	kN*m			
ILN	21.34	64.49	--	--	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	1.6
17.30	17.59	59.86	3.75	4.63	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	1.6
CAMP	11.17	49.39	10.17	15.11	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	1.6

X	M-	M+	ΔM-	ΔM+	Afs	Afi	Mr-	Mr+	C-	C+	CS
155.70	0.52	8.27	3.76	22.54	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	3.4
FLN	--	--	2.67	23.76	10.05	6.03	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	4.4

X	x-	d-	x-/d-	x+	d+	x+/d+	Mr-	Mr+	C-	C+	Stato-	Stato +
cm	cm	cm		cm	cm		kN*m	kN*m				
ILN	15.54	46.50	0.334	11.67	46.50	0.251	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
17.30	15.54	46.50	0.334	11.67	46.50	0.251	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
CAMP	15.54	46.50	0.334	11.67	46.50	0.251	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
155.70	15.46	46.50	0.332	11.54	46.50	0.248	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.
FLN	15.45	46.50	0.332	11.52	46.50	0.248	171.20	104.01	(24+25)-VII-4	(22+23)-VII-1	Parz.	Parz.

Verifica a taglio: cot(θ) =1.000 Comb: (22+23)-VIII-4

Sez	Td	VRdns	VRcd	VRsd	VRd	Tpl	Mr	Dx	Staffe	CS
	kN	kN	kN	kN	kN	kN	kN*m	cm	cmq/m	
Sin	202.57	--	442.88	205.79	205.79	190.90	104.01	173.00	12.57	1.0
Des							171.20			

Verifiche stato limite di esercizio

Verifica delle travi (Stati limite esercizio)

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Simbologia

Terreno — Nome della stratigrafia per travi Winkler
L [cm] — Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] — Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] — Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
- By[cm]: Larghezza (asse locale y)
- Bz[cm]: Larghezza (asse locale z)

Sez. T: Sezione a T (rovescia e non)
- Ba[cm]: Larghezza base inferiore
- Ha[cm]: Altezza inferiore
- Bs[cm]: Larghezza superiore
- Hs[cm]: Altezza superiore

Sez. L: Sezione ad L (rovescia e non)
- Ba[cm]: Larghezza base inferiore
- Ha[cm]: Altezza inferiore
- Bs[cm]: Larghezza superiore
- Hs[cm]: Altezza superiore

Sez. C: Sezione circolare
- R[cm]: Raggio

Sez. G: Sezione generica
- B[cm]: Larghezza
- H[cm]: Altezza

X [cm] — Punto di verifica
σca [MPa] — Tensione ammissibile nel cls
σfa [MPa] — Tensione ammissibile nell'acciaio
σcta [MPa] — Tensione ammissibile a trazione (quando richiesto dalla verifica)
M- [kN*m] — Momento negativo massimo di calcolo
M+ [kN*m] — Momento positivo massimo di calcolo
M [kN*m] — Momento di calcolo (travi a flessione, pilastri circolari

My [kN*m]	Momento calcolo per verifiche a pressoflessione
Mz [kN*m]	Momento calcolo per verifiche a pressoflessione (Sez. L,Pilastri)
N [kN]	Sforzo normale corrispondente ad My (e Mz per Sez. L,Pilastri)
Afsup [cmq]	Area di ferro superiore
Afinf [cmq]	Area di ferro inferiore
Afsin [cmq]	Area di ferro sinistra (Sez. L)
Afdes [cmq]	Area di ferro destra (Sez. L)
σc- [MPa]	Tensione nel cls compresso per effetto di M-
σcy [MPa]	Tensione nel cls compresso per effetto di (N,My) in caso di pressoflessione retta
σcz [MPa]	Tensione nel cls compresso per effetto di (N,Mz) in caso di pressoflessione retta
σc+ [MPa]	Tensione nel cls compresso per effetto di M+
σct- [MPa]	Tensione nel cls teso per effetto di M-
σct+ [MPa]	Tensione nel cls teso per effetto di M+
σf- [MPa]	Tensione nell'acciaio per effetto di M-
σf+ [MPa]	Tensione nell'acciaio per effetto di M+
σfy [MPa]	Tensione nel acciaio per effetto di (N,My) in caso di pressoflessione retta
σfz [MPa]	Tensione nel acciaio per effetto di (N,Mz) in caso di pressoflessione retta
Cb-	Combinazione di carico generatore di M-
Cb+	Combinazione di carico generatore di M+
σc [MPa]	Tensione nel cls per effetto di N My
σf [MPa]	Tensione nell'acciaio per effetto di N My
Cb	Combinazione di carico generatore di N My
Act [m^2]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso
$S_{r,max}$ [cm]	Distanza massima delle fessure
σsfmed [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di σAmm/σ tra acciaio e calcestruzzo oppure Wamm/Wk

Trave: 101 [129,130], Pilastrate [29,30] Sez. R: By=30.00 cm Bz=50.00 cm L=534.50 cm Ln=534.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	53.74	10.05	6.03	--	--	-4.26	128.12	45	30	Si	2.8
53.45	--	22.20	10.05	6.03	--	--	-1.76	52.93	45	30	Si	6.8
267.25	57.91	--	10.05	6.03	-4.89	224.31	--	--	44	40	Si	1.6
481.05	28.72	25.08	10.05	6.03	-2.43	111.24	-1.99	59.79	45	30	Si	3.2
534.50	12.98	57.66	10.05	6.03	-1.10	50.27	-4.57	137.46	45	30	Si	2.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	47.11	10.05	6.03	--	--	-3.74	112.31	48	46	Si	3.0
53.45	--	19.34	10.05	6.03	--	--	-1.53	46.10	48	46	Si	7.3
267.25	29.71	--	10.05	6.03	-2.51	115.09	--	--	46	48	Si	3.1
481.05	--	22.42	10.05	6.03	--	--	-1.78	53.45	48	46	Si	6.3
534.50	--	51.26	10.05	6.03	--	--	-4.07	122.21	48	46	Si	2.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	44.90	10.05	6.03	--	--	-3.56	107.03	52	52	Si	3.1
53.45	--	18.38	10.05	6.03	--	--	-1.46	43.82	52	52	Si	7.7

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
267.25	28.40	--	10.05	6.03	-2.40	110.01	--	--	52	52	Si	3.3
481.05	--	21.54	10.05	6.03	--	--	-1.71	51.34	52	52	Si	6.6
534.50	--	49.13	10.05	6.03	--	--	-3.90	117.13	52	52	Si	2.9

Trave: 101 [130,131], Pilastrate [30,31] Sez. R: By=30.00 cm Bz=50.00 cm L=614.50 cm Ln=614.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	86.51	10.05	6.03	--	--	-6.86	206.24	45	26	Si	1.7
61.45	--	44.19	10.05	6.03	--	--	-3.50	105.34	45	30	Si	3.4
307.25	65.62	--	10.05	6.03	-5.54	254.16	--	--	44	40	Si	1.4
553.05	40.46	24.20	10.05	6.03	-3.42	156.71	-1.92	57.70	45	30	Si	2.3
614.50	23.30	62.18	10.05	6.03	-1.97	90.25	-4.93	148.24	45	30	Si	2.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	76.11	10.05	6.03	--	--	-6.04	181.44	48	46	Si	1.9
61.45	--	39.38	10.05	6.03	--	--	-3.12	93.88	48	46	Si	3.6
307.25	33.87	--	10.05	6.03	-2.86	131.20	--	--	46	48	Si	2.7
553.05	--	21.02	10.05	6.03	--	--	-1.67	50.12	48	46	Si	6.7
614.50	--	54.50	10.05	6.03	--	--	-4.32	129.92	48	46	Si	2.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	72.91	10.05	6.03	--	--	-5.78	173.82	52	52	Si	1.9
61.45	--	37.78	10.05	6.03	--	--	-3.00	90.06	52	52	Si	3.7
307.25	32.40	--	10.05	6.03	-2.74	125.50	--	--	52	52	Si	2.9
553.05	--	19.96	10.05	6.03	--	--	-1.58	47.59	52	52	Si	7.1
614.50	--	51.93	10.05	6.03	--	--	-4.12	123.81	52	52	Si	2.7

Trave: 102 [124,125], Pilastrate [24,25] Sez. R: By=30.00 cm Bz=50.00 cm L=544.50 cm Ln=544.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	39.42	10.05	6.03	--	--	-3.13	93.97	45	26	Si	3.8
54.45	1.66	4.04	10.05	6.03	-0.14	6.43	-0.32	9.64	45	30	Si	37
272.25	62.65	--	10.05	6.03	-5.29	242.66	--	--	44	40	Si	1.5
490.05	9.05	32.22	10.05	6.03	-0.76	35.06	-2.56	76.81	45	30	Si	4.7
544.50	--	74.26	10.05	6.03	--	--	-5.89	177.04	45	30	Si	2.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	33.50	10.05	6.03	--	--	-2.66	79.87	48	46	Si	4.2
54.45	--	3.40	10.05	6.03	--	--	-0.27	8.10	48	46	Si	42
272.25	43.88	--	10.05	6.03	-3.71	169.96	--	--	46	48	Si	2.1
490.05	--	29.24	10.05	6.03	--	--	-2.32	69.71	48	46	Si	4.8
544.50	--	66.33	10.05	6.03	--	--	-5.26	158.14	48	46	Si	2.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	31.84	10.05	6.03	--	--	-2.53	75.91	52	52	Si	4.4
54.45	--	3.18	10.05	6.03	--	--	-0.25	7.58	52	52	Si	44
272.25	41.72	--	10.05	6.03	-3.52	161.60	--	--	52	52	Si	2.2
490.05	--	28.25	10.05	6.03	--	--	-2.24	67.35	52	52	Si	5.0
544.50	--	63.69	10.05	6.03	--	--	-5.05	151.84	52	52	Si	2.2

Trave: 102 [125,126], Pilastrate [25,26] Sez. R: By=30.00 cm Bz=50.00 cm L=604.50 cm Ln=604.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	114.61	20.11	8.04	--	--	-7.06	140.32	45	30	Si	2.1
60.45	--	60.90	20.11	8.04	--	--	-3.75	74.56	45	30	Si	4.0
302.25	75.08	--	10.05	8.04	-5.76	219.96	--	--	44	40	Si	1.6
544.05	21.16	11.53	10.05	8.04	-1.62	61.99	-0.87	27.35	45	30	Si	5.8
604.50	--	51.10	10.05	8.04	--	--	-3.84	121.20	45	30	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	104.75	20.11	8.04	--	--	-6.45	128.25	48	46	Si	1.7
60.45	--	55.40	20.11	8.04	--	--	-3.41	67.83	48	46	Si	3.3
302.25	44.84	--	10.05	8.04	-3.44	131.37	--	--	46	48	Si	2.7
544.05	--	10.50	10.05	8.04	--	--	-0.79	24.90	48	46	Si	14
604.50	--	47.06	10.05	8.04	--	--	-3.54	111.60	48	46	Si	3.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	101.47	20.11	8.04	--	--	-6.25	124.23	52	52	Si	1.8
60.45	--	53.56	20.11	8.04	--	--	-3.30	65.58	52	52	Si	3.4
302.25	43.71	--	10.05	8.04	-3.35	128.06	--	--	52	52	Si	2.8
544.05	--	10.15	10.05	8.04	--	--	-0.76	24.08	52	52	Si	15
604.50	--	45.71	10.05	8.04	--	--	-3.44	108.40	52	52	Si	3.3

Trave: 103 [121,122], Pilastrate [21,22] Sez. R: By=30.00 cm Bz=50.00 cm L=574.50 cm Ln=574.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	52.46	10.05	8.04	--	--	-3.94	124.41	45	26	Si	2.9
57.45	--	9.52	10.05	8.04	--	--	-0.72	22.57	45	30	Si	16
287.25	76.97	--	10.05	8.04	-5.90	225.49	--	--	26	40	Si	1.6
517.05	16.76	13.38	10.05	8.04	-1.29	49.09	-1.01	31.74	45	30	Si	7.3
574.50	--	57.29	10.05	8.04	--	--	-4.31	135.86	45	30	Si	2.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	46.18	10.05	8.04	--	--	-3.47	109.53	48	46	Si	3.2
57.45	--	8.47	10.05	8.04	--	--	-0.64	20.09	48	46	Si	18
287.25	58.66	--	10.05	8.04	-4.50	171.86	--	--	46	48	Si	2.1
517.05	--	11.62	10.05	8.04	--	--	-0.87	27.56	48	46	Si	13
574.50	--	50.14	10.05	8.04	--	--	-3.77	118.91	48	46	Si	3.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	44.10	10.05	8.04	--	--	-3.31	104.59	52	52	Si	3.4
57.45	--	8.12	10.05	8.04	--	--	-0.61	19.26	52	52	Si	18
287.25	55.97	--	10.05	8.04	-4.29	163.97	--	--	52	52	Si	2.2
517.05	--	11.03	10.05	8.04	--	--	-0.83	26.17	52	52	Si	14
574.50	--	47.76	10.05	8.04	--	--	-3.59	113.26	52	52	Si	3.1

Trave: 104 [115,113], Pilastrate [15,13] Sez. R: By=30.00 cm Bz=50.00 cm L=531.07 cm Ln=577.87 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	36.69	10.05	6.03	--	--	-2.91	87.47	40	26	Si	4.1
57.79	--	4.88	10.05	6.03	--	--	-0.39	11.63	45	30	Si	31
288.93	58.99	--	10.05	6.03	-4.98	228.49	--	--	44	40	Si	1.6
520.08	22.60	18.52	10.05	6.03	-1.91	87.52	-1.47	44.14	45	30	Si	4.1
577.87	6.79	50.29	10.05	6.03	-0.57	26.28	-3.99	119.90	45	30	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	31.70	10.05	6.03	--	--	-2.51	75.56	48	46	Si	4.5
57.79	--	4.44	10.05	6.03	--	--	-0.35	10.59	48	46	Si	32
288.93	39.57	--	10.05	6.03	-3.34	153.26	--	--	46	48	Si	2.3
520.08	--	16.25	10.05	6.03	--	--	-1.29	38.73	48	46	Si	8.7
577.87	--	44.37	10.05	6.03	--	--	-3.52	105.77	48	46	Si	3.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	30.38	10.05	6.03	--	--	-2.41	72.42	52	52	Si	4.7
57.79	--	4.30	10.05	6.03	--	--	-0.34	10.25	52	52	Si	33
288.93	37.87	--	10.05	6.03	-3.20	146.70	--	--	52	52	Si	2.5
520.08	--	15.49	10.05	6.03	--	--	-1.23	36.93	52	52	Si	9.1
577.87	--	42.39	10.05	6.03	--	--	-3.36	101.06	52	52	Si	3.3

Trave: 105 [102,108], Pilastrate [2,8] Sez. R: By=30.00 cm Bz=50.00 cm L=368.36 cm Ln=252.48 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	6.11	12.63	10.05	8.04	-0.47	17.90	-0.95	29.95	30	45	Si	12
25.25	7.29	5.49	10.05	8.04	-0.56	21.35	-0.41	13.03	30	45	Si	17
126.24	19.42	--	10.05	8.04	-1.49	56.89	--	--	44	40	Si	6.3
227.23	31.72	13.76	10.05	8.04	-2.43	92.92	-1.03	32.64	45	30	Si	3.9
252.48	33.24	21.38	10.05	8.04	-2.55	97.37	-1.61	50.70	45	30	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	5.58	--	10.05	8.04	-0.43	16.35	--	--	46	48	Si	22
25.25	6.61	--	10.05	8.04	-0.51	19.38	--	--	46	48	Si	19
126.24	4.07	--	10.05	8.04	-0.31	11.92	--	--	46	48	Si	30
227.23	--	12.41	10.05	8.04	--	--	-0.93	29.44	48	46	Si	12
252.48	--	19.22	10.05	8.04	--	--	-1.44	45.58	48	46	Si	7.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	5.40	--	10.05	8.04	-0.41	15.83	--	--	52	52	Si	23
25.25	6.39	--	10.05	8.04	-0.49	18.72	--	--	52	52	Si	19
126.24	3.90	--	10.05	8.04	-0.30	11.42	--	--	52	52	Si	32
227.23	--	11.96	10.05	8.04	--	--	-0.90	28.36	52	52	Si	12
252.48	--	18.50	10.05	8.04	--	--	-1.39	43.87	52	52	Si	8.1

Trave: 105 [108,113], Pilastrate [8,13] Sez. R: By=30.00 cm Bz=50.00 cm L=327.82 cm Ln=327.82 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	40.26	10.05	8.04	--	--	-3.03	95.49	45	30	Si	3.8

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
32.78	9.24	24.25	10.05	8.04	-0.71	27.07	-1.82	57.50	45	30	Si	6.3
163.91	42.36	--	10.05	8.04	-3.25	124.10	--	--	44	40	Si	2.9
295.03	44.04	--	10.05	8.04	-3.38	129.03	--	--	44	40	Si	2.8
327.82	38.25	--	10.05	8.04	-2.93	112.05	--	--	44	40	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	35.95	10.05	8.04	--	--	-2.70	85.27	48	46	Si	4.1
32.78	--	21.76	10.05	8.04	--	--	-1.64	51.60	48	46	Si	6.9
163.91	14.14	--	10.05	8.04	-1.08	41.42	--	--	46	48	Si	8.7
295.03	13.30	--	10.05	8.04	-1.02	38.97	--	--	46	48	Si	9.2
327.82	7.04	--	10.05	8.04	-0.54	20.62	--	--	46	48	Si	17

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	34.52	10.05	8.04	--	--	-2.59	81.87	52	52	Si	4.3
32.78	--	20.93	10.05	8.04	--	--	-1.57	49.63	52	52	Si	7.1
163.91	13.48	--	10.05	8.04	-1.03	39.49	--	--	52	52	Si	9.1
295.03	12.80	--	10.05	8.04	-0.98	37.49	--	--	52	52	Si	9.6
327.82	6.84	--	10.05	8.04	-0.52	20.04	--	--	52	52	Si	18

Trave: 105 [113,116], Pilastrate [13,16] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	44.15	10.05	8.04	--	--	-3.32	104.72	45	30	Si	3.4
32.99	1.13	31.25	10.05	8.04	-0.09	3.32	-2.35	74.11	45	30	Si	4.9
164.93	35.72	--	10.05	8.04	-2.74	104.65	--	--	44	40	Si	3.4
296.88	47.23	--	10.05	8.04	-3.62	138.37	--	--	44	40	Si	2.6
329.87	45.03	--	10.05	8.04	-3.45	131.91	--	--	44	40	Si	2.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	40.00	10.05	8.04	--	--	-3.01	94.87	48	46	Si	3.7
32.99	--	28.29	10.05	8.04	--	--	-2.13	67.09	48	46	Si	5.3
164.93	5.00	--	10.05	8.04	-0.38	14.64	--	--	46	47	Si	25
296.88	7.98	--	10.05	8.04	-0.61	23.37	--	--	46	48	Si	15
329.87	3.64	--	10.05	8.04	-0.28	10.66	--	--	46	48	Si	34

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	38.62	10.05	8.04	--	--	-2.90	91.59	52	52	Si	3.9
32.99	--	27.30	10.05	8.04	--	--	-2.05	64.75	52	52	Si	5.5
164.93	4.85	--	10.05	8.04	-0.37	14.20	--	--	52	52	Si	25
296.88	7.67	--	10.05	8.04	-0.59	22.47	--	--	52	52	Si	16
329.87	3.46	--	10.05	8.04	-0.27	10.13	--	--	52	52	Si	36

Trave: 105 [116,123], Pilastrate [16,23] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	61.11	10.05	8.04	--	--	-4.59	144.93	45	30	Si	2.5
53.25	--	30.55	10.05	8.04	--	--	-2.30	72.44	45	30	Si	5.0
266.26	57.76	--	10.05	8.04	-4.43	169.22	--	--	44	40	Si	2.1
479.27	25.76	12.95	10.05	8.04	-1.98	75.45	-0.97	30.73	45	30	Si	4.8

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
532.52	4.53	41.55	10.05	8.04	-0.35	13.28	-3.12	98.55	45	30	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	58.06	10.05	8.04	--	--	-4.36	137.71	47	46	Si	2.6
53.25	--	29.03	10.05	8.04	--	--	-2.18	68.86	47	46	Si	5.1
266.26	29.65	--	10.05	8.04	-2.27	86.87	--	--	46	47	Si	4.1
479.27	--	11.99	10.05	8.04	--	--	-0.90	28.43	48	46	Si	12
532.52	--	38.92	10.05	8.04	--	--	-2.93	92.31	48	46	Si	3.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	57.05	10.05	8.04	--	--	-4.29	135.30	52	52	Si	2.6
53.25	--	28.53	10.05	8.04	--	--	-2.14	67.66	52	52	Si	5.2
266.26	29.11	--	10.05	8.04	-2.23	85.27	--	--	52	52	Si	4.2
479.27	--	11.66	10.05	8.04	--	--	-0.88	27.66	52	52	Si	13
532.52	--	38.05	10.05	8.04	--	--	-2.86	90.23	52	52	Si	3.9

Trave: 106 [103,109], Pilastrate [3,9] Sez. R: By=30.00 cm Bz=50.00 cm L=327.85 cm Ln=327.85 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	40.42	10.05	6.03	--	--	-3.21	96.36	40	44	Si	3.7
32.79	--	24.64	10.05	6.03	--	--	-1.95	58.73	40	26	Si	6.1
163.93	26.15	--	10.05	6.03	-2.21	101.30	--	--	44	40	Si	3.6
295.07	47.91	--	10.05	6.03	-4.05	185.59	--	--	44	40	Si	1.9
327.85	48.03	--	10.05	6.03	-4.06	186.03	--	--	44	40	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	30.29	10.05	6.03	--	--	-2.40	72.20	48	46	Si	4.7
32.79	--	19.41	10.05	6.03	--	--	-1.54	46.28	48	46	Si	7.3
163.93	10.53	--	10.05	6.03	-0.89	40.78	--	--	46	48	Si	8.8
295.07	12.47	--	10.05	6.03	-1.05	48.31	--	--	46	48	Si	7.5
327.85	7.77	--	10.05	6.03	-0.66	30.09	--	--	46	47	Si	12

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	29.14	10.05	6.03	--	--	-2.31	69.47	52	52	Si	4.8
32.79	--	18.70	10.05	6.03	--	--	-1.48	44.58	52	52	Si	7.6
163.93	10.08	--	10.05	6.03	-0.85	39.06	--	--	52	52	Si	9.2
295.07	12.06	--	10.05	6.03	-1.02	46.72	--	--	52	52	Si	7.7
327.85	7.60	--	10.05	6.03	-0.64	29.43	--	--	52	52	Si	12

Trave: 106 [109,114], Pilastrate [9,14] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	42.99	10.05	6.03	--	--	-3.41	102.49	45	30	Si	3.5
32.99	9.07	28.31	10.05	6.03	-0.77	35.14	-2.24	67.48	45	30	Si	5.3
164.93	37.64	--	10.05	6.03	-3.18	145.81	--	--	44	40	Si	2.5
296.88	42.41	--	10.05	6.03	-3.58	164.27	--	--	44	40	Si	2.2
329.87	39.60	--	10.05	6.03	-3.34	153.38	--	--	44	40	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	38.52	10.05	6.03	--	--	-3.06	91.84	48	46	Si	3.7
32.99	--	25.40	10.05	6.03	--	--	-2.01	60.56	48	46	Si	5.6
164.93	7.33	--	10.05	6.03	-0.62	28.38	--	--	46	48	Si	13
296.88	9.51	--	10.05	6.03	-0.80	36.83	--	--	46	48	Si	9.8
329.87	6.08	--	10.05	6.03	-0.51	23.53	--	--	46	48	Si	15

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	37.03	10.05	6.03	--	--	-2.94	88.29	52	52	Si	3.8
32.99	--	24.43	10.05	6.03	--	--	-1.94	58.25	52	52	Si	5.8
164.93	7.03	--	10.05	6.03	-0.59	27.21	--	--	52	52	Si	13
296.88	9.07	--	10.05	6.03	-0.77	35.14	--	--	52	52	Si	10
329.87	5.74	--	10.05	6.03	-0.48	22.24	--	--	52	52	Si	16

Trave: 106 [114,117], Pilastrate [14,17] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	71.47	10.05	6.03	--	--	-5.67	170.38	45	30	Si	2.1
53.25	--	35.89	10.05	6.03	--	--	-2.85	85.57	45	30	Si	4.2
266.26	60.14	--	10.05	6.03	-5.08	232.96	--	--	44	40	Si	1.5
479.27	26.71	5.80	10.05	6.03	-2.26	103.45	-0.46	13.83	45	30	Si	3.5
532.52	6.52	31.79	10.05	6.03	-0.55	25.25	-2.52	75.80	45	30	Si	4.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	67.44	10.05	6.03	--	--	-5.35	160.77	47	46	Si	2.1
53.25	--	33.91	10.05	6.03	--	--	-2.69	80.84	47	46	Si	4.2
266.26	33.21	--	10.05	6.03	-2.81	128.65	--	--	46	47	Si	2.8
479.27	--	5.46	10.05	6.03	--	--	-0.43	13.02	48	46	Si	26
532.52	--	30.04	10.05	6.03	--	--	-2.38	71.62	48	46	Si	4.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	66.10	10.05	6.03	--	--	-5.24	157.57	52	52	Si	2.1
53.25	--	33.25	10.05	6.03	--	--	-2.64	79.26	52	52	Si	4.2
266.26	32.54	--	10.05	6.03	-2.75	126.02	--	--	52	52	Si	2.9
479.27	--	5.35	10.05	6.03	--	--	-0.42	12.75	52	52	Si	26
532.52	--	29.46	10.05	6.03	--	--	-2.34	70.23	52	52	Si	4.8

Trave: 107 [102,103], Pilastrate [2,3] Sez. R: By=30.00 cm Bz=50.00 cm L=514.30 cm Ln=514.30 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	37.43	10.05	6.03	--	--	-2.97	89.24	45	30	Si	4.0
51.43	0.60	20.69	10.05	6.03	-0.05	2.33	-1.64	49.32	45	30	Si	7.3
257.15	42.37	--	10.05	6.03	-3.58	164.12	--	--	44	40	Si	2.2
462.87	36.55	7.77	10.05	6.03	-3.09	141.58	-0.62	18.51	45	30	Si	2.5
514.30	29.26	24.29	10.05	6.03	-2.47	113.33	-1.93	57.91	45	30	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	33.73	10.05	6.03	--	--	-2.67	80.41	48	46	Si	4.2

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
51.43	--	18.62	10.05	6.03	--	--	-1.48	44.38	48	46	Si	7.6
257.15	14.07	--	10.05	6.03	-1.19	54.51	--	--	46	48	Si	6.6
462.87	--	6.94	10.05	6.03	--	--	-0.55	16.53	48	46	Si	20
514.30	--	21.71	10.05	6.03	--	--	-1.72	51.76	48	46	Si	6.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	32.49	10.05	6.03	--	--	-2.58	77.47	52	52	Si	4.3
51.43	--	17.93	10.05	6.03	--	--	-1.42	42.74	52	52	Si	7.9
257.15	13.54	--	10.05	6.03	-1.14	52.45	--	--	52	52	Si	6.9
462.87	--	6.66	10.05	6.03	--	--	-0.53	15.88	52	52	Si	21
514.30	--	20.85	10.05	6.03	--	--	-1.65	49.71	52	52	Si	6.8

Trave: 107 [103,104], Pilastrate [3,4] Sez. R: By=30.00 cm Bz=50.00 cm L=463.50 cm Ln=463.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	60.25	10.05	6.03	--	--	-4.78	143.64	45	30	Si	2.5
46.35	--	38.30	10.05	6.03	--	--	-3.04	91.30	45	30	Si	3.9
231.75	41.78	--	10.05	6.03	-3.53	161.82	--	--	44	40	Si	2.2
417.15	50.33	--	10.05	6.03	-4.25	194.94	--	--	44	40	Si	1.8
463.50	45.00	--	10.05	12.06	-3.04	89.16	--	--	45	35	Si	4.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	54.46	10.05	6.03	--	--	-4.32	129.84	48	46	Si	2.6
46.35	--	34.73	10.05	6.03	--	--	-2.75	82.79	48	46	Si	4.1
231.75	14.22	--	10.05	6.03	-1.20	55.06	--	--	46	48	Si	6.5
417.15	11.10	--	10.05	6.03	-0.94	43.00	--	--	46	48	Si	8.4
463.50	1.80	--	10.05	12.06	-0.12	3.58	--	--	48	46	Si	92

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	52.53	10.05	6.03	--	--	-4.17	125.24	52	52	Si	2.7
46.35	--	33.54	10.05	6.03	--	--	-2.66	79.96	52	52	Si	4.2
231.75	13.63	--	10.05	6.03	-1.15	52.81	--	--	52	52	Si	6.8
417.15	10.84	--	10.05	6.03	-0.92	41.97	--	--	52	52	Si	8.6
463.50	1.80	--	10.05	12.06	-0.12	3.58	--	--	52	52	Si	92

Trave: 107 [104,105], Pilastrate [4,5] Sez. R: By=30.00 cm Bz=50.00 cm L=590.40 cm Ln=590.40 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	79.11	10.05	6.03	--	--	-6.27	188.59	45	30	Si	1.9
59.04	--	39.74	10.05	6.03	--	--	-3.15	94.74	45	30	Si	3.8
295.20	63.53	--	10.05	6.03	-5.37	246.08	--	--	44	40	Si	1.5
531.36	13.00	27.13	10.05	6.03	-1.10	50.37	-2.15	64.68	45	30	Si	5.6
590.40	--	65.06	10.05	6.03	--	--	-5.16	155.10	45	30	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	73.69	10.05	6.03	--	--	-5.84	175.67	48	46	Si	1.9
59.04	--	36.90	10.05	6.03	--	--	-2.93	87.97	48	46	Si	3.8
295.20	33.76	--	10.05	6.03	-2.85	130.78	--	--	46	48	Si	2.8
531.36	--	25.52	10.05	6.03	--	--	-2.02	60.83	48	46	Si	5.5

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
590.40	--	60.99	10.05	6.03	--	--	-4.84	145.41	48	46	Si	2.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	71.88	10.05	6.03	--	--	-5.70	171.36	52	52	Si	2.0
59.04	--	35.95	10.05	6.03	--	--	-2.85	85.71	52	52	Si	3.9
295.20	32.99	--	10.05	6.03	-2.79	127.80	--	--	52	52	Si	2.8
531.36	--	24.98	10.05	6.03	--	--	-1.98	59.55	52	52	Si	5.7
590.40	--	59.64	10.05	6.03	--	--	-4.73	142.18	52	52	Si	2.4

Trave: 107 [105,106], Pilastrate [5,6] Sez. R: By=30.00 cm Bz=50.00 cm L=397.00 cm Ln=397.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	8.60	12.38	10.05	12.06	-0.58	17.05	-0.84	29.12	45	35	Si	12
39.70	21.94	1.53	10.05	12.06	-1.48	43.48	-0.10	3.59	44	40	Si	8.3
198.50	44.16	--	10.05	6.03	-3.73	171.04	--	--	44	40	Si	2.1
357.30	19.33	22.35	10.05	6.03	-1.63	74.88	-1.77	53.28	45	30	Si	4.8
397.00	6.89	40.46	10.05	6.03	-0.58	26.67	-3.21	96.45	45	30	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	12.16	10.05	12.06	--	--	-0.83	28.62	48	47	Si	13
39.70	--	0.46	10.05	12.06	--	--	-0.03	1.09	46	47	Si	>100
198.50	15.18	--	10.05	6.03	-1.28	58.80	--	--	46	48	Si	6.1
357.30	--	20.49	10.05	6.03	--	--	-1.62	48.84	48	46	Si	6.9
397.00	--	37.39	10.05	6.03	--	--	-2.97	89.14	48	46	Si	3.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	12.12	10.05	12.06	--	--	-0.83	28.51	52	52	Si	13
39.70	--	0.46	10.05	12.06	--	--	-0.03	1.09	52	52	Si	>100
198.50	14.87	--	10.05	6.03	-1.26	57.59	--	--	52	52	Si	6.3
357.30	--	19.86	10.05	6.03	--	--	-1.58	47.35	52	52	Si	7.1
397.00	--	36.37	10.05	6.03	--	--	-2.88	86.70	52	52	Si	3.9

Trave: 107 [106,107], Pilastrate [6,7] Sez. R: By=30.00 cm Bz=50.00 cm L=530.00 cm Ln=530.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	22.23	10.05	6.03	--	--	-1.76	53.01	45	30	Si	6.8
53.00	8.48	7.14	10.05	6.03	-0.72	32.85	-0.57	17.02	45	30	Si	11
265.00	46.68	--	10.05	6.03	-3.94	180.82	--	--	44	40	Si	2.0
477.00	35.51	25.92	10.05	6.03	-3.00	137.56	-2.06	61.79	45	30	Si	2.6
530.00	27.23	45.71	10.05	6.03	-2.30	105.49	-3.63	108.97	45	30	Si	3.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.06	10.05	6.03	--	--	-1.59	47.81	48	46	Si	7.0
53.00	--	6.47	10.05	6.03	--	--	-0.51	15.42	48	46	Si	22
265.00	13.09	--	10.05	6.03	-1.11	50.69	--	--	46	48	Si	7.1
477.00	--	23.43	10.05	6.03	--	--	-1.86	55.87	48	46	Si	6.0
530.00	--	41.26	10.05	6.03	--	--	-3.27	98.37	48	46	Si	3.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.33	10.05	6.03	--	--	-1.53	46.08	52	52	Si	7.3
53.00	--	6.24	10.05	6.03	--	--	-0.50	14.89	52	52	Si	23
265.00	12.58	--	10.05	6.03	-1.06	48.73	--	--	52	52	Si	7.4
477.00	--	22.61	10.05	6.03	--	--	-1.79	53.89	52	52	Si	6.2
530.00	--	39.78	10.05	6.03	--	--	-3.15	94.84	52	52	Si	3.6

Trave: 108 [107,112], Pilastrate [7,12] Sez. R: By=30.00 cm Bz=50.00 cm L=377.00 cm Ln=377.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	12.09	10.05	6.03	--	--	-0.96	28.83	40	26	Si	12
37.70	6.22	--	10.05	6.03	-0.52	24.08	--	--	45	35	Si	15
188.50	39.78	--	10.05	6.03	-3.36	154.09	--	--	44	40	Si	2.3
339.30	21.70	26.11	10.05	6.03	-1.83	84.03	-2.07	62.25	45	30	Si	4.3
377.00	13.02	47.49	10.05	6.03	-1.10	50.43	-3.77	113.22	45	30	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	8.69	10.05	6.03	--	--	-0.69	20.72	48	46	Si	16
37.70	3.50	--	10.05	6.03	-0.30	13.56	--	--	48	47	Si	27
188.50	18.28	--	10.05	6.03	-1.54	70.80	--	--	46	48	Si	5.1
339.30	--	23.57	10.05	6.03	--	--	-1.87	56.19	48	46	Si	6.0
377.00	--	42.52	10.05	6.03	--	--	-3.37	101.36	48	46	Si	3.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	8.08	10.05	6.03	--	--	-0.64	19.25	52	52	Si	17
37.70	3.50	--	10.05	6.03	-0.30	13.56	--	--	52	52	Si	27
188.50	17.43	--	10.05	6.03	-1.47	67.53	--	--	52	52	Si	5.3
339.30	--	22.72	10.05	6.03	--	--	-1.80	54.17	52	52	Si	6.2
377.00	--	40.86	10.05	6.03	--	--	-3.24	97.40	52	52	Si	3.5

Trave: 108 [112,120], Pilastrate [12,20] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	44.80	10.05	6.03	--	--	-3.55	106.81	45	30	Si	3.4
46.99	8.62	18.64	10.05	6.03	-0.73	33.38	-1.48	44.44	45	30	Si	8.1
234.95	50.46	--	10.05	6.03	-4.26	195.43	--	--	44	40	Si	1.8
422.91	17.37	33.99	10.05	6.03	-1.47	67.29	-2.70	81.02	45	30	Si	4.4
469.90	2.67	62.47	10.05	6.03	-0.23	10.35	-4.95	148.93	45	30	Si	2.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	39.47	10.05	6.03	--	--	-3.13	94.08	48	46	Si	3.6
46.99	--	16.43	10.05	6.03	--	--	-1.30	39.18	48	46	Si	8.6
234.95	20.70	--	10.05	6.03	-1.75	80.16	--	--	46	48	Si	4.5
422.91	--	30.12	10.05	6.03	--	--	-2.39	71.80	48	46	Si	4.7
469.90	--	55.16	10.05	6.03	--	--	-4.37	131.50	48	46	Si	2.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	37.69	10.05	6.03	--	--	-2.99	89.84	52	52	Si	3.7

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
46.99	--	15.70	10.05	6.03	--	--	-1.24	37.42	52	52	Si	9.0
234.95	19.73	--	10.05	6.03	-1.67	76.42	--	--	52	52	Si	4.7
422.91	--	28.83	10.05	6.03	--	--	-2.29	68.72	52	52	Si	4.9
469.90	--	52.73	10.05	6.03	--	--	-4.18	125.70	52	52	Si	2.7

Trave: 108 [120,128], Pilastrate [20,28] Sez. R: By=30.00 cm Bz=50.00 cm L=413.00 cm Ln=413.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	39.12	10.05	6.03	--	--	-3.10	93.26	45	30	Si	3.9
41.30	--	16.33	10.05	6.03	--	--	-1.29	38.92	45	30	Si	9.2
206.50	50.82	--	10.05	6.03	-4.29	196.85	--	--	44	40	Si	1.8
371.70	39.39	1.01	10.05	6.03	-3.33	152.57	-0.08	2.41	45	30	Si	2.4
413.00	31.96	19.60	10.05	6.03	-2.70	123.79	-1.55	46.74	45	30	Si	2.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	35.07	10.05	6.03	--	--	-2.78	83.61	48	46	Si	4.0
41.30	--	14.87	10.05	6.03	--	--	-1.18	35.45	48	46	Si	9.5
206.50	25.02	--	10.05	6.03	-2.11	96.91	--	--	46	48	Si	3.7
371.70	--	0.54	10.05	6.03	--	--	-0.04	1.29	48	46	Si	>100
413.00	--	16.82	10.05	6.03	--	--	-1.33	40.09	48	46	Si	8.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	33.72	10.05	6.03	--	--	-2.67	80.39	52	52	Si	4.2
41.30	--	14.39	10.05	6.03	--	--	-1.14	34.30	52	52	Si	9.8
206.50	23.88	--	10.05	6.03	-2.02	92.49	--	--	52	52	Si	3.9
371.70	--	0.39	10.05	6.03	--	--	-0.03	0.92	52	52	Si	>100
413.00	--	15.89	10.05	6.03	--	--	-1.26	37.88	52	52	Si	8.9

Trave: 109 [106,111], Pilastrate [6,11] Sez. R: By=30.00 cm Bz=50.00 cm L=377.00 cm Ln=377.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	7.98	23.60	10.05	6.03	-0.67	30.92	-1.87	56.26	45	30	Si	6.4
37.70	22.94	1.92	10.05	6.03	-1.94	88.84	-0.15	4.59	45	30	Si	4.1
188.50	48.33	--	10.05	6.03	-4.08	187.21	--	--	44	40	Si	1.9
339.30	--	44.03	10.05	6.03	--	--	-3.49	104.96	45	30	Si	3.4
377.00	--	76.23	10.05	6.03	--	--	-6.05	181.73	45	30	Si	2.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.79	10.05	6.03	--	--	-1.65	49.56	48	46	Si	6.8
37.70	--	1.25	10.05	6.03	--	--	-0.10	2.99	48	46	Si	>100
188.50	23.73	--	10.05	6.03	-2.00	91.90	--	--	46	48	Si	3.9
339.30	--	40.70	10.05	6.03	--	--	-3.23	97.02	48	46	Si	3.5
377.00	--	70.09	10.05	6.03	--	--	-5.56	167.10	48	46	Si	2.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.85	10.05	6.03	--	--	-1.57	47.32	52	52	Si	7.1
37.70	--	1.03	10.05	6.03	--	--	-0.08	2.45	52	52	Si	>100
188.50	22.90	--	10.05	6.03	-1.93	88.70	--	--	52	52	Si	4.1
339.30	--	39.59	10.05	6.03	--	--	-3.14	94.38	52	52	Si	3.6

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
377.00	--	68.05	10.05	6.03	--	--	-5.40	162.23	52	52	Si	2.1

Trave: 109 [111,119], Pilastrate [11,19] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	62.63	10.05	6.03	--	--	-4.97	149.30	45	30	Si	2.4
46.99	6.19	21.94	10.05	6.03	-0.52	23.96	-1.74	52.30	45	30	Si	6.9
234.95	68.68	--	10.05	6.03	-5.80	266.03	--	--	44	40	Si	1.4
422.91	5.01	40.16	10.05	6.03	-0.42	19.40	-3.18	95.73	45	30	Si	3.8
469.90	--	83.56	10.05	6.03	--	--	-6.63	199.20	45	30	Si	1.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	57.48	10.05	6.03	--	--	-4.56	137.04	48	46	Si	2.5
46.99	--	20.37	10.05	6.03	--	--	-1.62	48.57	48	46	Si	6.9
234.95	41.27	--	10.05	6.03	-3.49	159.86	--	--	46	48	Si	2.3
422.91	--	35.93	10.05	6.03	--	--	-2.85	85.65	48	46	Si	3.9
469.90	--	75.21	10.05	6.03	--	--	-5.96	179.29	48	46	Si	1.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	55.77	10.05	6.03	--	--	-4.42	132.95	52	52	Si	2.5
46.99	--	19.85	10.05	6.03	--	--	-1.57	47.32	52	52	Si	7.1
234.95	39.92	--	10.05	6.03	-3.37	154.62	--	--	52	52	Si	2.3
422.91	--	34.51	10.05	6.03	--	--	-2.74	82.28	52	52	Si	4.1
469.90	--	72.42	10.05	6.03	--	--	-5.74	172.66	52	52	Si	2.0

Trave: 110 [119,127], Pilastrate [19,27] Sez. R: By=30.00 cm Bz=50.00 cm L=414.09 cm Ln=410.83 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	41.19	10.05	6.03	--	--	-3.27	98.19	45	30	Si	3.7
41.08	3.13	18.95	10.05	6.03	-0.26	12.14	-1.50	45.18	45	30	Si	8.0
205.41	50.10	--	10.05	6.03	-4.23	194.06	--	--	44	40	Si	1.9
369.74	36.77	6.32	10.05	6.03	-3.11	142.42	-0.50	15.07	45	30	Si	2.5
410.83	28.72	25.07	10.05	6.03	-2.43	111.24	-1.99	59.76	45	30	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	37.01	10.05	6.03	--	--	-2.94	88.23	48	46	Si	3.8
41.08	--	17.31	10.05	6.03	--	--	-1.37	41.27	48	46	Si	8.2
205.41	21.00	--	10.05	6.03	-1.77	81.35	--	--	46	48	Si	4.4
369.74	--	5.45	10.05	6.03	--	--	-0.43	13.00	48	46	Si	26
410.83	--	21.87	10.05	6.03	--	--	-1.73	52.15	48	46	Si	6.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	35.62	10.05	6.03	--	--	-2.82	84.91	52	52	Si	4.0
41.08	--	16.77	10.05	6.03	--	--	-1.33	39.97	52	52	Si	8.4
205.41	19.97	--	10.05	6.03	-1.69	77.36	--	--	52	52	Si	4.7
369.74	--	5.16	10.05	6.03	--	--	-0.41	12.31	52	52	Si	27
410.83	--	20.81	10.05	6.03	--	--	-1.65	49.61	52	52	Si	6.8

Trave: 111 [102,115], Pilastrate [2,15] Sez. R: By=30.00 cm Bz=50.00 cm L=481.60 cm Ln=481.60 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	27.54	10.05	6.03	--	--	-2.18	65.65	45	30	Si	5.5
48.16	6.50	9.29	10.05	6.03	-0.55	25.16	-0.74	22.16	45	30	Si	14
240.80	46.51	--	10.05	6.03	-3.93	180.16	--	--	44	40	Si	2.0
433.44	21.58	24.09	10.05	6.03	-1.82	83.57	-1.91	57.44	45	30	Si	4.3
481.60	7.91	51.57	10.05	6.03	-0.67	30.64	-4.09	122.95	45	30	Si	2.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	24.18	10.05	6.03	--	--	-1.92	57.64	48	46	Si	5.8
48.16	--	8.02	10.05	6.03	--	--	-0.64	19.13	48	46	Si	18
240.80	21.54	--	10.05	6.03	-1.82	83.43	--	--	46	48	Si	4.3
433.44	--	21.57	10.05	6.03	--	--	-1.71	51.43	48	46	Si	6.5
481.60	--	45.87	10.05	6.03	--	--	-3.64	109.36	48	46	Si	3.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	23.06	10.05	6.03	--	--	-1.83	54.96	52	52	Si	6.1
48.16	--	7.60	10.05	6.03	--	--	-0.60	18.12	52	52	Si	19
240.80	20.60	--	10.05	6.03	-1.74	79.79	--	--	52	52	Si	4.5
433.44	--	20.73	10.05	6.03	--	--	-1.64	49.43	52	52	Si	6.8
481.60	--	43.97	10.05	6.03	--	--	-3.49	104.83	52	52	Si	3.2

Trave: 111 [115,121], Pilastrate [15,21] Sez. R: By=30.00 cm Bz=50.00 cm L=430.70 cm Ln=430.70 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	1.19	16.95	10.05	6.03	-0.10	4.62	-1.34	40.42	45	30	Si	8.9
43.07	11.94	5.35	10.05	6.03	-1.01	46.25	-0.42	12.76	45	30	Si	7.8
215.35	39.02	--	10.05	6.03	-3.30	151.13	--	--	44	40	Si	2.4
387.63	29.50	16.97	10.05	6.03	-2.49	114.28	-1.35	40.46	45	30	Si	3.2
430.70	23.23	31.35	10.05	6.03	-1.96	90.00	-2.49	74.75	45	30	Si	4.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	15.05	10.05	6.03	--	--	-1.19	35.88	48	46	Si	9.4
43.07	--	4.68	10.05	6.03	--	--	-0.37	11.15	48	46	Si	30
215.35	10.81	--	10.05	6.03	-0.91	41.86	--	--	46	48	Si	8.6
387.63	--	15.30	10.05	6.03	--	--	-1.21	36.47	48	46	Si	9.2
430.70	--	28.22	10.05	6.03	--	--	-2.24	67.27	48	46	Si	5.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	14.42	10.05	6.03	--	--	-1.14	34.37	52	52	Si	9.8
43.07	--	4.45	10.05	6.03	--	--	-0.35	10.62	52	52	Si	32
215.35	10.40	--	10.05	6.03	-0.88	40.28	--	--	52	52	Si	8.9
387.63	--	14.74	10.05	6.03	--	--	-1.17	35.14	52	52	Si	9.6
430.70	--	27.17	10.05	6.03	--	--	-2.15	64.77	52	52	Si	5.2

Trave: 111 [121,124], Pilastrate [21,24] Sez. R: By=30.00 cm Bz=50.00 cm L=287.70 cm Ln=287.70 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	4.72	4.71	10.05	6.03	-0.40	18.28	-0.37	11.23	45	30	Si	20
28.77	12.70	0.21	10.05	6.03	-1.07	49.19	-0.02	0.49	44	40	Si	7.3
143.85	36.27	--	10.05	6.03	-3.06	140.47	--	--	44	40	Si	2.6
258.93	42.08	5.15	10.05	6.03	-3.55	162.99	-0.41	12.28	45	30	Si	2.2
287.70	42.00	11.66	10.05	6.03	-3.55	162.67	-0.92	27.80	45	30	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	4.38	10.05	6.03	--	--	-0.35	10.44	48	46	Si	32
28.77	0.22	--	10.05	6.03	-0.02	0.86	--	--	46	48	Si	>100
143.85	7.05	--	10.05	6.03	-0.60	27.30	--	--	46	48	Si	13
258.93	--	4.66	10.05	6.03	--	--	-0.37	11.12	48	46	Si	30
287.70	--	10.49	10.05	6.03	--	--	-0.83	25.00	48	46	Si	13

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	4.27	10.05	6.03	--	--	-0.34	10.17	52	52	Si	33
28.77	0.16	--	10.05	6.03	-0.01	0.63	--	--	52	52	Si	>100
143.85	6.74	--	10.05	6.03	-0.57	26.11	--	--	52	52	Si	14
258.93	--	4.50	10.05	6.03	--	--	-0.36	10.73	52	52	Si	31
287.70	--	10.10	10.05	6.03	--	--	-0.80	24.07	52	52	Si	14

Trave: 111 [124,129], Pilastrate [24,29] Sez. R: By=30.00 cm Bz=50.00 cm L=439.90 cm Ln=439.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	32.90	10.05	6.03	--	--	-2.61	78.44	45	30	Si	4.6
43.99	1.41	17.23	10.05	6.03	-0.12	5.47	-1.37	41.07	45	30	Si	8.8
219.95	40.93	--	10.05	6.03	-3.46	158.56	--	--	44	40	Si	2.3
395.91	40.49	0.31	10.05	6.03	-3.42	156.82	-0.02	0.74	45	30	Si	2.3
439.90	36.52	11.75	10.05	6.03	-3.08	141.46	-0.93	28.02	45	30	Si	2.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	29.77	10.05	6.03	--	--	-2.36	70.96	48	46	Si	4.7
43.99	--	15.67	10.05	6.03	--	--	-1.24	37.36	48	46	Si	9.0
219.95	13.91	--	10.05	6.03	-1.17	53.87	--	--	46	48	Si	6.7
395.91	0.02	0.06	10.05	6.03	-0.00	0.09	-0.00	0.14	48	46	Si	>100
439.90	--	10.26	10.05	6.03	--	--	-0.81	24.45	48	46	Si	14

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	28.72	10.05	6.03	--	--	-2.28	68.47	52	52	Si	4.9
43.99	--	15.15	10.05	6.03	--	--	-1.20	36.12	52	52	Si	9.3
219.95	13.37	--	10.05	6.03	-1.13	51.77	--	--	52	52	Si	7.0
395.91	0.02	--	10.05	6.03	-0.00	0.09	--	--	52	52	Si	>100
439.90	--	9.76	10.05	6.03	--	--	-0.77	23.26	52	52	Si	14

Trave: 112 [113,122], Pilastrate [13,22] Sez. R: By=30.00 cm Bz=50.00 cm L=466.53 cm Ln=461.17 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	28.58	10.05	6.03	--	--	-2.27	68.15	45	30	Si	5.3
46.12	12.54	10.16	10.05	6.03	-1.06	48.56	-0.81	24.22	45	30	Si	7.4

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
230.59	49.52	--	10.05	6.03	-4.18	191.82	--	--	44	40	Si	1.9
415.05	14.94	23.01	10.05	6.03	-1.26	57.87	-1.82	54.85	45	30	Si	6.2
461.17	--	49.76	10.05	6.03	--	--	-3.95	118.64	45	30	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	27.04	10.05	6.03	--	--	-2.14	64.47	48	46	Si	5.2
46.12	--	9.65	10.05	6.03	--	--	-0.76	23.00	48	46	Si	15
230.59	22.23	--	10.05	6.03	-1.88	86.09	--	--	46	48	Si	4.2
415.05	--	21.61	10.05	6.03	--	--	-1.71	51.51	48	46	Si	6.5
461.17	--	46.57	10.05	6.03	--	--	-3.69	111.03	48	46	Si	3.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	26.53	10.05	6.03	--	--	-2.10	63.24	52	52	Si	5.3
46.12	--	9.48	10.05	6.03	--	--	-0.75	22.59	52	52	Si	15
230.59	21.70	--	10.05	6.03	-1.83	84.07	--	--	52	52	Si	4.3
415.05	--	21.14	10.05	6.03	--	--	-1.68	50.40	52	52	Si	6.7
461.17	--	45.51	10.05	6.03	--	--	-3.61	108.49	52	52	Si	3.1

Trave: 112 [122,125], Pilastrate [22,25] Sez. R: By=30.00 cm Bz=50.00 cm L=289.26 cm Ln=287.70 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	19.55	9.98	10.05	6.03	-1.65	75.74	-0.79	23.79	45	30	Si	4.8
28.77	28.48	0.26	10.05	6.03	-2.41	110.33	-0.02	0.62	44	40	Si	3.3
143.85	42.83	--	10.05	6.03	-3.62	165.88	--	--	44	40	Si	2.2
258.93	17.18	16.70	10.05	6.03	-1.45	66.56	-1.32	39.82	45	30	Si	5.4
287.70	5.99	32.09	10.05	6.03	-0.51	23.21	-2.55	76.51	45	30	Si	4.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	9.49	10.05	6.03	--	--	-0.75	22.63	47	46	Si	15
28.77	0.36	--	10.05	6.03	-0.03	1.41	--	--	46	48	Si	>100
143.85	14.14	--	10.05	6.03	-1.19	54.76	--	--	46	48	Si	6.6
258.93	--	15.30	10.05	6.03	--	--	-1.21	36.48	48	46	Si	9.2
287.70	--	29.48	10.05	6.03	--	--	-2.34	70.28	48	46	Si	4.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	9.33	10.05	6.03	--	--	-0.74	22.24	52	52	Si	15
28.77	0.27	--	10.05	6.03	-0.02	1.06	--	--	52	52	Si	>100
143.85	13.73	--	10.05	6.03	-1.16	53.19	--	--	52	52	Si	6.8
258.93	--	14.84	10.05	6.03	--	--	-1.18	35.37	52	52	Si	9.5
287.70	--	28.61	10.05	6.03	--	--	-2.27	68.20	52	52	Si	4.9

Trave: 112 [125,130], Pilastrate [25,30] Sez. R: By=60.00 cm Bz=25.00 cm L=440.01 cm Ln=440.13 cm
Criterio: Travi spessore

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.57	22.12	12.06	--	--	-2.34	45.43	45	30	Si	6.4
44.01	4.71	8.61	22.12	12.06	-0.56	19.43	-1.03	20.00	45	30	Si	14
220.06	26.89	--	12.06	12.06	-3.83	111.62	--	--	44	40	Si	3.2
396.11	15.29	9.10	12.06	12.06	-2.18	63.46	-1.30	37.78	45	30	Si	5.7
440.13	8.99	20.62	12.06	12.06	-1.28	37.34	-2.94	85.59	45	30	Si	4.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	17.66	22.12	12.06	--	--	-2.11	41.01	48	46	Si	5.3
44.01	--	7.79	22.12	12.06	--	--	-0.93	18.09	48	46	Si	12
220.06	10.73	--	12.06	12.06	-1.53	44.53	--	--	46	48	Si	7.3
396.11	--	8.16	12.06	12.06	--	--	-1.16	33.86	48	46	Si	9.6
440.13	--	18.51	12.06	12.06	--	--	-2.64	76.83	48	46	Si	4.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	17.03	22.12	12.06	--	--	-2.04	39.54	52	52	Si	5.5
44.01	--	7.52	22.12	12.06	--	--	-0.90	17.46	52	52	Si	12
220.06	10.33	--	12.06	12.06	-1.47	42.87	--	--	52	52	Si	7.6
396.11	--	7.84	12.06	12.06	--	--	-1.12	32.56	52	52	Si	10
440.13	--	17.80	12.06	12.06	--	--	-2.54	73.91	52	52	Si	4.4

Verifica formazione fessure: σcta[MPa]=2.15

X	M+	M-	Afsup	Afinf	σc+	σct+	σc-	σct-	Cb+	Cb-.	Ver.	Cs
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.57	22.12	12.06	--	--	-2.14	1.16	45	30	Si	1.8
44.01	4.71	8.61	22.12	12.06	-0.47	0.35	-0.94	0.51	45	30	Si	4.2
220.06	26.89	--	12.06	12.06	-3.22	2.08	--	--	44	40	Si	1.0
396.11	15.29	9.10	12.06	12.06	-1.83	1.18	-1.09	0.70	45	30	Si	1.8
440.13	8.99	20.62	12.06	12.06	-1.08	0.70	-2.47	1.60	45	30	Si	1.3

Trave: 113 [123,126], Pilastrate [23,26] Sez. R: By=30.00 cm Bz=50.00 cm L=142.97 cm Ln=165.76 cm
Criterio: Travi tozze

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	29.13	--	10.05	8.04	-2.23	85.34	--	--	44	40	Si	4.2
16.58	31.62	--	10.05	8.04	-2.42	92.63	--	--	44	40	Si	3.9
82.88	31.90	--	10.05	8.04	-2.45	93.44	--	--	44	40	Si	3.9
149.18	22.05	23.42	10.05	8.04	-1.69	64.61	-1.76	55.56	45	30	Si	5.6
165.76	18.14	32.05	10.05	8.04	-1.39	53.16	-2.41	76.02	45	30	Si	4.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	8.77	--	10.05	8.04	-0.67	25.68	--	--	46	48	Si	14
16.58	9.28	--	10.05	8.04	-0.71	27.17	--	--	46	48	Si	13
82.88	1.70	--	10.05	8.04	-0.13	4.98	--	--	46	48	Si	72
149.18	--	21.24	10.05	8.04	--	--	-1.60	50.36	48	46	Si	7.0
165.76	--	29.05	10.05	8.04	--	--	-2.18	68.89	48	46	Si	5.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	8.23	--	10.05	8.04	-0.63	24.12	--	--	52	52	Si	15
16.58	8.77	--	10.05	8.04	-0.67	25.70	--	--	52	52	Si	14
82.88	1.59	--	10.05	8.04	-0.12	4.66	--	--	52	52	Si	77
149.18	--	20.51	10.05	8.04	--	--	-1.54	48.63	52	52	Si	7.3
165.76	--	28.05	10.05	8.04	--	--	-2.11	66.52	52	52	Si	5.3

Trave: 113 [126,131], Pilastrate [26,31] Sez. R: By=30.00 cm Bz=50.00 cm L=439.90 cm Ln=439.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	11.28	9.44	10.05	8.04	-0.86	33.04	-0.71	22.40	45	30	Si	11
43.99	20.93	--	10.05	8.04	-1.61	61.32	--	--	45	35	Si	5.9
219.95	45.99	--	10.05	8.04	-3.53	134.74	--	--	44	40	Si	2.7
395.91	29.64	12.43	10.05	8.04	-2.27	86.84	-0.93	29.47	45	30	Si	4.1
439.90	21.89	27.77	10.05	8.04	-1.68	64.11	-2.09	65.86	45	30	Si	5.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	7.98	10.05	8.04	--	--	-0.60	18.94	48	46	Si	19
43.99	2.12	--	10.05	8.04	-0.16	6.22	--	--	48	47	Si	58
219.95	17.08	--	10.05	8.04	-1.31	50.05	--	--	46	48	Si	7.2
395.91	--	11.41	10.05	8.04	--	--	-0.86	27.06	48	46	Si	13
439.90	--	25.23	10.05	8.04	--	--	-1.90	59.85	48	46	Si	5.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	7.50	10.05	8.04	--	--	-0.56	17.78	52	52	Si	20
43.99	2.12	--	10.05	8.04	-0.16	6.22	--	--	52	52	Si	58
219.95	16.45	--	10.05	8.04	-1.26	48.18	--	--	52	52	Si	7.5
395.91	--	11.07	10.05	8.04	--	--	-0.83	26.25	52	52	Si	13
439.90	--	24.39	10.05	8.04	--	--	-1.83	57.85	52	52	Si	6.1

Trave: 114 [116,114], Pilastrate [16,14] Sez. R: By=30.00 cm Bz=50.00 cm L=310.00 cm Ln=310.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	10.48	10.34	10.05	6.03	-0.88	40.59	-0.82	24.65	45	30	Si	8.9
31.00	13.38	7.74	10.05	6.03	-1.13	51.82	-0.61	18.46	45	30	Si	6.9
155.00	20.00	3.19	10.05	6.03	-1.69	77.48	-0.25	7.60	45	30	Si	4.6
279.00	18.37	8.34	10.05	6.03	-1.55	71.17	-0.66	19.89	45	30	Si	5.1
310.00	16.72	11.09	10.05	6.03	-1.41	64.77	-0.88	26.44	45	30	Si	5.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	9.39	10.05	6.03	--	--	-0.74	22.38	48	46	Si	15
31.00	--	6.94	10.05	6.03	--	--	-0.55	16.55	48	46	Si	20
155.00	--	2.74	10.05	6.03	--	--	-0.22	6.53	48	46	Si	52
279.00	--	7.81	10.05	6.03	--	--	-0.62	18.61	47	46	Si	18
310.00	--	10.47	10.05	6.03	--	--	-0.83	24.96	47	46	Si	13

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	9.07	10.05	6.03	--	--	-0.72	21.62	52	52	Si	16
31.00	--	6.68	10.05	6.03	--	--	-0.53	15.91	52	52	Si	21
155.00	--	2.59	10.05	6.03	--	--	-0.21	6.17	52	52	Si	55
279.00	--	7.63	10.05	6.03	--	--	-0.61	18.19	52	52	Si	19
310.00	--	10.26	10.05	6.03	--	--	-0.81	24.47	52	52	Si	14

Trave: 115 [113,109], Pilastrate [13,9] Sez. R: By=60.00 cm Bz=25.00 cm L=310.56 cm Ln=310.56 cm
Criterio: Travi spessore

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	26.56	12.06	12.06	--	--	-3.79	110.25	45	30	Si	3.3
31.06	5.29	17.02	12.06	12.06	-0.75	21.95	-2.43	70.64	45	30	Si	5.1

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
155.28	20.43	--	12.06	12.06	-2.91	84.80	--	--	44	40	Si	4.2
279.51	13.40	--	12.06	12.06	-1.91	55.65	--	--	44	40	Si	6.5
310.56	7.82	4.51	12.06	12.06	-1.11	32.46	-0.64	18.72	44	40	Si	11

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	24.80	12.06	12.06	--	--	-3.54	102.95	48	46	Si	3.2
31.06	--	15.75	12.06	12.06	--	--	-2.25	65.39	48	46	Si	5.0
155.28	5.16	--	12.06	12.06	-0.74	21.43	--	--	46	47	Si	15
279.51	0.88	--	12.06	12.06	-0.13	3.66	--	--	46	48	Si	89
310.56	--	4.07	12.06	12.06	--	--	-0.58	16.91	46	48	Si	19

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	24.21	12.06	12.06	--	--	-3.45	100.52	52	52	Si	3.2
31.06	--	15.33	12.06	12.06	--	--	-2.19	63.63	52	52	Si	5.1
155.28	5.14	--	12.06	12.06	-0.73	21.35	--	--	52	52	Si	15
279.51	0.78	--	12.06	12.06	-0.11	3.23	--	--	52	52	Si	>100
310.56	--	4.07	12.06	12.06	--	--	-0.58	16.91	52	52	Si	19

Verifica formazione fessure: σcta[MPa]=2.15

X	M+	M-	Afsup	Afinf	σc+	σct+	σc-	σct-	Cb+	Cb-.	Ver.	Cs
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	26.56	12.06	12.06	--	--	-3.18	2.06	45	30	Si	1.0
31.06	5.29	17.02	12.06	12.06	-0.63	0.41	-2.04	1.32	45	30	Si	1.6
155.28	20.43	--	12.06	12.06	-2.44	1.58	--	--	44	40	Si	1.4
279.51	13.40	--	12.06	12.06	-1.60	1.04	--	--	44	40	Si	2.1
310.56	7.82	4.51	12.06	12.06	-0.94	0.61	-0.54	0.35	44	40	Si	3.5

Trave: 116 [108,103], Pilastrate [8,3] Sez. R: By=30.00 cm Bz=50.00 cm L=305.05 cm Ln=305.05 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	28.86	10.05	6.03	--	--	-2.29	68.79	40	26	Si	5.2
30.50	--	18.77	10.05	6.03	--	--	-1.49	44.75	40	26	Si	8.0
152.52	18.57	--	10.05	6.03	-1.57	71.92	--	--	44	40	Si	5.0
274.54	43.54	--	10.05	6.03	-3.68	168.64	--	--	44	40	Si	2.1
305.05	48.29	--	10.05	6.03	-4.08	187.04	--	--	44	40	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	23.97	10.05	6.03	--	--	-1.90	57.16	48	46	Si	5.9
30.50	--	16.69	10.05	6.03	--	--	-1.32	39.79	48	46	Si	8.5
152.52	5.46	--	10.05	6.03	-0.46	21.16	--	--	46	48	Si	17
274.54	16.81	--	10.05	6.03	-1.42	65.12	--	--	46	48	Si	5.5
305.05	18.18	--	10.05	6.03	-1.54	70.42	--	--	46	48	Si	5.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	23.24	10.05	6.03	--	--	-1.84	55.39	52	52	Si	6.1
30.50	--	16.17	10.05	6.03	--	--	-1.28	38.56	52	52	Si	8.7
152.52	5.30	--	10.05	6.03	-0.45	20.52	--	--	52	52	Si	18
274.54	16.26	--	10.05	6.03	-1.37	62.97	--	--	52	52	Si	5.7
305.05	17.56	--	10.05	6.03	-1.48	68.02	--	--	52	52	Si	5.3

Trave: 117 [117,118], Pilastrate [17,18] Sez. R: By=30.00 cm Bz=50.00 cm L=179.02 cm Ln=201.49 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	6.18	23.10	10.05	6.03	-0.52	23.92	-1.83	55.07	45	30	Si	6.5
20.15	12.20	17.19	10.05	6.03	-1.03	47.24	-1.36	40.98	45	30	Si	7.6
100.74	28.18	3.95	10.05	6.03	-2.38	109.17	-0.31	9.41	45	30	Si	3.3
181.34	31.22	7.32	10.05	6.03	-2.64	120.95	-0.58	17.45	45	30	Si	3.0
201.49	30.25	10.39	10.05	6.03	-2.55	117.17	-0.82	24.77	45	30	Si	3.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.96	10.05	6.03	--	--	-1.66	49.97	48	46	Si	6.7
20.15	--	15.55	10.05	6.03	--	--	-1.23	37.07	48	46	Si	9.1
100.74	--	3.61	10.05	6.03	--	--	-0.29	8.60	47	46	Si	39
181.34	--	7.18	10.05	6.03	--	--	-0.57	17.11	47	46	Si	20
201.49	--	10.15	10.05	6.03	--	--	-0.81	24.20	48	46	Si	14

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.25	10.05	6.03	--	--	-1.61	48.27	52	52	Si	7.0
20.15	--	15.00	10.05	6.03	--	--	-1.19	35.76	52	52	Si	9.4
100.74	--	3.49	10.05	6.03	--	--	-0.28	8.33	52	52	Si	40
181.34	--	7.13	10.05	6.03	--	--	-0.57	17.00	52	52	Si	20
201.49	--	10.07	10.05	6.03	--	--	-0.80	24.01	52	52	Si	14

Trave: 117 [118,119], Pilastrate [18,19] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	14.92	17.37	10.05	6.03	-1.26	57.80	-1.38	41.42	45	30	Si	6.2
42.70	27.25	2.23	10.05	6.03	-2.30	105.54	-0.18	5.31	45	35	Si	3.4
213.50	46.67	--	10.05	6.03	-3.94	180.79	--	--	44	40	Si	2.0
384.30	8.32	27.00	10.05	6.03	-0.70	32.22	-2.14	64.36	45	30	Si	5.6
427.00	--	48.66	10.05	6.03	--	--	-3.86	116.01	45	30	Si	3.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	16.38	10.05	6.03	--	--	-1.30	39.05	48	46	Si	8.6
42.70	--	1.99	10.05	6.03	--	--	-0.16	4.73	48	47	Si	71
213.50	17.38	--	10.05	6.03	-1.47	67.32	--	--	46	48	Si	5.3
384.30	--	25.19	10.05	6.03	--	--	-2.00	60.05	48	46	Si	5.6
427.00	--	45.51	10.05	6.03	--	--	-3.61	108.49	48	46	Si	3.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	16.05	10.05	6.03	--	--	-1.27	38.26	52	52	Si	8.8
42.70	--	1.93	10.05	6.03	--	--	-0.15	4.60	52	52	Si	73
213.50	17.02	--	10.05	6.03	-1.44	65.93	--	--	52	52	Si	5.5
384.30	--	24.59	10.05	6.03	--	--	-1.95	58.62	52	52	Si	5.7
427.00	--	44.45	10.05	6.03	--	--	-3.53	105.98	52	52	Si	3.2

Trave: 117 [119,120], Pilastrate [19,20] Sez. R: By=60.00 cm Bz=25.00 cm L=530.00 cm Ln=530.00 cm
Criterio: Travi spessore

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	26.06	24.13	14.07	--	--	-2.93	55.49	45	30	Si	5.1
53.00	2.89	12.04	24.13	14.07	-0.32	10.24	-1.35	25.63	45	30	Si	11
265.00	28.83	--	14.07	14.07	-3.77	102.93	--	--	44	40	Si	3.5
477.00	12.82	9.87	14.07	14.07	-1.68	45.77	-1.29	35.25	45	30	Si	7.9
530.00	4.35	23.74	14.07	14.07	-0.57	15.53	-3.10	84.76	45	30	Si	4.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	23.61	24.13	14.07	--	--	-2.66	50.28	48	46	Si	4.2
53.00	--	10.90	24.13	14.07	--	--	-1.23	23.21	48	46	Si	9.1
265.00	13.10	--	14.07	14.07	-1.71	46.78	--	--	46	48	Si	6.5
477.00	--	8.99	14.07	14.07	--	--	-1.18	32.11	48	46	Si	9.5
530.00	--	21.56	14.07	14.07	--	--	-2.82	76.99	48	46	Si	4.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	22.80	24.13	14.07	--	--	-2.57	48.54	52	52	Si	4.4
53.00	--	10.52	24.13	14.07	--	--	-1.18	22.40	52	52	Si	9.5
265.00	12.65	--	14.07	14.07	-1.65	45.15	--	--	52	52	Si	6.8
477.00	--	8.70	14.07	14.07	--	--	-1.14	31.06	52	52	Si	9.9
530.00	--	20.84	14.07	14.07	--	--	-2.72	74.40	52	52	Si	4.1

Verifica formazione fessure: σcta[MPa]=2.15

X	M+	M-	Afsup	Afinf	σc+	σct+	σc-	σct-	Cb+	Cb-.	Ver.	Cs
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	26.06	24.13	14.07	--	--	-2.71	1.47	45	30	Si	1.5
53.00	2.89	12.04	24.13	14.07	-0.28	0.20	-1.25	0.68	45	30	Si	3.2
265.00	28.83	--	14.07	14.07	-3.25	2.08	--	--	44	40	Si	1.0
477.00	12.82	9.87	14.07	14.07	-1.45	0.93	-1.11	0.71	45	30	Si	2.3
530.00	4.35	23.74	14.07	14.07	-0.49	0.31	-2.68	1.71	45	30	Si	1.3

Trave: 118 [127,128], Pilastrate [27,28] Sez. R: By=30.00 cm Bz=50.00 cm L=500.00 cm Ln=500.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	25.66	10.05	6.03	--	--	-2.04	61.17	40	26	Si	5.9
50.00	--	7.24	10.05	6.03	--	--	-0.57	17.27	45	30	Si	21
250.00	44.05	--	10.05	6.03	-3.72	170.63	--	--	44	40	Si	2.1
450.00	43.70	18.60	10.05	6.03	-3.69	169.27	-1.47	44.34	45	30	Si	2.1
500.00	38.68	36.28	10.05	6.03	-3.27	149.83	-2.88	86.49	45	30	Si	2.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.55	10.05	6.03	--	--	-1.55	46.62	48	46	Si	7.2
50.00	--	6.27	10.05	6.03	--	--	-0.50	14.95	48	46	Si	23
250.00	14.53	--	10.05	6.03	-1.23	56.28	--	--	46	48	Si	6.4
450.00	--	16.88	10.05	6.03	--	--	-1.34	40.23	48	46	Si	8.4
500.00	--	32.81	10.05	6.03	--	--	-2.60	78.22	48	46	Si	4.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	18.71	10.05	6.03	--	--	-1.48	44.61	52	52	Si	7.6
50.00	--	5.95	10.05	6.03	--	--	-0.47	14.18	52	52	Si	24
250.00	14.00	--	10.05	6.03	-1.18	54.21	--	--	52	52	Si	6.6
450.00	--	16.30	10.05	6.03	--	--	-1.29	38.87	52	52	Si	8.7

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
500.00	--	31.65	10.05	6.03	--	--	-2.51	75.46	52	52	Si	4.5

Trave: 119 [110,111], Pilastrate [10,11] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	15.84	0.68	10.05	6.03	-1.34	61.36	-0.05	1.62	44	40	Si	5.9
42.70	23.44	--	10.05	6.03	-1.98	90.79	--	--	44	40	Si	4.0
213.50	36.47	--	10.05	6.03	-3.08	141.28	--	--	44	40	Si	2.5
384.30	24.05	15.64	10.05	6.03	-2.03	93.17	-1.24	37.27	45	30	Si	3.9
427.00	17.66	27.06	10.05	6.03	-1.49	68.42	-2.15	64.50	45	30	Si	5.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	0.15	--	10.05	6.03	-0.01	0.57	--	--	46	48	Si	>100
42.70	5.60	--	10.05	6.03	-0.47	21.67	--	--	46	48	Si	17
213.50	10.03	--	10.05	6.03	-0.85	38.84	--	--	46	47	Si	9.3
384.30	--	14.26	10.05	6.03	--	--	-1.13	33.99	48	46	Si	9.9
427.00	--	24.82	10.05	6.03	--	--	-1.97	59.16	48	46	Si	5.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	0.03	--	10.05	6.03	-0.00	0.12	--	--	52	52	Si	>100
42.70	5.37	--	10.05	6.03	-0.45	20.78	--	--	52	52	Si	17
213.50	9.79	--	10.05	6.03	-0.83	37.90	--	--	52	52	Si	9.5
384.30	--	13.80	10.05	6.03	--	--	-1.09	32.89	52	52	Si	10
427.00	--	24.07	10.05	6.03	--	--	-1.91	57.38	52	52	Si	5.9

Trave: 119 [111,112], Pilastrate [11,12] Sez. R: By=30.00 cm Bz=50.00 cm L=530.00 cm Ln=530.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	22.40	10.05	6.03	--	--	-1.78	53.40	45	30	Si	6.7
53.00	11.34	8.88	10.05	6.03	-0.96	43.93	-0.70	21.17	45	30	Si	8.2
265.00	41.92	--	10.05	6.03	-3.54	162.37	--	--	44	40	Si	2.2
477.00	31.64	7.14	10.05	6.03	-2.67	122.56	-0.57	17.02	45	30	Si	2.9
530.00	24.90	20.22	10.05	6.03	-2.10	96.44	-1.60	48.21	45	30	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.43	10.05	6.03	--	--	-1.62	48.72	48	46	Si	6.9
53.00	--	8.13	10.05	6.03	--	--	-0.65	19.39	48	46	Si	17
265.00	14.45	--	10.05	6.03	-1.22	55.97	--	--	46	48	Si	6.4
477.00	--	6.48	10.05	6.03	--	--	-0.51	15.45	48	46	Si	22
530.00	--	18.37	10.05	6.03	--	--	-1.46	43.80	48	46	Si	7.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.78	10.05	6.03	--	--	-1.57	47.16	52	52	Si	7.1
53.00	--	7.88	10.05	6.03	--	--	-0.63	18.80	52	52	Si	18
265.00	13.96	--	10.05	6.03	-1.18	54.08	--	--	52	52	Si	6.7
477.00	--	6.26	10.05	6.03	--	--	-0.50	14.93	52	52	Si	23
530.00	--	17.75	10.05	6.03	--	--	-1.41	42.32	52	52	Si	8.0

Trave: 120 [105,110], Pilastrate [5,10] Sez. R: By=30.00 cm Bz=50.00 cm L=378.19 cm Ln=379.38 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	10.05	21.63	10.05	6.03	-0.85	38.93	-1.72	51.56	45	30	Si	7.0
37.94	22.76	2.80	10.05	6.03	-1.92	88.18	-0.22	6.69	45	30	Si	4.1
189.69	45.80	--	10.05	6.03	-3.87	177.39	--	--	44	40	Si	2.0
341.44	0.21	36.53	10.05	6.03	-0.02	0.83	-2.90	87.10	45	30	Si	4.1
379.38	--	64.25	10.05	6.03	--	--	-5.10	153.16	45	30	Si	2.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	18.59	10.05	6.03	--	--	-1.47	44.31	48	46	Si	7.6
37.94	--	1.82	10.05	6.03	--	--	-0.14	4.35	48	46	Si	78
189.69	20.43	--	10.05	6.03	-1.73	79.14	--	--	46	48	Si	4.5
341.44	--	34.03	10.05	6.03	--	--	-2.70	81.12	47	46	Si	4.2
379.38	--	59.27	10.05	6.03	--	--	-4.70	141.30	47	46	Si	2.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	17.57	10.05	6.03	--	--	-1.39	41.89	52	52	Si	8.0
37.94	--	1.50	10.05	6.03	--	--	-0.12	3.57	52	52	Si	94
189.69	19.65	--	10.05	6.03	-1.66	76.12	--	--	52	52	Si	4.7
341.44	--	33.19	10.05	6.03	--	--	-2.63	79.13	52	52	Si	4.3
379.38	--	57.61	10.05	6.03	--	--	-4.57	137.35	52	52	Si	2.5

Trave: 120 [110,118], Pilastrate [10,18] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	56.04	10.05	6.03	--	--	-4.44	133.59	45	30	Si	2.7
46.99	8.00	21.02	10.05	6.03	-0.68	31.00	-1.67	50.11	45	30	Si	7.2
234.95	60.45	--	10.05	6.03	-5.11	234.15	--	--	44	40	Si	1.5
422.91	17.15	16.93	10.05	6.03	-1.45	66.41	-1.34	40.36	45	30	Si	5.4
469.90	--	45.77	10.05	6.03	--	--	-3.63	109.12	45	30	Si	3.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	51.49	10.05	6.03	--	--	-4.08	122.74	47	46	Si	2.7
46.99	--	19.66	10.05	6.03	--	--	-1.56	46.86	47	46	Si	7.2
234.95	35.11	--	10.05	6.03	-2.97	136.00	--	--	46	47	Si	2.6
422.91	--	14.60	10.05	6.03	--	--	-1.16	34.80	48	46	Si	9.7
469.90	--	40.52	10.05	6.03	--	--	-3.21	96.60	48	46	Si	3.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	49.97	10.05	6.03	--	--	-3.96	119.13	52	52	Si	2.8
46.99	--	19.20	10.05	6.03	--	--	-1.52	45.78	52	52	Si	7.4
234.95	33.89	--	10.05	6.03	-2.86	131.27	--	--	52	52	Si	2.7
422.91	--	13.82	10.05	6.03	--	--	-1.10	32.94	52	52	Si	10
469.90	--	38.77	10.05	6.03	--	--	-3.07	92.43	52	52	Si	3.6

Trave: 121 [104,114], Pilastrate [4,14] Sez. R: By=30.00 cm Bz=50.00 cm L=461.53 cm Ln=503.95 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	45.97	10.05	6.03	--	--	-3.65	109.59	45	30	Si	3.3
50.40	18.23	14.42	10.05	6.03	-1.54	70.59	-1.14	34.38	45	30	Si	5.1
251.98	62.56	--	10.05	6.03	-5.28	242.34	--	--	44	40	Si	1.5
453.56	10.89	26.89	10.05	6.03	-0.92	42.19	-2.13	64.10	45	30	Si	5.6
503.95	--	60.21	10.05	6.03	--	--	-4.77	143.54	45	30	Si	2.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	40.90	10.05	6.03	--	--	-3.24	97.49	48	46	Si	3.5
50.40	--	12.66	10.05	6.03	--	--	-1.00	30.17	48	46	Si	11
251.98	33.92	--	10.05	6.03	-2.86	131.37	--	--	46	48	Si	2.7
453.56	--	24.58	10.05	6.03	--	--	-1.95	58.61	48	46	Si	5.7
503.95	--	54.67	10.05	6.03	--	--	-4.34	130.33	48	46	Si	2.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	39.20	10.05	6.03	--	--	-3.11	93.46	52	52	Si	3.6
50.40	--	12.07	10.05	6.03	--	--	-0.96	28.77	52	52	Si	12
251.98	32.64	--	10.05	6.03	-2.76	126.44	--	--	52	52	Si	2.8
453.56	--	23.82	10.05	6.03	--	--	-1.89	56.78	52	52	Si	5.9
503.95	--	52.82	10.05	6.03	--	--	-4.19	125.93	52	52	Si	2.7

Trave: 122 [36,35], Pilastrate [23,17] Sez. R: By=30.00 cm Bz=50.00 cm L=310.00 cm Ln=310.00 cm L2=310.00 cm L3=310.00 cm Criterio: Travi alte
Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	25.26	2116.50	0.012	35.795	228.845

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	7.60	24.49	10.05	6.03	-0.64	29.46	-1.94	58.39	45	30	Si	6.2
31.00	16.27	12.90	10.05	6.03	-1.37	63.02	-1.02	30.75	45	30	Si	5.7
155.00	35.35	--	10.05	6.03	-2.99	136.93	--	--	44	40	Si	2.6
279.00	23.16	6.49	10.05	6.03	-1.96	89.71	-0.52	15.48	45	30	Si	4.0
310.00	16.22	16.49	10.05	6.03	-1.37	62.83	-1.31	39.31	45	30	Si	5.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	22.21	10.05	6.03	--	--	-1.76	52.94	48	46	Si	6.4
31.00	--	11.62	10.05	6.03	--	--	-0.92	27.70	48	46	Si	12
155.00	8.73	--	10.05	6.03	-0.74	33.83	--	--	46	47	Si	11
279.00	--	6.10	10.05	6.03	--	--	-0.48	14.55	48	46	Si	23
310.00	--	15.31	10.05	6.03	--	--	-1.21	36.50	48	46	Si	9.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	21.44	10.05	6.03	--	--	-1.70	51.12	52	52	Si	6.6
31.00	--	11.19	10.05	6.03	--	--	-0.89	26.69	52	52	Si	13
155.00	8.48	--	10.05	6.03	-0.72	32.84	--	--	52	52	Si	11
279.00	--	5.97	10.05	6.03	--	--	-0.47	14.24	52	52	Si	24
310.00	--	14.92	10.05	6.03	--	--	-1.18	35.57	52	52	Si	9.5

Trave: 123 [36,39], Pilastrate [23,--] Sez. R: By=30.00 cm Bz=50.00 cm L=173.00 cm Ln=143.00 cm Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	44	30	Si	>100
14.30	3.04	--	10.05	6.03	-0.26	11.77	--	--	26	40	Si	31
71.50	11.95	--	10.05	6.03	-1.01	46.28	--	--	26	40	Si	7.8
128.70	15.83	--	10.05	6.03	-1.34	61.33	--	--	44	40	Si	5.9
143.00	16.15	--	10.05	6.03	-1.36	62.56	--	--	44	40	Si	5.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	46	48	Si	>100
14.30	2.28	--	10.05	6.03	-0.19	8.84	--	--	46	48	Si	41
71.50	8.53	--	10.05	6.03	-0.72	33.05	--	--	46	48	Si	11
128.70	10.17	--	10.05	6.03	-0.86	39.38	--	--	46	48	Si	9.1
143.00	9.86	--	10.05	6.03	-0.83	38.17	--	--	46	48	Si	9.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	52	52	Si	>100
14.30	2.16	--	10.05	6.03	-0.18	8.37	--	--	52	52	Si	43
71.50	8.04	--	10.05	6.03	-0.68	31.16	--	--	52	52	Si	12
128.70	9.51	--	10.05	6.03	-0.80	36.83	--	--	52	52	Si	9.8
143.00	9.19	--	10.05	6.03	-0.78	35.58	--	--	52	52	Si	10

Trave: 123 [39,116], Pilastrate [--,16] Sez. R: By=30.00 cm Bz=50.00 cm L=398.55 cm Ln=345.39 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	17.05	--	10.05	6.03	-1.44	66.04	--	--	44	40	Si	5.5
34.54	22.60	--	10.05	6.03	-1.91	87.55	--	--	26	40	Si	4.1
172.70	29.38	--	10.05	6.03	-2.48	113.79	--	--	26	40	Si	3.2
310.86	9.24	--	10.05	6.03	-0.78	35.79	--	--	26	40	Si	10
345.39	--	0.00	10.05	6.03	--	--	-0.00	0.00	40	26	Si	>100

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	10.54	--	10.05	6.03	-0.89	40.81	--	--	46	48	Si	8.8
34.54	16.05	--	10.05	6.03	-1.36	62.15	--	--	46	48	Si	5.8
172.70	23.50	--	10.05	6.03	-1.98	91.03	--	--	46	48	Si	4.0
310.86	7.62	--	10.05	6.03	-0.64	29.51	--	--	46	48	Si	12
345.39	--	0.00	10.05	6.03	--	--	-0.00	0.00	47	46	Si	>100

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	9.83	--	10.05	6.03	-0.83	38.07	--	--	52	52	Si	9.5
34.54	15.13	--	10.05	6.03	-1.28	58.61	--	--	52	52	Si	6.1
172.70	22.37	--	10.05	6.03	-1.89	86.66	--	--	52	52	Si	4.2
310.86	7.27	--	10.05	6.03	-0.61	28.15	--	--	52	52	Si	13
345.39	--	0.00	10.05	6.03	--	--	-0.00	0.00	52	52	Si	>100

Trave: 201 [225,226], Pilastrate [25,26] Sez. R: By=30.00 cm Bz=50.00 cm L=604.50 cm Ln=604.50 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	44.96	10.05	6.03	--	--	-3.57	107.19	40	26	Si	3.4
60.45	--	11.16	10.05	6.03	--	--	-0.89	26.61	40	44	Si	14

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
302.25	57.47	--	10.05	6.03	-4.85	222.61	--	--	44	40	Si	1.6
544.05	32.03	6.36	10.05	6.03	-2.70	124.05	-0.50	15.16	45	30	Si	2.9
604.50	17.72	33.37	10.05	6.03	-1.50	68.63	-2.65	79.55	45	30	Si	4.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	37.32	10.05	6.03	--	--	-2.96	88.97	48	46	Si	3.8
60.45	--	9.43	10.05	6.03	--	--	-0.75	22.49	48	46	Si	15
302.25	39.34	--	10.05	6.03	-3.32	152.39	--	--	46	48	Si	2.4
544.05	--	5.74	10.05	6.03	--	--	-0.45	13.67	48	46	Si	25
604.50	--	30.36	10.05	6.03	--	--	-2.41	72.37	48	46	Si	4.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	36.25	10.05	6.03	--	--	-2.87	86.42	52	52	Si	3.9
60.45	--	9.27	10.05	6.03	--	--	-0.74	22.11	52	52	Si	15
302.25	38.00	--	10.05	6.03	-3.21	147.20	--	--	52	52	Si	2.4
544.05	--	5.53	10.05	6.03	--	--	-0.44	13.18	52	52	Si	26
604.50	--	29.36	10.05	6.03	--	--	-2.33	69.98	52	52	Si	4.8

Trave: 202 [213,216], Pilastrate [13,16] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	47.42	10.05	6.03	--	--	-3.76	113.04	40	44	Si	3.2
32.99	--	29.26	10.05	6.03	--	--	-2.32	69.75	40	44	Si	5.2
164.93	27.63	--	10.05	6.03	-2.33	107.01	--	--	44	40	Si	3.4
296.88	54.76	0.10	10.05	6.03	-4.63	212.12	-0.01	0.23	45	30	Si	1.7
329.87	58.66	8.01	10.05	6.03	-4.95	227.23	-0.64	19.10	45	30	Si	1.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	25.39	10.05	6.03	--	--	-2.01	60.52	48	46	Si	5.6
32.99	--	15.73	10.05	6.03	--	--	-1.25	37.50	48	46	Si	9.0
164.93	7.56	--	10.05	6.03	-0.64	29.26	--	--	46	48	Si	12
296.88	0.60	--	10.05	6.03	-0.05	2.34	--	--	48	46	Si	>100
329.87	--	6.43	10.05	6.03	--	--	-0.51	15.34	48	46	Si	22

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	24.58	10.05	6.03	--	--	-1.95	58.59	52	52	Si	5.7
32.99	--	15.28	10.05	6.03	--	--	-1.21	36.43	52	52	Si	9.2
164.93	7.21	--	10.05	6.03	-0.61	27.94	--	--	52	52	Si	13
296.88	0.60	--	10.05	6.03	-0.05	2.34	--	--	52	52	Si	>100
329.87	--	5.91	10.05	6.03	--	--	-0.47	14.09	52	52	Si	24

Trave: 202 [216,223], Pilastrate [16,23] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	68.89	10.05	6.03	--	--	-5.46	164.24	45	30	Si	2.2
53.25	--	34.74	10.05	6.03	--	--	-2.76	82.83	45	30	Si	4.3
266.26	62.49	--	10.05	6.03	-5.28	242.05	--	--	44	40	Si	1.5
479.27	36.06	3.64	10.05	6.03	-3.05	139.69	-0.29	8.67	45	30	Si	2.6
532.52	21.05	33.15	10.05	6.03	-1.78	81.52	-2.63	79.04	45	30	Si	4.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	61.06	10.05	6.03	--	--	-4.84	145.56	48	46	Si	2.3
53.25	--	30.90	10.05	6.03	--	--	-2.45	73.67	48	46	Si	4.6
266.26	34.19	--	10.05	6.03	-2.89	132.44	--	--	46	48	Si	2.7
479.27	--	2.91	10.05	6.03	--	--	-0.23	6.93	48	46	Si	49
532.52	--	28.81	10.05	6.03	--	--	-2.29	68.69	48	46	Si	4.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	58.44	10.05	6.03	--	--	-4.63	139.33	52	52	Si	2.4
53.25	--	29.62	10.05	6.03	--	--	-2.35	70.61	52	52	Si	4.8
266.26	32.66	--	10.05	6.03	-2.76	126.51	--	--	52	52	Si	2.8
479.27	--	2.66	10.05	6.03	--	--	-0.21	6.35	52	52	Si	53
532.52	--	27.37	10.05	6.03	--	--	-2.17	65.24	52	52	Si	5.2

Trave: 203 [213,222], Pilastrate [13,22] Sez. R: By=30.00 cm Bz=50.00 cm L=466.53 cm Ln=461.17 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	33.99	10.05	6.03	--	--	-2.70	81.02	45	30	Si	4.4
46.12	9.81	16.31	10.05	6.03	-0.83	37.99	-1.29	38.88	45	30	Si	9.3
230.59	49.69	--	10.05	6.03	-4.20	192.49	--	--	44	40	Si	1.9
415.05	31.70	13.37	10.05	6.03	-2.68	122.78	-1.06	31.88	45	30	Si	2.9
461.17	20.02	34.00	10.05	6.03	-1.69	77.56	-2.70	81.05	45	30	Si	4.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	30.65	10.05	6.03	--	--	-2.43	73.08	48	46	Si	4.6
46.12	--	14.63	10.05	6.03	--	--	-1.16	34.87	48	46	Si	9.7
230.59	18.58	--	10.05	6.03	-1.57	71.98	--	--	46	48	Si	5.0
415.05	--	12.12	10.05	6.03	--	--	-0.96	28.90	48	46	Si	12
461.17	--	30.83	10.05	6.03	--	--	-2.44	73.50	48	46	Si	4.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	29.54	10.05	6.03	--	--	-2.34	70.43	52	52	Si	4.8
46.12	--	14.07	10.05	6.03	--	--	-1.12	33.54	52	52	Si	10
230.59	17.92	--	10.05	6.03	-1.51	69.39	--	--	52	52	Si	5.2
415.05	--	11.71	10.05	6.03	--	--	-0.93	27.91	52	52	Si	12
461.17	--	29.77	10.05	6.03	--	--	-2.36	70.98	52	52	Si	4.7

Trave: 203 [222,225], Pilastrate [22,25] Sez. R: By=30.00 cm Bz=50.00 cm L=289.26 cm Ln=347.70 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	30.42	10.05	6.03	--	--	-2.41	72.53	45	30	Si	5.0
34.77	3.58	15.62	10.05	6.03	-0.30	13.88	-1.24	37.24	45	30	Si	9.7
173.85	43.65	--	10.05	6.03	-3.69	169.09	--	--	44	40	Si	2.1
312.93	35.07	6.83	10.05	6.03	-2.96	135.84	-0.54	16.28	45	30	Si	2.7
347.70	28.86	22.05	10.05	6.03	-2.44	111.77	-1.75	52.58	45	30	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	26.80	10.05	6.03	--	--	-2.13	63.90	48	46	Si	5.3
34.77	--	13.72	10.05	6.03	--	--	-1.09	32.70	48	46	Si	10
173.85	16.67	--	10.05	6.03	-1.41	64.57	--	--	46	48	Si	5.6
312.93	--	6.32	10.05	6.03	--	--	-0.50	15.07	48	46	Si	22
347.70	--	19.87	10.05	6.03	--	--	-1.58	47.37	48	46	Si	7.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	25.60	10.05	6.03	--	--	-2.03	61.03	52	52	Si	5.5
34.77	--	13.08	10.05	6.03	--	--	-1.04	31.18	52	52	Si	11
173.85	15.93	--	10.05	6.03	-1.35	61.69	--	--	52	52	Si	5.8
312.93	--	6.15	10.05	6.03	--	--	-0.49	14.67	52	52	Si	23
347.70	--	19.14	10.05	6.03	--	--	-1.52	45.63	52	52	Si	7.4

Trave: 204 [223,226], Pilastrate [23,26] Sez. R: By=30.00 cm Bz=50.00 cm L=142.97 cm Ln=165.76 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	1.68	9.66	10.05	6.03	-0.14	6.49	-0.77	23.03	45	30	Si	16
16.58	8.07	6.37	10.05	6.03	-0.68	31.25	-0.51	15.20	45	30	Si	12
82.88	27.89	2.38	10.05	6.03	-2.36	108.02	-0.19	5.68	45	30	Si	3.3
149.18	38.52	13.02	10.05	6.03	-3.25	149.20	-1.03	31.03	45	30	Si	2.4
165.76	39.89	17.74	10.05	6.03	-3.37	154.50	-1.41	42.30	45	30	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	7.92	10.05	6.03	--	--	-0.63	18.88	48	46	Si	18
16.58	--	5.10	10.05	6.03	--	--	-0.40	12.16	48	46	Si	28
82.88	--	1.96	10.05	6.03	--	--	-0.16	4.67	48	46	Si	72
149.18	--	11.81	10.05	6.03	--	--	-0.94	28.16	48	46	Si	12
165.76	--	16.11	10.05	6.03	--	--	-1.28	38.41	48	46	Si	8.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	7.34	10.05	6.03	--	--	-0.58	17.50	52	52	Si	19
16.58	--	4.68	10.05	6.03	--	--	-0.37	11.15	52	52	Si	30
82.88	--	1.82	10.05	6.03	--	--	-0.14	4.34	52	52	Si	78
149.18	--	11.41	10.05	6.03	--	--	-0.91	27.21	52	52	Si	12
165.76	--	15.57	10.05	6.03	--	--	-1.23	37.11	52	52	Si	9.1

Trave: 205 [223,217], Pilastrate [23,17] Sez. R: By=30.00 cm Bz=50.00 cm L=310.00 cm Ln=310.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	29.36	25.27	10.05	6.03	-2.48	113.73	-2.00	60.24	45	30	Si	3.2
31.00	31.32	16.57	10.05	6.03	-2.65	121.31	-1.31	39.50	45	30	Si	3.0
155.00	27.61	--	10.05	6.03	-2.33	106.95	--	--	45	30	Si	3.4
279.00	4.98	6.59	10.05	6.03	-0.42	19.30	-0.52	15.72	45	30	Si	19
310.00	--	12.80	10.05	6.03	--	--	-1.02	30.52	45	30	Si	12

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	22.54	10.05	6.03	--	--	-1.79	53.74	48	46	Si	6.3
31.00	--	14.64	10.05	6.03	--	--	-1.16	34.90	48	46	Si	9.7

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
155.00	2.08	--	10.05	6.03	-0.18	8.07	--	--	48	46	Si	45
279.00	--	5.78	10.05	6.03	--	--	-0.46	13.77	48	46	Si	24
310.00	--	11.46	10.05	6.03	--	--	-0.91	27.32	48	46	Si	12

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	21.63	10.05	6.03	--	--	-1.72	51.57	52	52	Si	6.5
31.00	--	14.00	10.05	6.03	--	--	-1.11	33.37	52	52	Si	10
155.00	2.08	--	10.05	6.03	-0.18	8.07	--	--	52	52	Si	45
279.00	--	5.50	10.05	6.03	--	--	-0.44	13.12	52	52	Si	26
310.00	--	11.01	10.05	6.03	--	--	-0.87	26.26	52	52	Si	13

Trave: 206 [217,218], Pilastrate [17,18] Sez. R: By=30.00 cm Bz=50.00 cm L=179.02 cm Ln=179.02 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	23.86	18.13	10.05	6.03	-2.02	92.43	-1.44	43.22	45	30	Si	3.9
17.90	28.21	13.34	10.05	6.03	-2.38	109.27	-1.06	31.81	45	30	Si	3.3
89.51	41.09	0.81	10.05	6.03	-3.47	159.15	-0.06	1.92	45	30	Si	2.3
161.11	47.86	0.24	10.05	6.03	-4.04	185.39	-0.02	0.57	44	40	Si	1.9
179.02	48.30	1.55	10.05	6.03	-4.08	187.10	-0.12	3.70	44	40	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	15.29	10.05	6.03	--	--	-1.21	36.44	48	46	Si	9.2
17.90	--	11.11	10.05	6.03	--	--	-0.88	26.50	48	46	Si	13
89.51	--	0.41	10.05	6.03	--	--	-0.03	0.98	48	46	Si	>100
161.11	0.76	--	10.05	6.03	-0.06	2.95	--	--	46	48	Si	>100
179.02	--	0.59	10.05	6.03	--	--	-0.05	1.41	46	48	Si	>100

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	14.34	10.05	6.03	--	--	-1.14	34.18	52	52	Si	9.9
17.90	--	10.37	10.05	6.03	--	--	-0.82	24.73	52	52	Si	14
89.51	--	0.28	10.05	6.03	--	--	-0.02	0.66	52	52	Si	>100
161.11	0.62	--	10.05	6.03	-0.05	2.39	--	--	52	52	Si	>100
179.02	--	0.59	10.05	6.03	--	--	-0.05	1.41	52	52	Si	>100

Trave: 206 [218,219], Pilastrate [18,19] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	2.72	18.18	10.05	6.03	-0.23	10.53	-1.44	43.34	45	30	Si	8.3
42.70	14.46	5.09	10.05	6.03	-1.22	56.01	-0.40	12.12	45	30	Si	6.4
213.50	42.99	--	10.05	6.03	-3.63	166.53	--	--	44	40	Si	2.2
384.30	28.45	13.46	10.05	6.03	-2.40	110.21	-1.07	32.09	45	30	Si	3.3
427.00	20.14	28.74	10.05	6.03	-1.70	78.00	-2.28	68.52	45	30	Si	4.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	16.19	10.05	6.03	--	--	-1.28	38.61	48	46	Si	8.7
42.70	--	4.34	10.05	6.03	--	--	-0.34	10.34	48	46	Si	33
213.50	14.59	--	10.05	6.03	-1.23	56.51	--	--	46	48	Si	6.4
384.30	--	12.64	10.05	6.03	--	--	-1.00	30.13	48	46	Si	11
427.00	--	26.66	10.05	6.03	--	--	-2.11	63.56	48	46	Si	5.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	15.53	10.05	6.03	--	--	-1.23	37.03	52	52	Si	9.1
42.70	--	4.09	10.05	6.03	--	--	-0.32	9.74	52	52	Si	35
213.50	14.11	--	10.05	6.03	-1.19	54.66	--	--	52	52	Si	6.6
384.30	--	12.37	10.05	6.03	--	--	-0.98	29.48	52	52	Si	11
427.00	--	25.97	10.05	6.03	--	--	-2.06	61.90	52	52	Si	5.4

Trave: 207 [204,205], Pilastrate [4,5] Sez. R: By=30.00 cm Bz=50.00 cm L=590.40 cm Ln=590.40 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	60.96	10.05	6.03	--	--	-4.83	145.33	45	30	Si	2.5
59.04	--	30.01	10.05	6.03	--	--	-2.38	71.54	45	30	Si	5.0
295.20	54.43	--	10.05	6.03	-4.60	210.83	--	--	44	40	Si	1.7
531.36	32.36	19.27	10.05	6.03	-2.73	125.35	-1.53	45.95	45	30	Si	2.9
590.40	16.64	49.29	10.05	6.03	-1.40	64.43	-3.91	117.50	45	30	Si	3.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	55.43	10.05	6.03	--	--	-4.40	132.14	48	46	Si	2.5
59.04	--	27.31	10.05	6.03	--	--	-2.17	65.10	48	46	Si	5.2
295.20	27.52	--	10.05	6.03	-2.32	106.60	--	--	46	48	Si	3.4
531.36	--	17.39	10.05	6.03	--	--	-1.38	41.45	48	46	Si	8.1
590.40	--	44.54	10.05	6.03	--	--	-3.53	106.18	48	46	Si	3.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	53.58	10.05	6.03	--	--	-4.25	127.74	52	52	Si	2.6
59.04	--	26.41	10.05	6.03	--	--	-2.09	62.95	52	52	Si	5.4
295.20	26.57	--	10.05	6.03	-2.24	102.91	--	--	52	52	Si	3.5
531.36	--	16.76	10.05	6.03	--	--	-1.33	39.95	52	52	Si	8.4
590.40	--	42.96	10.05	6.03	--	--	-3.41	102.41	52	52	Si	3.3

Trave: 207 [205,206], Pilastrate [5,6] Sez. R: By=30.00 cm Bz=50.00 cm L=397.00 cm Ln=397.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	11.57	10.05	6.03	--	--	-0.92	27.58	45	30	Si	13
39.70	8.98	1.63	10.05	6.03	-0.76	34.79	-0.13	3.89	45	35	Si	10
198.50	40.48	--	10.05	6.03	-3.42	156.80	--	--	44	40	Si	2.3
357.30	36.79	12.63	10.05	6.03	-3.11	142.50	-1.00	30.12	45	30	Si	2.5
397.00	31.99	25.56	10.05	6.03	-2.70	123.92	-2.03	60.94	45	30	Si	2.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	10.69	10.05	6.03	--	--	-0.85	25.48	48	46	Si	13
39.70	--	1.43	10.05	6.03	--	--	-0.11	3.41	48	47	Si	99
198.50	12.31	--	10.05	6.03	-1.04	47.70	--	--	46	48	Si	7.5
357.30	--	11.49	10.05	6.03	--	--	-0.91	27.39	48	46	Si	12
397.00	--	23.30	10.05	6.03	--	--	-1.85	55.55	48	46	Si	6.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	10.39	10.05	6.03	--	--	-0.82	24.78	52	52	Si	14
39.70	--	1.38	10.05	6.03	--	--	-0.11	3.30	52	52	Si	>100
198.50	11.93	--	10.05	6.03	-1.01	46.23	--	--	52	52	Si	7.8
357.30	--	11.11	10.05	6.03	--	--	-0.88	26.48	52	52	Si	13
397.00	--	22.55	10.05	6.03	--	--	-1.79	53.76	52	52	Si	6.3

Trave: 208 [209,214], Pilastrate [9,14] Sez. R: By=30.00 cm Bz=50.00 cm L=329.87 cm Ln=329.87 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	47.83	10.05	6.03	--	--	-3.79	114.04	40	44	Si	3.2
32.99	--	29.98	10.05	6.03	--	--	-2.38	71.48	40	26	Si	5.0
164.93	25.63	--	10.05	6.03	-2.16	99.28	--	--	44	40	Si	3.6
296.88	52.50	--	10.05	6.03	-4.43	203.34	--	--	44	40	Si	1.8
329.87	54.98	--	10.05	6.03	-4.64	212.96	--	--	44	40	Si	1.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	35.43	10.05	6.03	--	--	-2.81	84.46	48	46	Si	4.0
32.99	--	23.75	10.05	6.03	--	--	-1.88	56.61	48	46	Si	6.0
164.93	6.11	--	10.05	6.03	-0.52	23.67	--	--	46	48	Si	15
296.88	8.22	--	10.05	6.03	-0.69	31.84	--	--	46	47	Si	11
329.87	4.62	--	10.05	6.03	-0.39	17.88	--	--	46	47	Si	20

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	34.11	10.05	6.03	--	--	-2.71	81.32	52	52	Si	4.1
32.99	--	22.89	10.05	6.03	--	--	-1.82	54.58	52	52	Si	6.2
164.93	5.84	--	10.05	6.03	-0.49	22.61	--	--	52	52	Si	16
296.88	7.98	--	10.05	6.03	-0.67	30.92	--	--	52	52	Si	12
329.87	4.56	--	10.05	6.03	-0.39	17.66	--	--	52	52	Si	20

Trave: 208 [214,217], Pilastrate [14,17] Sez. R: By=30.00 cm Bz=50.00 cm L=532.52 cm Ln=532.52 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	71.96	10.05	6.03	--	--	-5.71	171.56	45	30	Si	2.1
53.25	--	35.08	10.05	6.03	--	--	-2.78	83.64	45	30	Si	4.3
266.26	64.76	--	10.05	6.03	-5.47	250.86	--	--	44	40	Si	1.4
479.27	39.84	10.90	10.05	6.03	-3.36	154.32	-0.86	25.97	45	30	Si	2.3
532.52	26.53	39.70	10.05	6.03	-2.24	102.74	-3.15	94.64	45	30	Si	3.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	63.71	10.05	6.03	--	--	-5.05	151.88	48	46	Si	2.2
53.25	--	31.23	10.05	6.03	--	--	-2.48	74.44	48	46	Si	4.5
266.26	33.60	--	10.05	6.03	-2.84	130.15	--	--	46	48	Si	2.8
479.27	--	9.35	10.05	6.03	--	--	-0.74	22.28	48	46	Si	15
532.52	--	34.65	10.05	6.03	--	--	-2.75	82.61	48	46	Si	4.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	60.96	10.05	6.03	--	--	-4.83	145.32	52	52	Si	2.3
53.25	--	29.94	10.05	6.03	--	--	-2.37	71.38	52	52	Si	4.7

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
266.26	32.06	--	10.05	6.03	-2.71	124.19	--	--	52	52	Si	2.9
479.27	--	8.83	10.05	6.03	--	--	-0.70	21.05	52	52	Si	16
532.52	--	32.97	10.05	6.03	--	--	-2.61	78.60	52	52	Si	4.3

Trave: 209 [204,209], Pilastrate [4,9] Sez. R: By=30.00 cm Bz=50.00 cm L=322.79 cm Ln=322.79 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	38.51	--	10.05	6.03	-3.25	149.15	--	--	44	40	Si	2.4
32.28	41.70	--	10.05	6.03	-3.52	161.53	--	--	44	40	Si	2.2
161.40	38.47	--	10.05	6.03	-3.25	149.01	--	--	44	40	Si	2.4
290.51	9.99	10.24	10.05	6.03	-0.84	38.71	-0.81	24.41	45	30	Si	9.3
322.79	0.79	22.43	10.05	6.03	-0.07	3.05	-1.78	53.47	45	30	Si	6.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	13.58	--	10.05	6.03	-1.15	52.59	--	--	46	48	Si	6.8
32.28	17.47	--	10.05	6.03	-1.48	67.67	--	--	46	48	Si	5.3
161.40	17.33	--	10.05	6.03	-1.46	67.14	--	--	46	48	Si	5.4
290.51	--	9.46	10.05	6.03	--	--	-0.75	22.56	48	46	Si	15
322.79	--	20.53	10.05	6.03	--	--	-1.63	48.94	48	46	Si	6.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	13.00	--	10.05	6.03	-1.10	50.36	--	--	52	52	Si	7.1
32.28	16.78	--	10.05	6.03	-1.42	64.99	--	--	52	52	Si	5.5
161.40	16.68	--	10.05	6.03	-1.41	64.59	--	--	52	52	Si	5.6
290.51	--	9.21	10.05	6.03	--	--	-0.73	21.95	52	52	Si	15
322.79	--	19.89	10.05	6.03	--	--	-1.58	47.43	52	52	Si	7.1

Trave: 209 [209,213], Pilastrate [9,13] Sez. R: By=30.00 cm Bz=50.00 cm L=310.56 cm Ln=310.56 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	34.99	22.35	10.05	6.03	-2.95	135.51	-1.77	53.27	45	30	Si	2.7
31.06	34.35	14.92	10.05	6.03	-2.90	133.06	-1.18	35.58	45	30	Si	2.7
155.28	20.82	0.59	10.05	6.03	-1.76	80.64	-0.05	1.41	45	30	Si	4.5
279.51	--	12.94	10.05	6.03	--	--	-1.03	30.86	40	44	Si	12
310.56	--	24.90	10.05	6.03	--	--	-1.97	59.36	40	44	Si	6.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.32	10.05	6.03	--	--	-1.61	48.44	48	46	Si	7.0
31.06	--	13.54	10.05	6.03	--	--	-1.07	32.29	48	46	Si	10
155.28	--	0.50	10.05	6.03	--	--	-0.04	1.18	48	46	Si	>100
279.51	--	10.31	10.05	6.03	--	--	-0.82	24.57	48	46	Si	14
310.56	--	16.27	10.05	6.03	--	--	-1.29	38.79	48	46	Si	8.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	19.64	10.05	6.03	--	--	-1.56	46.82	52	52	Si	7.2
31.06	--	13.08	10.05	6.03	--	--	-1.04	31.19	52	52	Si	11
155.28	--	0.46	10.05	6.03	--	--	-0.04	1.11	52	52	Si	>100
279.51	--	10.00	10.05	6.03	--	--	-0.79	23.83	52	52	Si	14
310.56	--	15.78	10.05	6.03	--	--	-1.25	37.62	52	52	Si	9.0

Trave: 210 [214,216], Pilastrate [14,16] Sez. R: By=60.00 cm Bz=25.00 cm L=310.00 cm Ln=310.00 cm
Criterio: Travi spessore

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	17.83	13.91	8.04	8.04	-3.16	109.90	-2.47	85.70	45	30	Si	3.3
31.00	18.78	8.71	8.04	8.04	-3.33	115.75	-1.54	53.69	45	30	Si	3.1
155.00	16.12	--	8.04	8.04	-2.86	99.37	--	--	44	40	Si	3.6
279.00	1.26	3.48	8.04	8.04	-0.22	7.76	-0.62	21.45	45	30	Si	17
310.00	--	7.37	8.04	8.04	--	--	-1.31	45.42	45	30	Si	7.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	12.45	8.04	8.04	--	--	-2.21	76.72	48	46	Si	4.7
31.00	--	7.75	8.04	8.04	--	--	-1.37	47.78	48	46	Si	7.5
155.00	2.13	--	8.04	8.04	-0.38	13.15	--	--	46	48	Si	27
279.00	--	3.15	8.04	8.04	--	--	-0.56	19.44	48	46	Si	19
310.00	--	6.70	8.04	8.04	--	--	-1.19	41.29	48	46	Si	8.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	11.96	8.04	8.04	--	--	-2.12	73.73	52	52	Si	4.9
31.00	--	7.43	8.04	8.04	--	--	-1.32	45.82	52	52	Si	7.9
155.00	2.09	--	8.04	8.04	-0.37	12.90	--	--	52	52	Si	28
279.00	--	3.04	8.04	8.04	--	--	-0.54	18.76	52	52	Si	19
310.00	--	6.48	8.04	8.04	--	--	-1.15	39.91	52	52	Si	9.0

Verifica formazione fessure: σcta[MPa]=2.15

X	M+	M-	Afsup	Afinf	σc+	σct+	σc-	σct-	Cb+	Cb-.	Ver.	Cs
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	17.83	13.91	8.04	8.04	-2.44	1.62	-1.90	1.26	45	30	Si	1.3
31.00	18.78	8.71	8.04	8.04	-2.57	1.70	-1.19	0.79	45	30	Si	1.3
155.00	16.12	--	8.04	8.04	-2.20	1.46	--	--	44	40	Si	1.5
279.00	1.26	3.48	8.04	8.04	-0.17	0.11	-0.48	0.32	45	30	Si	6.8
310.00	--	7.37	8.04	8.04	--	--	-1.01	0.67	45	30	Si	3.2

Trave: 211 [204,214], Pilastrate [4,14] Sez. R: By=30.00 cm Bz=50.00 cm L=461.53 cm Ln=503.95 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	51.40	10.05	6.03	--	--	-4.08	122.54	40	26	Si	2.9
50.40	--	18.16	10.05	6.03	--	--	-1.44	43.28	40	26	Si	8.3
251.98	48.49	--	10.05	6.03	-4.10	187.83	--	--	44	40	Si	1.9
453.56	12.91	22.03	10.05	6.03	-1.09	50.02	-1.75	52.52	45	30	Si	6.9
503.95	--	53.96	10.05	6.03	--	--	-4.28	128.64	45	30	Si	2.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	41.69	10.05	6.03	--	--	-3.31	99.39	48	46	Si	3.4
50.40	--	15.00	10.05	6.03	--	--	-1.19	35.76	48	46	Si	9.4
251.98	34.73	--	10.05	6.03	-2.93	134.53	--	--	46	48	Si	2.7
453.56	--	19.59	10.05	6.03	--	--	-1.55	46.69	48	46	Si	7.2
503.95	--	47.69	10.05	6.03	--	--	-3.78	113.68	48	46	Si	3.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	39.77	10.05	6.03	--	--	-3.15	94.81	52	52	Si	3.6
50.40	--	14.32	10.05	6.03	--	--	-1.14	34.13	52	52	Si	9.9
251.98	33.08	--	10.05	6.03	-2.79	128.15	--	--	52	52	Si	2.8
453.56	--	18.77	10.05	6.03	--	--	-1.49	44.75	52	52	Si	7.5
503.95	--	45.59	10.05	6.03	--	--	-3.62	108.70	52	52	Si	3.1

Trave: 212 [205,210], Pilastrate [5,10] Sez. R: By=30.00 cm Bz=50.00 cm L=378.19 cm Ln=379.38 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	25.14	10.05	6.03	--	--	-1.99	59.93	40	44	Si	6.0
37.94	0.91	2.15	10.05	6.03	-0.08	3.51	-0.17	5.13	40	44	Si	70
189.69	42.41	--	10.05	6.03	-3.58	164.26	--	--	44	40	Si	2.2
341.44	17.87	43.02	10.05	6.03	-1.51	69.23	-3.41	102.56	45	30	Si	3.5
379.38	5.77	73.27	10.05	6.03	-0.49	22.36	-5.81	174.68	45	30	Si	2.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	16.55	10.05	6.03	--	--	-1.31	39.46	48	46	Si	8.5
37.94	0.15	--	10.05	6.03	-0.01	0.60	--	--	47	46	Si	>100
189.69	20.24	--	10.05	6.03	-1.71	78.41	--	--	46	48	Si	4.6
341.44	--	38.37	10.05	6.03	--	--	-3.04	91.47	48	46	Si	3.7
379.38	--	64.96	10.05	6.03	--	--	-5.15	154.85	48	46	Si	2.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	15.57	10.05	6.03	--	--	-1.23	37.12	52	52	Si	9.1
37.94	0.14	--	10.05	6.03	-0.01	0.54	--	--	52	52	Si	>100
189.69	19.21	--	10.05	6.03	-1.62	74.41	--	--	52	52	Si	4.8
341.44	--	36.82	10.05	6.03	--	--	-2.92	87.77	52	52	Si	3.8
379.38	--	62.18	10.05	6.03	--	--	-4.93	148.25	52	52	Si	2.3

Trave: 212 [210,218], Pilastrate [10,18] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	57.87	10.05	6.03	--	--	-4.59	137.96	45	30	Si	2.6
46.99	--	20.18	10.05	6.03	--	--	-1.60	48.10	45	30	Si	7.5
234.95	65.70	--	10.05	6.03	-5.55	254.48	--	--	44	40	Si	1.4
422.91	31.09	11.97	10.05	6.03	-2.63	120.44	-0.95	28.53	45	30	Si	3.0
469.90	16.79	42.18	10.05	6.03	-1.42	65.03	-3.35	100.55	45	30	Si	3.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	51.43	10.05	6.03	--	--	-4.08	122.60	48	46	Si	2.7
46.99	--	18.31	10.05	6.03	--	--	-1.45	43.64	48	46	Si	7.7
234.95	39.60	--	10.05	6.03	-3.34	153.38	--	--	46	48	Si	2.3
422.91	--	10.23	10.05	6.03	--	--	-0.81	24.39	48	46	Si	14
469.90	--	36.60	10.05	6.03	--	--	-2.90	87.25	48	46	Si	3.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	49.28	10.05	6.03	--	--	-3.91	117.49	52	52	Si	2.9
46.99	--	17.68	10.05	6.03	--	--	-1.40	42.15	52	52	Si	8.0

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
234.95	37.67	--	10.05	6.03	-3.18	145.90	--	--	52	52	Si	2.5
422.91	--	9.65	10.05	6.03	--	--	-0.77	23.01	52	52	Si	15
469.90	--	34.74	10.05	6.03	--	--	-2.75	82.82	52	52	Si	4.1

Trave: 213 [206,211], Pilastrate [6,11] Sez. R: By=30.00 cm Bz=50.00 cm L=377.00 cm Ln=347.00 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	7.37	10.05	6.03	--	--	-0.58	17.58	40	44	Si	20
34.70	7.49	--	10.05	6.03	-0.63	28.99	--	--	26	40	Si	12
173.50	32.25	--	10.05	6.03	-2.72	124.93	--	--	44	40	Si	2.9
312.30	15.30	35.83	10.05	6.03	-1.29	59.25	-2.84	85.43	45	30	Si	4.2
347.00	6.75	56.65	10.05	6.03	-0.57	26.13	-4.49	135.06	45	30	Si	2.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	2.49	10.05	6.03	--	--	-0.20	5.93	48	46	Si	57
34.70	6.61	--	10.05	6.03	-0.56	25.62	--	--	46	48	Si	14
173.50	12.17	--	10.05	6.03	-1.03	47.13	--	--	46	48	Si	7.6
312.30	--	32.34	10.05	6.03	--	--	-2.56	77.09	48	46	Si	4.4
347.00	--	50.95	10.05	6.03	--	--	-4.04	121.47	48	46	Si	2.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	2.31	10.05	6.03	--	--	-0.18	5.50	52	52	Si	61
34.70	6.40	--	10.05	6.03	-0.54	24.78	--	--	52	52	Si	15
173.50	11.63	--	10.05	6.03	-0.98	45.05	--	--	52	52	Si	8.0
312.30	--	31.17	10.05	6.03	--	--	-2.47	74.31	52	52	Si	4.5
347.00	--	49.05	10.05	6.03	--	--	-3.89	116.94	52	52	Si	2.9

Trave: 213 [211,219], Pilastrate [11,19] Sez. R: By=30.00 cm Bz=50.00 cm L=469.90 cm Ln=469.90 cm
Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	45.83	10.05	6.03	--	--	-3.63	109.25	45	30	Si	3.3
46.99	7.16	15.77	10.05	6.03	-0.60	27.74	-1.25	37.60	45	30	Si	9.6
234.95	62.61	--	10.05	6.03	-5.29	242.51	--	--	44	40	Si	1.5
422.91	29.40	6.94	10.05	6.03	-2.48	113.87	-0.55	16.53	45	30	Si	3.2
469.90	13.95	34.42	10.05	6.03	-1.18	54.02	-2.73	82.07	45	30	Si	4.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	41.24	10.05	6.03	--	--	-3.27	98.31	48	46	Si	3.4
46.99	--	14.39	10.05	6.03	--	--	-1.14	34.31	48	46	Si	9.8
234.95	35.61	--	10.05	6.03	-3.01	137.93	--	--	46	48	Si	2.6
422.91	--	6.19	10.05	6.03	--	--	-0.49	14.75	48	46	Si	23
469.90	--	30.64	10.05	6.03	--	--	-2.43	73.06	48	46	Si	4.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	39.71	10.05	6.03	--	--	-3.15	94.66	52	52	Si	3.6
46.99	--	13.93	10.05	6.03	--	--	-1.11	33.22	52	52	Si	10
234.95	34.11	--	10.05	6.03	-2.88	132.11	--	--	52	52	Si	2.7
422.91	--	5.94	10.05	6.03	--	--	-0.47	14.15	52	52	Si	24
469.90	--	29.38	10.05	6.03	--	--	-2.33	70.05	52	52	Si	4.8

Trave: 214 [210,211], Pilastrate [10,11] Sez. R: By=30.00 cm Bz=50.00 cm L=427.00 cm Ln=427.00 cm Criterio: Travi alte

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	8.27	10.05	6.03	--	--	-0.66	19.72	40	44	Si	18
42.70	3.52	--	10.05	6.03	-0.30	13.64	--	--	26	40	Si	26
213.50	31.20	--	10.05	6.03	-2.63	120.83	--	--	44	40	Si	3.0
384.30	33.90	16.25	10.05	6.03	-2.86	131.33	-1.29	38.75	45	30	Si	2.7
427.00	31.67	27.60	10.05	6.03	-2.67	122.66	-2.19	65.79	45	30	Si	2.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	2.72	10.05	6.03	--	--	-0.22	6.48	48	47	Si	52
42.70	3.02	--	10.05	6.03	-0.25	11.69	--	--	46	48	Si	31
213.50	8.55	--	10.05	6.03	-0.72	33.13	--	--	46	48	Si	11
384.30	--	14.63	10.05	6.03	--	--	-1.16	34.88	48	46	Si	9.7
427.00	--	24.91	10.05	6.03	--	--	-1.98	59.39	48	46	Si	5.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	2.66	10.05	6.03	--	--	-0.21	6.35	52	52	Si	53
42.70	2.88	--	10.05	6.03	-0.24	11.15	--	--	52	52	Si	32
213.50	8.28	--	10.05	6.03	-0.70	32.07	--	--	52	52	Si	11
384.30	--	14.09	10.05	6.03	--	--	-1.12	33.58	52	52	Si	10
427.00	--	24.02	10.05	6.03	--	--	-1.90	57.26	52	52	Si	5.9

Trave: 8000 [37,38], Pilastrate [14,--] Sez. R: By=30.00 cm Bz=50.00 cm L=405.25 cm Ln=405.25 cm L2=405.25 cm L3=405.25 cm Criterio: Travi alte

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	68.54	2116.50	0.032	46.794	138.920

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	45	35	Si	>100
40.53	13.34	--	10.05	6.03	-1.13	51.66	--	--	26	40	Si	7.0
202.63	43.52	--	10.05	6.03	-3.68	168.57	--	--	26	40	Si	2.1
364.73	36.64	--	10.05	6.03	-3.09	141.90	--	--	26	40	Si	2.5
405.25	29.12	--	10.05	6.03	-2.46	112.81	--	--	26	40	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	48	46	Si	>100
40.53	11.50	--	10.05	6.03	-0.97	44.55	--	--	46	47	Si	8.1
202.63	36.96	--	10.05	6.03	-3.12	143.15	--	--	46	47	Si	2.5
364.73	29.55	--	10.05	6.03	-2.50	114.45	--	--	46	47	Si	3.1
405.25	22.56	--	10.05	6.03	-1.91	87.38	--	--	46	47	Si	4.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	52	52	Si	>100
40.53	11.01	--	10.05	6.03	-0.93	42.64	--	--	52	52	Si	8.4
202.63	35.37	--	10.05	6.03	-2.99	137.00	--	--	52	52	Si	2.6
364.73	28.26	--	10.05	6.03	-2.39	109.47	--	--	52	52	Si	3.3
405.25	21.57	--	10.05	6.03	-1.82	83.53	--	--	52	52	Si	4.3

Trave: 8000 [38,35], Pilastrate [--,17] Sez. R: By=30.00 cm Bz=50.00 cm L=173.00 cm Ln=173.00 cm L2=173.00 cm L3=173.00 cm Criterio: Travi alte
Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	44.70	2116.50	0.021	19.976	172.018

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	30.69	--	10.05	6.03	-2.59	118.89	--	--	26	40	Si	3.0
17.30	29.76	--	10.05	6.03	-2.51	115.29	--	--	26	40	Si	3.1
86.50	21.29	--	10.05	6.03	-1.80	82.48	--	--	26	40	Si	4.4
155.70	5.21	--	10.05	6.03	-0.44	20.18	--	--	26	40	Si	18
173.00	0.00	0.00	10.05	6.03	-0.00	0.00	-0.00	0.00	35	45	Si	>100

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	23.87	--	10.05	6.03	-2.02	92.44	--	--	46	47	Si	3.9
17.30	23.38	--	10.05	6.03	-1.97	90.55	--	--	46	47	Si	4.0
86.50	17.21	--	10.05	6.03	-1.45	66.65	--	--	46	47	Si	5.4
155.70	4.29	--	10.05	6.03	-0.36	16.60	--	--	46	47	Si	22
173.00	0.00	0.00	10.05	6.03	-0.00	0.00	-0.00	0.00	46	48	Si	>100

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	22.82	--	10.05	6.03	-1.93	88.38	--	--	52	52	Si	4.1
17.30	22.35	--	10.05	6.03	-1.89	86.59	--	--	52	52	Si	4.2
86.50	16.46	--	10.05	6.03	-1.39	63.75	--	--	52	52	Si	5.6
155.70	4.10	--	10.05	6.03	-0.35	15.88	--	--	52	52	Si	23
173.00	--	0.00	10.05	6.03	--	--	-0.00	0.00	52	52	Si	>100

Trave di fondazione: 9001 [2,3], Pilastrate [2,3] Sez. R: By=50.00 cm Bz=100.00 cm L=514.30 cm Ln=514.30 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	212.03	--	12.72	12.72	-3.48	185.84	--	--	44	40	Si	1.9
51.43	162.56	--	12.72	12.72	-2.66	142.48	--	--	44	40	Si	2.5
257.15	57.67	64.05	12.72	12.72	-0.95	50.54	-1.05	56.13	45	30	Si	6.4
462.87	64.41	40.10	12.72	12.72	-1.06	56.45	-0.66	35.15	45	30	Si	6.4
514.30	83.70	15.27	12.72	12.72	-1.37	73.36	-0.25	13.38	45	30	Si	4.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	53.49	--	12.72	12.72	-0.88	46.88	--	--	46	48	Si	7.7
51.43	18.89	--	12.72	12.72	-0.31	16.56	--	--	46	48	Si	22
257.15	--	59.40	12.72	12.72	--	--	-0.97	52.07	48	46	Si	6.9
462.87	--	37.05	12.72	12.72	--	--	-0.61	32.48	48	46	Si	11
514.30	--	13.96	12.72	12.72	--	--	-0.23	12.23	47	46	Si	29

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	52.20	--	12.72	12.72	-0.86	45.75	--	--	52	52	Si	7.9
51.43	18.47	--	12.72	12.72	-0.30	16.19	--	--	52	52	Si	22
257.15	--	57.86	12.72	12.72	--	--	-0.95	50.71	52	52	Si	7.1
462.87	--	36.04	12.72	12.72	--	--	-0.59	31.59	52	52	Si	11
514.30	--	13.52	12.72	12.72	--	--	-0.22	11.85	52	52	Si	30

Trave di fondazione: 9001 [3,4], Pilastrate [3,4] Sez. R: By=50.00 cm Bz=100.00 cm L=463.50 cm Ln=463.50 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	140.63	15.51	12.72	12.72	-2.31	123.26	-0.25	13.59	44	40	Si	2.9
46.35	122.36	29.33	12.72	12.72	-2.01	107.24	-0.48	25.70	45	30	Si	3.4
231.75	100.22	33.27	12.72	12.72	-1.64	87.84	-0.55	29.16	45	30	Si	4.1
417.15	181.99	--	12.72	12.72	-2.98	159.51	--	--	44	40	Si	2.3
463.50	225.82	--	12.72	12.72	-3.70	197.92	--	--	44	40	Si	1.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	14.97	12.72	12.72	--	--	-0.25	13.12	47	48	Si	27
46.35	--	27.83	12.72	12.72	--	--	-0.46	24.39	48	46	Si	15
231.75	--	30.15	12.72	12.72	--	--	-0.49	26.43	48	46	Si	14
417.15	65.21	--	12.72	12.72	-1.07	57.15	--	--	46	48	Si	6.3
463.50	107.56	--	12.72	12.72	-1.76	94.27	--	--	46	48	Si	3.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	14.97	12.72	12.72	--	--	-0.25	13.12	52	52	Si	27
46.35	--	27.33	12.72	12.72	--	--	-0.45	23.95	52	52	Si	15
231.75	--	29.12	12.72	12.72	--	--	-0.48	25.52	52	52	Si	14
417.15	63.35	--	12.72	12.72	-1.04	55.52	--	--	52	52	Si	6.5
463.50	104.34	--	12.72	12.72	-1.71	91.45	--	--	52	52	Si	3.9

Trave di fondazione: 9001 [4,5], Pilastrate [4,5] Sez. R: By=50.00 cm Bz=100.00 cm L=590.40 cm Ln=590.40 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	332.19	--	12.72	15.27	-5.10	244.06	--	--	44	40	Si	1.5
59.04	258.01	--	12.72	15.27	-3.96	189.56	--	--	44	40	Si	1.9
295.20	127.09	10.40	12.72	15.27	-1.95	93.37	-0.17	9.09	45	30	Si	3.9
531.36	260.38	--	12.72	15.27	-4.00	191.30	--	--	44	40	Si	1.9
590.40	338.57	--	12.72	15.27	-5.20	248.75	--	--	44	40	Si	1.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	166.23	--	12.72	15.27	-2.55	122.13	--	--	46	48	Si	2.9
59.04	102.86	--	12.72	15.27	-1.58	75.57	--	--	46	48	Si	4.8
295.20	--	9.05	12.72	15.27	--	--	-0.14	7.92	48	46	Si	45
531.36	118.24	--	12.72	15.27	-1.82	86.87	--	--	46	48	Si	4.1
590.40	189.37	--	12.72	15.27	-2.91	139.13	--	--	46	48	Si	2.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	160.95	--	12.72	15.27	-2.47	118.25	--	--	52	52	Si	3.0
59.04	99.67	--	12.72	15.27	-1.53	73.23	--	--	52	52	Si	4.9
295.20	--	8.61	12.72	15.27	--	--	-0.14	7.52	52	52	Si	48
531.36	114.40	--	12.72	15.27	-1.76	84.05	--	--	52	52	Si	4.3
590.40	183.16	--	12.72	15.27	-2.81	134.57	--	--	52	52	Si	2.7

Trave di fondazione: 9001 [5,6], Pilastrate [5,6] Sez. R: By=50.00 cm Bz=100.00 cm L=397.00 cm Ln=397.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	270.99	--	12.72	15.27	-4.16	199.09	--	--	44	40	Si	1.8
39.70	223.61	--	12.72	15.27	-3.43	164.29	--	--	44	40	Si	2.2
198.50	112.86	9.18	12.72	15.27	-1.73	82.92	-0.15	8.03	45	30	Si	4.3
357.30	110.91	--	12.72	15.27	-1.70	81.48	--	--	44	40	Si	4.4
397.00	127.36	--	12.72	15.27	-1.96	93.57	--	--	44	40	Si	3.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	110.96	--	12.72	15.27	-1.70	81.52	--	--	46	48	Si	4.4
39.70	73.20	--	12.72	15.27	-1.12	53.78	--	--	46	48	Si	6.7
198.50	--	8.36	12.72	15.27	--	--	-0.13	7.31	48	46	Si	49
357.30	14.38	--	12.72	15.27	-0.22	10.56	--	--	46	48	Si	34
397.00	35.34	--	12.72	15.27	-0.54	25.96	--	--	46	48	Si	14

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	107.19	--	12.72	15.27	-1.65	78.75	--	--	52	52	Si	4.6
39.70	70.70	--	12.72	15.27	-1.09	51.94	--	--	52	52	Si	6.9
198.50	--	8.08	12.72	15.27	--	--	-0.13	7.07	52	52	Si	51
357.30	13.98	--	12.72	15.27	-0.21	10.27	--	--	52	52	Si	35
397.00	34.27	--	12.72	15.27	-0.53	25.18	--	--	52	52	Si	14

Trave di fondazione: 9001 [6,7], Pilastrate [6,7] Sez. R: By=50.00 cm Bz=100.00 cm L=530.00 cm Ln=530.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	233.72	--	10.18	10.18	-4.29	255.02	--	--	44	40	Si	1.4
53.00	167.76	--	10.18	10.18	-3.08	183.04	--	--	44	40	Si	2.0
265.00	19.37	55.61	10.18	10.18	-0.36	21.14	-1.02	60.68	45	30	Si	5.9
477.00	1.07	26.05	10.18	10.18	-0.02	1.17	-0.48	28.43	45	30	Si	13
530.00	17.05	--	10.18	10.18	-0.31	18.61	--	--	44	40	Si	19

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	104.17	--	10.18	10.18	-1.91	113.66	--	--	46	48	Si	3.2
53.00	54.20	--	10.18	10.18	-1.00	59.14	--	--	46	48	Si	6.1
265.00	--	50.53	10.18	10.18	--	--	-0.93	55.14	48	46	Si	6.5
477.00	--	23.88	10.18	10.18	--	--	-0.44	26.06	48	46	Si	14
530.00	1.08	--	10.18	10.18	-0.02	1.18	--	--	47	48	Si	>100

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	100.83	--	10.18	10.18	-1.85	110.02	--	--	52	52	Si	3.3
53.00	52.50	--	10.18	10.18	-0.96	57.28	--	--	52	52	Si	6.3
265.00	--	48.84	10.18	10.18	--	--	-0.90	53.29	52	52	Si	6.8
477.00	--	23.16	10.18	10.18	--	--	-0.43	25.27	52	52	Si	14
530.00	0.90	--	10.18	10.18	-0.02	0.98	--	--	52	52	Si	>100

Trave di fondazione: 9002 [10,11], Pilastrate [10,11] Sez. R: By=50.00 cm Bz=100.00 cm L=427.00 cm Ln=427.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	91.19	--	10.18	10.18	-1.67	99.49	--	--	44	40	Si	3.6

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
42.70	60.99	--	10.18	10.18	-1.12	66.55	--	--	44	40	Si	5.4
213.50	39.27	60.58	10.18	10.18	-0.72	42.85	-1.11	66.10	45	30	Si	5.4
384.30	114.85	--	10.18	10.18	-2.11	125.32	--	--	44	40	Si	2.9
427.00	154.23	--	10.18	10.18	-2.83	168.28	--	--	44	40	Si	2.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	42.13	--	10.18	10.18	-0.77	45.97	--	--	46	48	Si	7.8
42.70	3.86	--	10.18	10.18	-0.07	4.21	--	--	46	47	Si	86
213.50	--	55.55	10.18	10.18	--	--	-1.02	60.62	48	46	Si	5.9
384.30	23.68	--	10.18	10.18	-0.43	25.83	--	--	46	48	Si	14
427.00	63.88	--	10.18	10.18	-1.17	69.70	--	--	46	48	Si	5.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	40.68	--	10.18	10.18	-0.75	44.38	--	--	52	52	Si	8.1
42.70	3.61	--	10.18	10.18	-0.07	3.94	--	--	52	52	Si	91
213.50	--	53.88	10.18	10.18	--	--	-0.99	58.79	52	52	Si	6.1
384.30	23.02	--	10.18	10.18	-0.42	25.11	--	--	52	52	Si	14
427.00	62.02	--	10.18	10.18	-1.14	67.67	--	--	52	52	Si	5.3

Trave di fondazione: 9002 [11,12], Pilastrate [11,12] Sez. R: By=50.00 cm Bz=100.00 cm L=530.00 cm Ln=530.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	248.36	--	10.18	10.18	-4.56	270.99	--	--	44	40	Si	1.3
53.00	182.37	--	10.18	10.18	-3.35	198.99	--	--	44	40	Si	1.8
265.00	25.75	63.31	10.18	10.18	-0.47	28.10	-1.16	69.08	45	30	Si	5.2
477.00	--	32.31	10.18	10.18	--	--	-0.59	35.25	45	30	Si	10
530.00	1.29	7.31	10.18	10.18	-0.02	1.41	-0.13	7.97	40	44	Si	45

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	130.45	--	10.18	10.18	-2.40	142.33	--	--	46	48	Si	2.5
53.00	70.32	--	10.18	10.18	-1.29	76.72	--	--	46	48	Si	4.7
265.00	--	58.16	10.18	10.18	--	--	-1.07	63.46	48	46	Si	5.7
477.00	--	29.34	10.18	10.18	--	--	-0.54	32.02	48	46	Si	11
530.00	0.34	--	10.18	10.18	-0.01	0.37	--	--	47	46	Si	>100

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	126.46	--	10.18	10.18	-2.32	137.98	--	--	52	52	Si	2.6
53.00	68.14	--	10.18	10.18	-1.25	74.34	--	--	52	52	Si	4.8
265.00	--	56.44	10.18	10.18	--	--	-1.04	61.59	52	52	Si	5.8
477.00	--	28.36	10.18	10.18	--	--	-0.52	30.94	52	52	Si	12
530.00	0.30	--	10.18	10.18	-0.01	0.33	--	--	52	52	Si	>100

Trave di fondazione: 9003 [17,18], Pilastrate [17,18] Sez. R: By=50.00 cm Bz=100.00 cm L=179.02 cm Ln=179.30 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	288.93	--	12.72	15.27	-4.44	212.27	--	--	44	40	Si	1.7
17.93	274.98	--	12.72	15.27	-4.22	202.02	--	--	44	40	Si	1.8
89.65	234.89	--	12.72	15.27	-3.61	172.57	--	--	44	40	Si	2.1
161.37	219.64	--	12.72	15.27	-3.37	161.37	--	--	44	40	Si	2.2

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
179.30	219.64	--	12.72	15.27	-3.37	161.37	--	--	44	40	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	122.92	--	12.72	15.27	-1.89	90.31	--	--	46	48	Si	4.0
17.93	110.17	--	12.72	15.27	-1.69	80.94	--	--	46	48	Si	4.4
89.65	74.69	--	12.72	15.27	-1.15	54.88	--	--	46	48	Si	6.6
161.37	63.78	--	12.72	15.27	-0.98	46.86	--	--	46	48	Si	7.7
179.30	64.83	--	12.72	15.27	-1.00	47.63	--	--	46	48	Si	7.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	119.95	--	12.72	15.27	-1.84	88.13	--	--	52	52	Si	4.1
17.93	107.54	--	12.72	15.27	-1.65	79.01	--	--	52	52	Si	4.6
89.65	72.91	--	12.72	15.27	-1.12	53.57	--	--	52	52	Si	6.7
161.37	62.05	--	12.72	15.27	-0.95	45.59	--	--	52	52	Si	7.9
179.30	62.99	--	12.72	15.27	-0.97	46.28	--	--	52	52	Si	7.8

Trave di fondazione: 9003 [18,19], Pilastrate [18,19] Sez. R: By=50.00 cm Bz=100.00 cm L=427.00 cm Ln=427.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	313.19	--	12.72	15.27	-4.81	230.10	--	--	44	40	Si	1.6
42.70	259.06	--	12.72	15.27	-3.98	190.33	--	--	44	40	Si	1.9
213.50	125.92	14.78	12.72	15.27	-1.93	92.51	-0.24	12.92	45	30	Si	3.9
384.30	92.09	5.29	12.72	15.27	-1.41	67.66	-0.08	4.62	44	40	Si	5.3
427.00	99.06	--	12.72	15.27	-1.52	72.78	--	--	44	40	Si	4.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	138.81	--	12.72	15.27	-2.13	101.99	--	--	46	48	Si	3.5
42.70	92.53	--	12.72	15.27	-1.42	67.98	--	--	46	48	Si	5.3
213.50	--	12.95	12.72	15.27	--	--	-0.21	11.32	48	46	Si	32
384.30	--	4.25	12.72	15.27	--	--	-0.07	3.72	47	48	Si	97
427.00	14.06	--	12.72	15.27	-0.22	10.33	--	--	46	48	Si	35

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	134.90	--	12.72	15.27	-2.07	99.11	--	--	52	52	Si	3.6
42.70	90.04	--	12.72	15.27	-1.38	66.15	--	--	52	52	Si	5.4
213.50	--	12.34	12.72	15.27	--	--	-0.20	10.78	52	52	Si	33
384.30	--	4.25	12.72	15.27	--	--	-0.07	3.72	52	52	Si	97
427.00	13.13	--	12.72	15.27	-0.20	9.65	--	--	52	52	Si	37

Trave di fondazione: 9003 [19,20], Pilastrate [19,20] Sez. R: By=50.00 cm Bz=100.00 cm L=530.00 cm Ln=530.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	195.11	--	10.18	10.18	-3.58	212.89	--	--	44	40	Si	1.7
53.00	135.45	--	10.18	10.18	-2.49	147.79	--	--	44	40	Si	2.4
265.00	3.64	79.30	10.18	10.18	-0.07	3.97	-1.46	86.52	45	30	Si	4.2
477.00	--	32.84	10.18	10.18	--	--	-0.60	35.83	45	30	Si	10
530.00	2.01	13.34	10.18	10.18	-0.04	2.19	-0.24	14.56	35	45	Si	25

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	84.24	--	10.18	10.18	-1.55	91.92	--	--	46	48	Si	3.9
53.00	31.46	--	10.18	10.18	-0.58	34.32	--	--	46	48	Si	10
265.00	--	73.49	10.18	10.18	--	--	-1.35	80.19	48	46	Si	4.5
477.00	--	30.30	10.18	10.18	--	--	-0.56	33.06	48	46	Si	11
530.00	1.74	--	10.18	10.18	-0.03	1.90	--	--	47	48	Si	>100

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	81.49	--	10.18	10.18	-1.50	88.92	--	--	52	52	Si	4.0
53.00	30.25	--	10.18	10.18	-0.56	33.00	--	--	52	52	Si	11
265.00	--	71.56	10.18	10.18	--	--	-1.31	78.08	52	52	Si	4.6
477.00	--	29.45	10.18	10.18	--	--	-0.54	32.13	52	52	Si	11
530.00	1.68	--	10.18	10.18	-0.03	1.84	--	--	52	52	Si	>100

Trave di fondazione: 9004 [27,28], Pilastrate [27,28] Sez. R: By=50.00 cm Bz=100.00 cm L=500.00 cm Ln=500.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	161.58	--	10.18	10.18	-2.97	176.30	--	--	44	40	Si	2.0
50.00	113.55	--	10.18	10.18	-2.09	123.90	--	--	44	40	Si	2.9
250.00	9.57	43.80	10.18	10.18	-0.18	10.44	-0.80	47.79	45	30	Si	7.5
450.00	6.15	2.21	10.18	10.18	-0.11	6.71	-0.04	2.41	44	40	Si	54
500.00	28.73	--	10.18	10.18	-0.53	31.35	--	--	26	40	Si	11

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	49.76	--	10.18	10.18	-0.91	54.29	--	--	46	48	Si	6.6
50.00	18.87	--	10.18	10.18	-0.35	20.59	--	--	46	48	Si	17
250.00	--	39.99	10.18	10.18	--	--	-0.73	43.63	48	46	Si	8.3
450.00	--	1.71	10.18	10.18	--	--	-0.03	1.87	46	48	Si	>100
500.00	22.79	--	10.18	10.18	-0.42	24.87	--	--	46	48	Si	14

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	48.22	--	10.18	10.18	-0.89	52.61	--	--	52	52	Si	6.8
50.00	18.31	--	10.18	10.18	-0.34	19.98	--	--	52	52	Si	18
250.00	--	38.71	10.18	10.18	--	--	-0.71	42.24	52	52	Si	8.5
450.00	--	1.71	10.18	10.18	--	--	-0.03	1.87	52	52	Si	>100
500.00	21.88	--	10.18	10.18	-0.40	23.87	--	--	52	52	Si	15

Trave di fondazione: 9005 [15,13], Pilastrate [15,13] Sez. R: By=50.00 cm Bz=100.00 cm L=531.07 cm Ln=578.55 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	44.65	--	10.18	10.18	-0.82	48.72	--	--	44	40	Si	7.4
57.85	25.70	31.62	10.18	10.18	-0.47	28.04	-0.58	34.50	45	30	Si	10
289.27	16.57	97.18	10.18	10.18	-0.30	18.08	-1.78	106.03	45	30	Si	3.4
520.69	106.50	2.72	10.18	10.18	-1.96	116.20	-0.05	2.96	45	30	Si	3.1
578.55	158.14	--	10.18	10.18	-2.90	172.55	--	--	44	40	Si	2.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	7.67	--	10.18	10.18	-0.14	8.37	--	--	46	48	Si	43

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
57.85	--	28.85	10.18	10.18	--	--	-0.53	31.48	48	46	Si	11
289.27	--	89.38	10.18	10.18	--	--	-1.64	97.52	48	46	Si	3.7
520.69	--	2.64	10.18	10.18	--	--	-0.05	2.89	47	46	Si	>100
578.55	46.21	--	10.18	10.18	-0.85	50.42	--	--	46	48	Si	7.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	7.56	--	10.18	10.18	-0.14	8.25	--	--	52	52	Si	44
57.85	--	27.93	10.18	10.18	--	--	-0.51	30.47	52	52	Si	12
289.27	--	86.78	10.18	10.18	--	--	-1.59	94.68	52	52	Si	3.8
520.69	--	2.62	10.18	10.18	--	--	-0.05	2.86	52	52	Si	>100
578.55	44.80	--	10.18	10.18	-0.82	48.88	--	--	52	52	Si	7.4

Trave di fondazione: 9006 [21,22], Pilastrate [21,22] Sez. R: By=50.00 cm Bz=100.00 cm L=574.50 cm Ln=574.50 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	43.39	2.25	10.18	10.18	-0.80	47.34	-0.04	2.46	45	30	Si	7.6
57.45	16.50	44.29	10.18	10.18	-0.30	18.01	-0.81	48.33	45	30	Si	7.4
287.25	--	114.72	10.18	10.18	--	--	-2.11	125.17	45	30	Si	2.9
517.05	21.77	12.68	10.18	10.18	-0.40	23.75	-0.23	13.84	45	30	Si	15
574.50	62.95	--	10.18	10.18	-1.16	68.68	--	--	44	40	Si	5.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	1.58	10.18	10.18	--	--	-0.03	1.72	48	46	Si	>100
57.45	--	40.18	10.18	10.18	--	--	-0.74	43.84	48	46	Si	8.2
287.25	--	104.90	10.18	10.18	--	--	-1.93	114.46	48	46	Si	3.1
517.05	--	11.65	10.18	10.18	--	--	-0.21	12.71	48	46	Si	28
574.50	41.53	--	10.18	10.18	-0.76	45.32	--	--	46	48	Si	7.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	1.36	10.18	10.18	--	--	-0.02	1.48	52	52	Si	>100
57.45	--	38.81	10.18	10.18	--	--	-0.71	42.34	52	52	Si	8.5
287.25	--	101.63	10.18	10.18	--	--	-1.87	110.89	52	52	Si	3.2
517.05	--	11.30	10.18	10.18	--	--	-0.21	12.33	52	52	Si	29
574.50	40.22	--	10.18	10.18	-0.74	43.88	--	--	52	52	Si	8.2

Trave di fondazione: 9007 [24,25], Pilastrate [24,25] Sez. R: By=50.00 cm Bz=100.00 cm L=544.50 cm Ln=544.50 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	34.41	5.97	10.18	10.18	-0.63	37.55	-0.11	6.51	45	30	Si	9.6
54.45	20.48	38.02	10.18	10.18	-0.38	22.34	-0.70	41.48	45	30	Si	8.7
272.25	27.54	73.77	10.18	10.18	-0.51	30.05	-1.35	80.49	45	30	Si	4.5
490.05	145.08	--	10.18	10.18	-2.66	158.29	--	--	44	40	Si	2.3
544.50	200.28	--	10.18	10.18	-3.68	218.52	--	--	44	40	Si	1.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	4.41	10.18	10.18	--	--	-0.08	4.81	48	46	Si	75
54.45	--	34.17	10.18	10.18	--	--	-0.63	37.28	48	46	Si	9.7
272.25	--	68.28	10.18	10.18	--	--	-1.25	74.50	48	46	Si	4.8
490.05	43.06	--	10.18	10.18	-0.79	46.99	--	--	46	48	Si	7.7

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
544.50	96.64	--	10.18	10.18	-1.77	105.44	--	--	46	48	Si	3.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	3.89	10.18	10.18	--	--	-0.07	4.24	52	52	Si	85
54.45	--	32.88	10.18	10.18	--	--	-0.60	35.88	52	52	Si	10
272.25	--	66.46	10.18	10.18	--	--	-1.22	72.51	52	52	Si	5.0
490.05	40.98	--	10.18	10.18	-0.75	44.71	--	--	52	52	Si	8.1
544.50	92.77	--	10.18	10.18	-1.70	101.22	--	--	52	52	Si	3.6

Trave di fondazione: 9007 [25,26], Pilastrate [25,26] Sez. R: By=50.00 cm Bz=100.00 cm L=604.50 cm Ln=604.50 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	282.66	--	10.18	12.72	-4.78	248.41	--	--	44	40	Si	1.4
60.45	199.83	--	10.18	12.72	-3.38	175.62	--	--	44	40	Si	2.0
302.25	13.44	100.85	10.18	12.72	-0.23	11.81	-1.79	109.78	45	30	Si	3.3
544.05	28.58	12.90	10.18	12.72	-0.48	25.12	-0.23	14.04	45	30	Si	14
604.50	74.29	--	10.18	12.72	-1.26	65.29	--	--	44	40	Si	5.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	145.76	--	10.18	12.72	-2.46	128.10	--	--	46	48	Si	2.8
60.45	69.13	--	10.18	12.72	-1.17	60.76	--	--	46	48	Si	5.9
302.25	--	94.14	10.18	12.72	--	--	-1.67	102.47	48	46	Si	3.5
544.05	--	10.88	10.18	12.72	--	--	-0.19	11.84	48	46	Si	30
604.50	54.18	--	10.18	12.72	-0.92	47.62	--	--	46	48	Si	7.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	139.98	--	10.18	12.72	-2.37	123.02	--	--	52	52	Si	2.9
60.45	65.83	--	10.18	12.72	-1.11	57.86	--	--	52	52	Si	6.2
302.25	--	91.91	10.18	12.72	--	--	-1.63	100.04	52	52	Si	3.6
544.05	--	10.20	10.18	12.72	--	--	-0.18	11.11	52	52	Si	32
604.50	53.27	--	10.18	12.72	-0.90	46.82	--	--	52	52	Si	7.7

Trave di fondazione: 9008 [29,30], Pilastrate [29,30] Sez. R: By=50.00 cm Bz=100.00 cm L=534.50 cm Ln=534.50 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	170.16	--	10.18	10.18	-3.12	185.66	--	--	44	40	Si	1.9
53.45	127.59	--	10.18	10.18	-2.34	139.21	--	--	44	40	Si	2.6
267.25	52.97	52.28	10.18	10.18	-0.97	57.79	-0.96	57.04	45	30	Si	6.2
481.05	69.62	16.51	10.18	10.18	-1.28	75.96	-0.30	18.02	44	40	Si	4.7
534.50	94.09	0.55	10.18	10.18	-1.73	102.66	-0.01	0.60	44	40	Si	3.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	47.17	--	10.18	10.18	-0.87	51.47	--	--	46	48	Si	7.0
53.45	15.80	--	10.18	10.18	-0.29	17.24	--	--	46	48	Si	21
267.25	--	47.44	10.18	10.18	--	--	-0.87	51.76	48	46	Si	7.0
481.05	--	15.53	10.18	10.18	--	--	-0.29	16.95	46	48	Si	21
534.50	7.85	--	10.18	10.18	-0.14	8.56	--	--	46	48	Si	42

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	45.90	--	10.18	10.18	-0.84	50.08	--	--	52	52	Si	7.2
53.45	15.56	--	10.18	10.18	-0.29	16.98	--	--	52	52	Si	21
267.25	--	45.83	10.18	10.18	--	--	-0.84	50.01	52	52	Si	7.2
481.05	--	15.53	10.18	10.18	--	--	-0.29	16.95	52	52	Si	21
534.50	6.65	--	10.18	10.18	-0.12	7.25	--	--	52	52	Si	50

Trave di fondazione: 9008 [30,31], Pilastrate [30,31] Sez. R: By=50.00 cm Bz=100.00 cm L=614.50 cm Ln=614.50 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	230.55	--	10.18	10.18	-4.23	251.55	--	--	44	40	Si	1.4
61.45	167.10	--	10.18	10.18	-3.07	182.33	--	--	44	40	Si	2.0
307.25	23.35	60.13	10.18	10.18	-0.43	25.48	-1.10	65.61	45	30	Si	5.5
553.05	30.14	--	10.18	10.18	-0.55	32.89	--	--	45	30	Si	11
614.50	68.61	--	10.18	10.18	-1.26	74.87	--	--	44	40	Si	4.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	77.35	--	10.18	10.18	-1.42	84.39	--	--	46	48	Si	4.3
61.45	33.53	--	10.18	10.18	-0.62	36.59	--	--	46	48	Si	9.8
307.25	--	55.14	10.18	10.18	--	--	-1.01	60.16	48	46	Si	6.0
553.05	4.81	--	10.18	10.18	-0.09	5.24	--	--	47	46	Si	69
614.50	46.27	--	10.18	10.18	-0.85	50.49	--	--	46	48	Si	7.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	73.42	--	10.18	10.18	-1.35	80.11	--	--	52	52	Si	4.5
61.45	31.39	--	10.18	10.18	-0.58	34.25	--	--	52	52	Si	11
307.25	--	53.47	10.18	10.18	--	--	-0.98	58.34	52	52	Si	6.2
553.05	4.80	--	10.18	10.18	-0.09	5.24	--	--	52	52	Si	69
614.50	45.09	--	10.18	10.18	-0.83	49.20	--	--	52	52	Si	7.3

Trave di fondazione: 9009 [2,15], Pilastrate [2,15] Sez. R: By=50.00 cm Bz=100.00 cm L=481.60 cm Ln=481.60 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	37.77	--	10.18	10.18	-0.69	41.21	--	--	44	40	Si	8.7
48.16	31.12	--	10.18	10.18	-0.57	33.95	--	--	45	35	Si	11
240.80	49.72	12.34	10.18	10.18	-0.91	54.25	-0.23	13.46	45	30	Si	6.6
433.44	127.46	--	10.18	10.18	-2.34	139.07	--	--	44	40	Si	2.6
481.60	157.66	--	10.18	10.18	-2.89	172.03	--	--	44	40	Si	2.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	11.87	--	10.18	10.18	-0.22	12.96	--	--	46	48	Si	28
48.16	1.03	--	10.18	10.18	-0.02	1.12	--	--	48	46	Si	>100
240.80	--	11.10	10.18	10.18	--	--	-0.20	12.11	48	46	Si	30
433.44	31.24	--	10.18	10.18	-0.57	34.08	--	--	46	48	Si	11
481.60	51.03	--	10.18	10.18	-0.94	55.68	--	--	46	48	Si	6.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	11.55	--	10.18	10.18	-0.21	12.61	--	--	52	52	Si	29

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
48.16	1.03	--	10.18	10.18	-0.02	1.12	--	--	52	52	Si	>100
240.80	--	10.68	10.18	10.18	--	--	-0.20	11.65	52	52	Si	31
433.44	29.64	--	10.18	10.18	-0.54	32.34	--	--	52	52	Si	11
481.60	48.53	--	10.18	10.18	-0.89	52.95	--	--	52	52	Si	6.8

Trave di fondazione: 9009 [15,21], Pilastrate [15,21] Sez. R: By=50.00 cm Bz=100.00 cm L=430.70 cm Ln=430.70 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	167.00	--	10.18	10.18	-3.07	182.22	--	--	44	40	Si	2.0
43.07	150.18	--	10.18	10.18	-2.76	163.86	--	--	44	40	Si	2.2
215.35	118.65	12.52	10.18	10.18	-2.18	129.45	-0.23	13.66	45	30	Si	2.8
387.63	135.74	--	10.18	10.18	-2.49	148.11	--	--	44	40	Si	2.4
430.70	149.32	--	10.18	10.18	-2.74	162.92	--	--	44	40	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	27.10	--	10.18	10.18	-0.50	29.57	--	--	46	48	Si	12
43.07	13.16	--	10.18	10.18	-0.24	14.36	--	--	46	48	Si	25
215.35	--	11.51	10.18	10.18	--	--	-0.21	12.56	48	46	Si	29
387.63	14.48	--	10.18	10.18	-0.27	15.80	--	--	46	48	Si	23
430.70	29.14	--	10.18	10.18	-0.54	31.80	--	--	46	48	Si	11

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	25.77	--	10.18	10.18	-0.47	28.12	--	--	52	52	Si	13
43.07	12.44	--	10.18	10.18	-0.23	13.57	--	--	52	52	Si	27
215.35	--	11.17	10.18	10.18	--	--	-0.21	12.19	52	52	Si	30
387.63	13.58	--	10.18	10.18	-0.25	14.82	--	--	52	52	Si	24
430.70	27.56	--	10.18	10.18	-0.51	30.07	--	--	52	52	Si	12

Trave di fondazione: 9009 [21,24], Pilastrate [21,24] Sez. R: By=50.00 cm Bz=100.00 cm L=287.70 cm Ln=287.70 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	157.89	--	10.18	10.18	-2.90	172.28	--	--	44	40	Si	2.1
28.77	144.71	2.76	10.18	10.18	-2.66	157.89	-0.05	3.01	44	40	Si	2.3
143.85	109.36	14.13	10.18	10.18	-2.01	119.32	-0.26	15.41	45	30	Si	3.0
258.93	97.02	5.06	10.18	10.18	-1.78	105.86	-0.09	5.52	44	40	Si	3.4
287.70	98.44	0.56	10.18	10.18	-1.81	107.41	-0.01	0.61	44	40	Si	3.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	6.62	--	10.18	10.18	-0.12	7.22	--	--	46	48	Si	50
28.77	--	0.75	10.18	10.18	--	--	-0.01	0.82	46	48	Si	>100
143.85	--	13.57	10.18	10.18	--	--	-0.25	14.81	48	46	Si	24
258.93	--	2.77	10.18	10.18	--	--	-0.05	3.02	46	48	Si	>100
287.70	4.30	--	10.18	10.18	-0.08	4.69	--	--	46	48	Si	77

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	5.99	--	10.18	10.18	-0.11	6.53	--	--	52	52	Si	55
28.77	--	0.75	10.18	10.18	--	--	-0.01	0.82	52	52	Si	>100
143.85	--	13.39	10.18	10.18	--	--	-0.25	14.61	52	52	Si	25
258.93	--	2.77	10.18	10.18	--	--	-0.05	3.02	52	52	Si	>100

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
287.70	3.60	--	10.18	10.18	-0.07	3.93	--	--	52	52	Si	92

Trave di fondazione: 9009 [24,29], Pilastrate [24,29] Sez. R: By=50.00 cm Bz=100.00 cm L=439.90 cm Ln=439.90 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	159.75	--	10.18	10.18	-2.93	174.31	--	--	44	40	Si	2.1
43.99	124.01	--	10.18	10.18	-2.28	135.31	--	--	44	40	Si	2.7
219.95	28.85	31.98	10.18	10.18	-0.53	31.48	-0.59	34.89	45	30	Si	10
395.91	--	6.19	10.18	10.18	--	--	-0.11	6.76	40	26	Si	53
439.90	13.10	1.18	10.18	10.18	-0.24	14.30	-0.02	1.29	30	45	Si	25

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	27.31	--	10.18	10.18	-0.50	29.80	--	--	46	48	Si	12
43.99	8.44	--	10.18	10.18	-0.15	9.20	--	--	46	48	Si	39
219.95	--	29.42	10.18	10.18	--	--	-0.54	32.10	48	46	Si	11
395.91	--	4.46	10.18	10.18	--	--	-0.08	4.86	48	46	Si	74
439.90	12.29	--	10.18	10.18	-0.23	13.41	--	--	46	48	Si	27

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	25.38	--	10.18	10.18	-0.47	27.69	--	--	52	52	Si	13
43.99	7.38	--	10.18	10.18	-0.14	8.05	--	--	52	52	Si	45
219.95	--	28.56	10.18	10.18	--	--	-0.52	31.17	52	52	Si	12
395.91	--	4.19	10.18	10.18	--	--	-0.08	4.57	52	52	Si	79
439.90	12.02	--	10.18	10.18	-0.22	13.11	--	--	52	52	Si	27

Trave di fondazione: 9010 [13,22], Pilastrate [13,22] Sez. R: By=50.00 cm Bz=100.00 cm L=466.53 cm Ln=460.87 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	149.82	--	12.72	12.72	-2.46	131.31	--	--	44	40	Si	2.7
46.09	128.37	--	12.72	12.72	-2.10	112.51	--	--	45	35	Si	3.2
230.43	116.65	16.95	12.72	12.72	-1.91	102.23	-0.28	14.85	45	30	Si	3.5
414.78	219.69	--	12.72	12.72	-3.60	192.55	--	--	44	40	Si	1.9
460.87	265.97	--	12.72	12.72	-4.36	233.12	--	--	44	40	Si	1.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	37.73	--	12.72	12.72	-0.62	33.07	--	--	46	48	Si	11
46.09	11.23	--	12.72	12.72	-0.18	9.85	--	--	48	47	Si	37
230.43	--	15.73	12.72	12.72	--	--	-0.26	13.79	48	46	Si	26
414.78	88.87	--	12.72	12.72	-1.46	77.89	--	--	46	48	Si	4.6
460.87	136.52	--	12.72	12.72	-2.24	119.65	--	--	46	48	Si	3.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	37.07	--	12.72	12.72	-0.61	32.49	--	--	52	52	Si	11
46.09	11.23	--	12.72	12.72	-0.18	9.85	--	--	52	52	Si	37
230.43	--	15.33	12.72	12.72	--	--	-0.25	13.43	52	52	Si	27
414.78	85.67	--	12.72	12.72	-1.40	75.09	--	--	52	52	Si	4.8
460.87	131.75	--	12.72	12.72	-2.16	115.47	--	--	52	52	Si	3.1

Trave di fondazione: 9010 [22,25], Pilastrate [22,25] Sez. R: By=50.00 cm Bz=100.00 cm L=289.26 cm Ln=287.70 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	243.15	--	12.72	12.72	-3.99	213.11	--	--	44	40	Si	1.7
28.77	215.55	--	12.72	12.72	-3.53	188.92	--	--	44	40	Si	1.9
143.85	136.01	--	12.72	12.72	-2.23	119.21	--	--	44	40	Si	3.0
258.93	104.26	--	12.72	12.72	-1.71	91.38	--	--	44	40	Si	3.9
287.70	103.53	--	12.72	12.72	-1.70	90.74	--	--	44	40	Si	4.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	80.60	--	12.72	12.72	-1.32	70.64	--	--	46	48	Si	5.1
28.77	59.69	--	12.72	12.72	-0.98	52.32	--	--	46	48	Si	6.9
143.85	9.90	--	12.72	12.72	-0.16	8.67	--	--	46	48	Si	41
258.93	13.16	--	12.72	12.72	-0.22	11.53	--	--	46	48	Si	31
287.70	22.08	--	12.72	12.72	-0.36	19.35	--	--	46	48	Si	19

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	77.73	--	12.72	12.72	-1.27	68.12	--	--	52	52	Si	5.3
28.77	57.45	--	12.72	12.72	-0.94	50.35	--	--	52	52	Si	7.1
143.85	9.13	--	12.72	12.72	-0.15	8.01	--	--	52	52	Si	45
258.93	12.21	--	12.72	12.72	-0.20	10.70	--	--	52	52	Si	34
287.70	20.83	--	12.72	12.72	-0.34	18.25	--	--	52	52	Si	20

Trave di fondazione: 9010 [25,30], Pilastrate [25,30] Sez. R: By=50.00 cm Bz=100.00 cm L=440.01 cm Ln=440.13 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	214.14	--	10.18	10.18	-3.93	233.64	--	--	44	40	Si	1.5
44.01	161.96	--	10.18	10.18	-2.97	176.72	--	--	44	40	Si	2.0
220.06	22.56	38.39	10.18	10.18	-0.41	24.61	-0.70	41.89	45	30	Si	8.6
396.11	--	31.48	10.18	10.18	--	--	-0.58	34.35	40	44	Si	10
440.13	--	27.69	10.18	10.18	--	--	-0.51	30.22	40	44	Si	12

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	98.90	--	10.18	10.18	-1.82	107.91	--	--	46	48	Si	3.3
44.01	57.62	--	10.18	10.18	-1.06	62.87	--	--	46	48	Si	5.7
220.06	--	36.05	10.18	10.18	--	--	-0.66	39.33	48	46	Si	9.2
396.11	--	23.34	10.18	10.18	--	--	-0.43	25.47	48	46	Si	14
440.13	--	4.42	10.18	10.18	--	--	-0.08	4.82	48	46	Si	75

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	95.03	--	10.18	10.18	-1.74	103.68	--	--	52	52	Si	3.5
44.01	55.12	--	10.18	10.18	-1.01	60.15	--	--	52	52	Si	6.0
220.06	--	35.27	10.18	10.18	--	--	-0.65	38.48	52	52	Si	9.4
396.11	--	22.45	10.18	10.18	--	--	-0.41	24.50	52	52	Si	15
440.13	--	3.95	10.18	10.18	--	--	-0.07	4.31	52	52	Si	83

Trave di fondazione: 9011 [23,26], Pilastrate [23,26] Sez. R: By=50.00 cm Bz=100.00 cm L=142.97 cm Ln=188.74 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	331.83	--	10.18	15.27	-5.25	244.52	--	--	44	40	Si	1.5
18.87	306.74	--	10.18	15.27	-4.85	226.03	--	--	44	40	Si	1.6
94.37	223.86	--	10.18	15.27	-3.54	164.96	--	--	44	40	Si	2.2
169.86	169.17	--	10.18	15.27	-2.68	124.66	--	--	44	40	Si	2.9
188.74	160.35	--	10.18	15.27	-2.54	118.16	--	--	44	40	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	120.59	--	10.18	15.27	-1.91	88.86	--	--	46	48	Si	4.1
18.87	106.86	--	10.18	15.27	-1.69	78.74	--	--	46	48	Si	4.6
94.37	68.81	--	10.18	15.27	-1.09	50.70	--	--	46	48	Si	7.1
169.86	57.69	--	10.18	15.27	-0.91	42.51	--	--	46	48	Si	8.5
188.74	59.55	--	10.18	15.27	-0.94	43.88	--	--	46	48	Si	8.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	117.62	--	10.18	15.27	-1.86	86.67	--	--	52	52	Si	4.2
18.87	104.26	--	10.18	15.27	-1.65	76.83	--	--	52	52	Si	4.7
94.37	67.13	--	10.18	15.27	-1.06	49.47	--	--	52	52	Si	7.3
169.86	56.11	--	10.18	15.27	-0.89	41.35	--	--	52	52	Si	8.7
188.74	57.85	--	10.18	15.27	-0.92	42.63	--	--	52	52	Si	8.4

Trave di fondazione: 9011 [26,31], Pilastrate [26,31] Sez. R: By=50.00 cm Bz=100.00 cm L=439.90 cm Ln=439.90 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	263.80	--	10.18	15.27	-4.17	194.39	--	--	44	40	Si	1.9
43.99	196.54	--	10.18	15.27	-3.11	144.83	--	--	44	40	Si	2.5
219.95	23.38	32.15	10.18	15.27	-0.37	17.23	-0.55	34.92	45	30	Si	10
395.91	--	34.80	10.18	15.27	--	--	-0.60	37.80	40	26	Si	9.5
439.90	--	23.97	10.18	15.27	--	--	-0.41	26.04	40	44	Si	14

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	138.36	--	10.18	15.27	-2.19	101.96	--	--	46	48	Si	3.5
43.99	88.57	--	10.18	15.27	-1.40	65.26	--	--	46	48	Si	5.5
219.95	--	29.10	10.18	15.27	--	--	-0.50	31.61	48	46	Si	11
395.91	--	31.20	10.18	15.27	--	--	-0.54	33.89	48	46	Si	11
439.90	--	15.70	10.18	15.27	--	--	-0.27	17.05	47	46	Si	21

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	134.25	--	10.18	15.27	-2.12	98.93	--	--	52	52	Si	3.6
43.99	86.00	--	10.18	15.27	-1.36	63.37	--	--	52	52	Si	5.7
219.95	--	28.08	10.18	15.27	--	--	-0.48	30.51	52	52	Si	12
395.91	--	30.30	10.18	15.27	--	--	-0.52	32.92	52	52	Si	11
439.90	--	15.36	10.18	15.27	--	--	-0.26	16.68	52	52	Si	22

Trave di fondazione: 9012 [2,8], Pilastrate [2,8] Sez. R: By=50.00 cm Bz=100.00 cm L=368.36 cm Ln=252.48 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	64.54	28.17	12.72	10.18	-1.15	70.25	-0.48	24.75	45	30	Si	5.1
25.25	57.15	33.38	12.72	10.18	-1.02	62.21	-0.56	29.33	45	30	Si	5.8

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
126.24	43.35	37.96	12.72	10.18	-0.77	47.19	-0.64	33.36	45	30	Si	7.6
227.23	47.41	20.82	12.72	10.18	-0.84	51.60	-0.35	18.29	45	30	Si	7.0
252.48	50.36	13.56	12.72	10.18	-0.90	54.81	-0.23	11.91	45	30	Si	6.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	25.57	12.72	10.18	--	--	-0.43	22.48	48	46	Si	16
25.25	--	30.44	12.72	10.18	--	--	-0.51	26.75	48	46	Si	13
126.24	--	34.75	12.72	10.18	--	--	-0.59	30.54	48	46	Si	12
227.23	--	19.27	12.72	10.18	--	--	-0.33	16.94	48	46	Si	21
252.48	--	12.76	12.72	10.18	--	--	-0.22	11.21	47	46	Si	32

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	24.71	12.72	10.18	--	--	-0.42	21.72	52	52	Si	17
25.25	--	29.46	12.72	10.18	--	--	-0.50	25.89	52	52	Si	14
126.24	--	33.68	12.72	10.18	--	--	-0.57	29.60	52	52	Si	12
227.23	--	18.76	12.72	10.18	--	--	-0.32	16.49	52	52	Si	22
252.48	--	12.49	12.72	10.18	--	--	-0.21	10.98	52	52	Si	33

Trave di fondazione: 9012 [8,13], Pilastrate [8,13] Sez. R: By=50.00 cm Bz=100.00 cm L=327.82 cm Ln=327.82 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	68.56	1.69	12.72	10.18	-1.22	74.63	-0.03	1.48	45	30	Si	4.8
32.78	59.87	17.90	12.72	10.18	-1.06	65.17	-0.30	15.73	45	30	Si	5.5
163.91	47.49	49.98	12.72	10.18	-0.84	51.69	-0.84	43.92	45	30	Si	7.0
295.03	72.07	25.25	12.72	10.18	-1.28	78.45	-0.43	22.19	45	30	Si	4.6
327.82	84.58	9.60	12.72	10.18	-1.50	92.06	-0.16	8.44	44	40	Si	3.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	1.58	12.72	10.18	--	--	-0.03	1.39	47	46	Si	>100
32.78	--	16.62	12.72	10.18	--	--	-0.28	14.60	48	46	Si	25
163.91	--	46.49	12.72	10.18	--	--	-0.79	40.86	48	46	Si	8.8
295.03	--	24.00	12.72	10.18	--	--	-0.41	21.09	48	46	Si	17
327.82	--	9.47	12.72	10.18	--	--	-0.16	8.32	46	47	Si	43

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	1.55	12.72	10.18	--	--	-0.03	1.36	52	52	Si	>100
32.78	--	16.19	12.72	10.18	--	--	-0.27	14.23	52	52	Si	25
163.91	--	45.33	12.72	10.18	--	--	-0.77	39.84	52	52	Si	9.0
295.03	--	23.58	12.72	10.18	--	--	-0.40	20.72	52	52	Si	17
327.82	--	9.45	12.72	10.18	--	--	-0.16	8.30	52	52	Si	43

Trave di fondazione: 9012 [13,16], Pilastrate [13,16] Sez. R: By=50.00 cm Bz=100.00 cm L=329.87 cm Ln=329.87 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	141.54	--	12.72	12.72	-2.32	124.05	--	--	44	40	Si	2.9
32.99	129.74	5.50	12.72	12.72	-2.13	113.71	-0.09	4.82	44	40	Si	3.2
164.93	120.65	8.07	12.72	12.72	-1.98	105.75	-0.13	7.07	44	40	Si	3.4
296.88	179.05	--	12.72	12.72	-2.93	156.93	--	--	44	40	Si	2.3
329.87	205.26	--	12.72	12.72	-3.36	179.90	--	--	44	40	Si	2.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	11.80	--	12.72	12.72	-0.19	10.34	--	--	46	48	Si	35
32.99	0.31	0.52	12.72	12.72	-0.01	0.27	-0.01	0.46	46	48	Si	>100
164.93	--	5.03	12.72	12.72	--	--	-0.08	4.41	46	48	Si	82
296.88	62.57	--	12.72	12.72	-1.03	54.84	--	--	46	48	Si	6.6
329.87	91.56	--	12.72	12.72	-1.50	80.25	--	--	46	48	Si	4.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	10.59	--	12.72	12.72	-0.17	9.28	--	--	52	52	Si	39
32.99	--	0.52	12.72	12.72	--	--	-0.01	0.46	52	52	Si	>100
164.93	--	5.03	12.72	12.72	--	--	-0.08	4.41	52	52	Si	82
296.88	60.29	--	12.72	12.72	-0.99	52.84	--	--	52	52	Si	6.8
329.87	88.48	--	12.72	12.72	-1.45	77.55	--	--	52	52	Si	4.6

Trave di fondazione: 9012 [16,23], Pilastrate [16,23] Sez. R: By=50.00 cm Bz=100.00 cm L=532.52 cm Ln=532.52 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	274.05	--	10.18	12.72	-4.63	240.85	--	--	44	40	Si	1.5
53.25	213.27	--	10.18	12.72	-3.60	187.43	--	--	44	40	Si	1.9
266.26	88.22	42.11	10.18	12.72	-1.49	77.53	-0.75	45.84	45	30	Si	4.6
479.27	131.22	--	10.18	12.72	-2.22	115.32	--	--	44	40	Si	3.1
532.52	177.20	--	10.18	12.72	-2.99	155.73	--	--	44	40	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	137.57	--	10.18	12.72	-2.33	120.91	--	--	46	48	Si	3.0
53.25	79.97	--	10.18	12.72	-1.35	70.28	--	--	46	48	Si	5.1
266.26	--	38.14	10.18	12.72	--	--	-0.68	41.51	48	46	Si	8.7
479.27	34.55	--	10.18	12.72	-0.58	30.36	--	--	46	48	Si	12
532.52	84.96	--	10.18	12.72	-1.44	74.67	--	--	46	48	Si	4.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	132.65	--	10.18	12.72	-2.24	116.58	--	--	52	52	Si	3.1
53.25	77.08	--	10.18	12.72	-1.30	67.74	--	--	52	52	Si	5.3
266.26	--	36.81	10.18	12.72	--	--	-0.65	40.07	52	52	Si	9.0
479.27	33.73	--	10.18	12.72	-0.57	29.64	--	--	52	52	Si	12
532.52	82.57	--	10.18	12.72	-1.40	72.56	--	--	52	52	Si	5.0

Trave di fondazione: 9013 [3,9], Pilastrate [3,9] Sez. R: By=50.00 cm Bz=100.00 cm L=327.85 cm Ln=327.85 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	41.43	15.36	12.72	10.18	-0.74	45.09	-0.26	13.50	45	30	Si	8.0
32.79	37.95	25.18	12.72	10.18	-0.67	41.31	-0.43	22.13	45	30	Si	8.7
163.93	54.54	28.47	12.72	10.18	-0.97	59.37	-0.48	25.02	45	30	Si	6.1
295.07	129.22	--	12.72	10.18	-2.30	140.65	--	--	44	40	Si	2.6
327.85	159.53	--	12.72	10.18	-2.84	173.65	--	--	44	40	Si	2.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	13.00	12.72	10.18	--	--	-0.22	11.43	48	46	Si	32
32.79	--	22.32	12.72	10.18	--	--	-0.38	19.62	48	46	Si	18
163.93	--	26.27	12.72	10.18	--	--	-0.44	23.08	48	46	Si	16
295.07	28.86	--	12.72	10.18	-0.51	31.42	--	--	46	48	Si	11
327.85	52.87	--	12.72	10.18	-0.94	57.55	--	--	46	48	Si	6.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	12.22	12.72	10.18	--	--	-0.21	10.74	52	52	Si	34
32.79	--	21.37	12.72	10.18	--	--	-0.36	18.78	52	52	Si	19
163.93	--	25.53	12.72	10.18	--	--	-0.43	22.44	52	52	Si	16
295.07	27.76	--	12.72	10.18	-0.49	30.22	--	--	52	52	Si	12
327.85	51.02	--	12.72	10.18	-0.91	55.54	--	--	52	52	Si	6.5

Trave di fondazione: 9013 [9,14], Pilastrate [9,14] Sez. R: By=50.00 cm Bz=100.00 cm L=329.87 cm Ln=329.87 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	254.76	--	12.72	12.72	-4.18	223.29	--	--	44	40	Si	1.6
32.99	216.29	--	12.72	12.72	-3.55	189.57	--	--	44	40	Si	1.9
164.93	107.56	1.49	12.72	12.72	-1.76	94.27	-0.02	1.31	44	40	Si	3.8
296.88	73.74	--	12.72	12.72	-1.21	64.63	--	--	44	40	Si	5.6
329.87	77.48	--	12.72	12.72	-1.27	67.91	--	--	44	40	Si	5.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	85.09	--	12.72	12.72	-1.39	74.58	--	--	46	48	Si	4.8
32.99	59.25	--	12.72	12.72	-0.97	51.93	--	--	46	48	Si	6.9
164.93	2.06	--	12.72	12.72	-0.03	1.80	--	--	46	48	Si	>100
296.88	23.26	--	12.72	12.72	-0.38	20.38	--	--	46	48	Si	18
329.87	41.51	--	12.72	12.72	-0.68	36.38	--	--	46	48	Si	9.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	82.50	--	12.72	12.72	-1.35	72.31	--	--	52	52	Si	5.0
32.99	57.34	--	12.72	12.72	-0.94	50.26	--	--	52	52	Si	7.2
164.93	1.55	--	12.72	12.72	-0.03	1.36	--	--	52	52	Si	>100
296.88	21.87	--	12.72	12.72	-0.36	19.17	--	--	52	52	Si	19
329.87	39.53	--	12.72	12.72	-0.65	34.65	--	--	52	52	Si	10

Trave di fondazione: 9013 [14,17], Pilastrate [14,17] Sez. R: By=50.00 cm Bz=100.00 cm L=532.52 cm Ln=532.52 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	266.07	--	10.18	12.72	-4.50	233.83	--	--	44	40	Si	1.5
53.25	205.48	--	10.18	12.72	-3.47	180.58	--	--	44	40	Si	2.0
266.26	83.86	48.18	10.18	12.72	-1.42	73.70	-0.86	52.45	45	30	Si	4.9
479.27	131.46	--	10.18	12.72	-2.22	115.54	--	--	44	40	Si	3.1
532.52	178.71	--	10.18	12.72	-3.02	157.06	--	--	44	40	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	134.86	--	10.18	12.72	-2.28	118.52	--	--	46	48	Si	3.0
53.25	75.59	--	10.18	12.72	-1.28	66.43	--	--	46	48	Si	5.4

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
266.26	--	44.11	10.18	12.72	--	--	-0.78	48.01	48	46	Si	7.5
479.27	33.08	--	10.18	12.72	-0.56	29.07	--	--	46	48	Si	12
532.52	85.37	--	10.18	12.72	-1.44	75.03	--	--	46	48	Si	4.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	129.21	--	10.18	12.72	-2.18	113.56	--	--	52	52	Si	3.2
53.25	72.17	--	10.18	12.72	-1.22	63.43	--	--	52	52	Si	5.7
266.26	--	42.75	10.18	12.72	--	--	-0.76	46.53	52	52	Si	7.7
479.27	32.53	--	10.18	12.72	-0.55	28.59	--	--	52	52	Si	13
532.52	83.27	--	10.18	12.72	-1.41	73.18	--	--	52	52	Si	4.9

Trave di fondazione: 9014 [17,23], Pilastrate [17,23] Sez. R: By=50.00 cm Bz=100.00 cm L=310.00 cm Ln=310.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	329.37	--	10.18	15.27	-5.21	242.71	--	--	44	40	Si	1.5
31.00	294.40	--	10.18	15.27	-4.66	216.94	--	--	44	40	Si	1.7
155.00	206.86	--	10.18	15.27	-3.27	152.43	--	--	44	40	Si	2.4
279.00	203.58	--	10.18	15.27	-3.22	150.02	--	--	44	40	Si	2.4
310.00	215.83	--	10.18	15.27	-3.41	159.04	--	--	44	40	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	140.91	--	10.18	15.27	-2.23	103.84	--	--	46	48	Si	3.5
31.00	114.99	--	10.18	15.27	-1.82	84.74	--	--	46	48	Si	4.2
155.00	62.63	--	10.18	15.27	-0.99	46.15	--	--	46	48	Si	7.8
279.00	92.29	--	10.18	15.27	-1.46	68.01	--	--	46	48	Si	5.3
310.00	112.37	--	10.18	15.27	-1.78	82.80	--	--	46	48	Si	4.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	137.16	--	10.18	15.27	-2.17	101.07	--	--	52	52	Si	3.6
31.00	112.01	--	10.18	15.27	-1.77	82.54	--	--	52	52	Si	4.4
155.00	61.23	--	10.18	15.27	-0.97	45.12	--	--	52	52	Si	8.0
279.00	90.09	--	10.18	15.27	-1.43	66.39	--	--	52	52	Si	5.4
310.00	109.60	--	10.18	15.27	-1.73	80.77	--	--	52	52	Si	4.5

Trave di fondazione: 9015 [14,16], Pilastrate [14,16] Sez. R: By=50.00 cm Bz=100.00 cm L=310.00 cm Ln=310.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	141.49	--	10.18	10.18	-2.60	154.38	--	--	44	40	Si	2.3
31.00	114.42	--	10.18	10.18	-2.10	124.85	--	--	44	40	Si	2.9
155.00	51.19	10.82	10.18	10.18	-0.94	55.85	-0.20	11.81	45	35	Si	6.4
279.00	57.17	--	10.18	10.18	-1.05	62.38	--	--	44	40	Si	5.8
310.00	69.72	--	10.18	10.18	-1.28	76.07	--	--	44	40	Si	4.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	75.28	--	10.18	10.18	-1.38	82.14	--	--	46	48	Si	4.4
31.00	48.62	--	10.18	10.18	-0.89	53.05	--	--	46	48	Si	6.8
155.00	--	10.48	10.18	10.18	--	--	-0.19	11.43	48	47	Si	31
279.00	5.44	--	10.18	10.18	-0.10	5.93	--	--	47	48	Si	61
310.00	20.94	--	10.18	10.18	-0.38	22.85	--	--	46	48	Si	16

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	72.31	--	10.18	10.18	-1.33	78.90	--	--	52	52	Si	4.6
31.00	46.53	--	10.18	10.18	-0.85	50.77	--	--	52	52	Si	7.1
155.00	--	10.40	10.18	10.18	--	--	-0.19	11.35	52	52	Si	32
279.00	5.41	--	10.18	10.18	-0.10	5.91	--	--	52	52	Si	61
310.00	20.59	--	10.18	10.18	-0.38	22.46	--	--	52	52	Si	16

Trave di fondazione: 9016 [9,13], Pilastrate [9,13] Sez. R: By=50.00 cm Bz=100.00 cm L=310.56 cm Ln=310.56 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	25.23	--	10.18	10.18	-0.46	27.53	--	--	30	45	Si	13
31.06	11.11	--	10.18	10.18	-0.20	12.12	--	--	44	40	Si	30
155.28	70.04	13.49	10.18	10.18	-1.29	76.42	-0.25	14.72	45	30	Si	4.7
279.51	179.78	--	10.18	10.18	-3.30	196.16	--	--	44	40	Si	1.8
310.56	216.20	--	10.18	10.18	-3.97	235.90	--	--	44	40	Si	1.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	23.23	--	10.18	10.18	-0.43	25.34	--	--	46	48	Si	14
31.06	8.30	--	10.18	10.18	-0.15	9.05	--	--	46	48	Si	40
155.28	--	12.42	10.18	10.18	--	--	-0.23	13.55	48	46	Si	27
279.51	26.62	--	10.18	10.18	-0.49	29.05	--	--	46	48	Si	12
310.56	45.35	--	10.18	10.18	-0.83	49.48	--	--	46	48	Si	7.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	22.56	--	10.18	10.18	-0.41	24.61	--	--	52	52	Si	15
31.06	8.06	--	10.18	10.18	-0.15	8.79	--	--	52	52	Si	41
155.28	--	12.06	10.18	10.18	--	--	-0.22	13.16	52	52	Si	27
279.51	25.86	--	10.18	10.18	-0.47	28.21	--	--	52	52	Si	13
310.56	44.03	--	10.18	10.18	-0.81	48.05	--	--	52	52	Si	7.5

Trave di fondazione: 9017 [3,8], Pilastrate [3,8] Sez. R: By=50.00 cm Bz=100.00 cm L=305.05 cm Ln=305.05 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	29.74	21.95	10.18	10.18	-0.55	32.45	-0.40	23.95	45	30	Si	11
30.50	28.42	26.54	10.18	10.18	-0.52	31.01	-0.49	28.96	45	30	Si	12
152.52	39.11	24.30	10.18	10.18	-0.72	42.68	-0.45	26.52	45	30	Si	8.4
274.54	74.15	--	10.18	10.18	-1.36	80.90	--	--	44	40	Si	4.4
305.05	88.23	--	10.18	10.18	-1.62	96.27	--	--	44	40	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.89	10.18	10.18	--	--	-0.38	22.79	48	46	Si	16
30.50	--	24.89	10.18	10.18	--	--	-0.46	27.16	48	46	Si	13
152.52	--	22.43	10.18	10.18	--	--	-0.41	24.47	48	46	Si	15
274.54	8.25	--	10.18	10.18	-0.15	9.00	--	--	46	48	Si	40
305.05	20.18	--	10.18	10.18	-0.37	22.02	--	--	46	48	Si	16

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	20.54	10.18	10.18	--	--	-0.38	22.41	52	52	Si	16
30.50	--	24.34	10.18	10.18	--	--	-0.45	26.56	52	52	Si	14
152.52	--	21.80	10.18	10.18	--	--	-0.40	23.79	52	52	Si	15
274.54	7.83	--	10.18	10.18	-0.14	8.55	--	--	52	52	Si	42
305.05	19.33	--	10.18	10.18	-0.35	21.09	--	--	52	52	Si	17

Trave di fondazione: 9018 [4,14], Pilastrate [4,14] Sez. R: By=50.00 cm Bz=100.00 cm L=461.53 cm Ln=472.02 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	66.09	--	10.18	10.18	-1.21	72.11	--	--	44	40	Si	5.0
47.20	31.09	16.41	10.18	10.18	-0.57	33.93	-0.30	17.90	45	30	Si	11
236.01	3.29	90.32	10.18	10.18	-0.06	3.59	-1.66	98.55	45	30	Si	3.7
424.82	115.10	--	10.18	10.18	-2.11	125.58	--	--	44	40	Si	2.9
472.02	172.27	--	10.18	10.18	-3.16	187.97	--	--	44	40	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	28.30	--	10.18	10.18	-0.52	30.88	--	--	46	48	Si	12
47.20	--	15.23	10.18	10.18	--	--	-0.28	16.62	48	46	Si	22
236.01	--	84.58	10.18	10.18	--	--	-1.55	92.28	48	46	Si	3.9
424.82	11.99	--	10.18	10.18	-0.22	13.08	--	--	46	48	Si	28
472.02	62.87	--	10.18	10.18	-1.15	68.60	--	--	46	48	Si	5.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	27.59	--	10.18	10.18	-0.51	30.11	--	--	52	52	Si	12
47.20	--	14.84	10.18	10.18	--	--	-0.27	16.19	52	52	Si	22
236.01	--	82.66	10.18	10.18	--	--	-1.52	90.19	52	52	Si	4.0
424.82	10.70	--	10.18	10.18	-0.20	11.68	--	--	52	52	Si	31
472.02	60.01	--	10.18	10.18	-1.10	65.48	--	--	52	52	Si	5.5

Trave di fondazione: 9019 [5,10], Pilastrate [5,10] Sez. R: By=50.00 cm Bz=100.00 cm L=378.19 cm Ln=377.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	37.83	--	10.18	10.18	-0.69	41.27	--	--	45	30	Si	8.7
37.70	23.30	17.65	10.18	10.18	-0.43	25.43	-0.32	19.25	45	30	Si	14
188.50	34.33	27.87	10.18	10.18	-0.63	37.46	-0.51	30.41	44	40	Si	9.6
339.30	172.94	--	10.18	10.18	-3.18	188.70	--	--	44	40	Si	1.9
377.00	226.17	--	10.18	10.18	-4.15	246.77	--	--	44	40	Si	1.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	6.07	--	10.18	10.18	-0.11	6.62	--	--	47	46	Si	54
37.70	--	15.80	10.18	10.18	--	--	-0.29	17.24	48	46	Si	21
188.50	--	24.70	10.18	10.18	--	--	-0.45	26.95	46	47	Si	13
339.30	90.58	--	10.18	10.18	-1.66	98.83	--	--	46	48	Si	3.6
377.00	138.46	--	10.18	10.18	-2.54	151.08	--	--	46	48	Si	2.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	6.05	--	10.18	10.18	-0.11	6.60	--	--	52	52	Si	55
37.70	--	15.18	10.18	10.18	--	--	-0.28	16.57	52	52	Si	22

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
188.50	--	24.68	10.18	10.18	--	--	-0.45	26.93	52	52	Si	13
339.30	85.25	--	10.18	10.18	-1.57	93.01	--	--	52	52	Si	3.9
377.00	131.34	--	10.18	10.18	-2.41	143.30	--	--	52	52	Si	2.5

Trave di fondazione: 9019 [10,18], Pilastrate [10,18] Sez. R: By=50.00 cm Bz=100.00 cm L=469.90 cm Ln=469.90 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	176.26	--	10.18	10.18	-3.24	192.31	--	--	44	40	Si	1.9
46.99	113.01	17.89	10.18	10.18	-2.08	123.31	-0.33	19.52	44	40	Si	2.9
234.95	--	113.32	10.18	10.18	--	--	-2.08	123.64	45	30	Si	2.9
422.91	7.54	30.94	10.18	10.18	-0.14	8.22	-0.57	33.76	45	30	Si	11
469.90	35.61	--	10.18	10.18	-0.65	38.86	--	--	45	30	Si	9.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	51.20	--	10.18	10.18	-0.94	55.86	--	--	46	48	Si	6.4
46.99	--	5.48	10.18	10.18	--	--	-0.10	5.98	46	48	Si	60
234.95	--	106.49	10.18	10.18	--	--	-1.96	116.19	48	46	Si	3.1
422.91	--	27.23	10.18	10.18	--	--	-0.50	29.71	48	46	Si	12
469.90	22.27	--	10.18	10.18	-0.41	24.30	--	--	47	46	Si	15

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	47.15	--	10.18	10.18	-0.87	51.45	--	--	52	52	Si	7.0
46.99	--	5.48	10.18	10.18	--	--	-0.10	5.98	52	52	Si	60
234.95	--	104.22	10.18	10.18	--	--	-1.91	113.71	52	52	Si	3.2
422.91	--	26.00	10.18	10.18	--	--	-0.48	28.37	52	52	Si	13
469.90	22.24	--	10.18	10.18	-0.41	24.27	--	--	52	52	Si	15

Trave di fondazione: 9020 [6,11], Pilastrate [6,11] Sez. R: By=50.00 cm Bz=100.00 cm L=377.00 cm Ln=377.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	52.72	--	12.72	12.72	-0.86	46.21	--	--	44	40	Si	7.8
37.70	35.27	8.49	12.72	12.72	-0.58	30.92	-0.14	7.44	45	30	Si	12
188.50	20.24	35.12	12.72	12.72	-0.33	17.74	-0.58	30.78	45	30	Si	12
339.30	94.38	--	12.72	12.72	-1.55	82.72	--	--	44	40	Si	4.4
377.00	126.40	--	12.72	12.72	-2.07	110.78	--	--	44	40	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	14.85	--	12.72	12.72	-0.24	13.01	--	--	46	48	Si	28
37.70	--	7.67	12.72	12.72	--	--	-0.13	6.72	48	46	Si	54
188.50	--	34.47	12.72	12.72	--	--	-0.57	30.21	48	46	Si	12
339.30	37.06	--	12.72	12.72	-0.61	32.48	--	--	46	48	Si	11
377.00	70.05	--	12.72	12.72	-1.15	61.40	--	--	46	48	Si	5.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	14.71	--	12.72	12.72	-0.24	12.89	--	--	52	52	Si	28
37.70	--	7.39	12.72	12.72	--	--	-0.12	6.48	52	52	Si	56
188.50	--	34.26	12.72	12.72	--	--	-0.56	30.02	52	52	Si	12
339.30	34.42	--	12.72	12.72	-0.56	30.16	--	--	52	52	Si	12
377.00	66.25	--	12.72	12.72	-1.09	58.06	--	--	52	52	Si	6.2

Trave di fondazione: 9020 [11,19], Pilastrate [11,19] Sez. R: By=50.00 cm Bz=100.00 cm L=469.90 cm Ln=469.90 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	125.57	--	12.72	12.72	-2.06	110.06	--	--	44	40	Si	3.3
46.99	97.58	3.34	12.72	12.72	-1.60	85.52	-0.05	2.93	44	40	Si	4.2
234.95	65.08	47.53	12.72	12.72	-1.07	57.04	-0.78	41.65	45	30	Si	6.3
422.91	142.71	--	12.72	12.72	-2.34	125.08	--	--	44	40	Si	2.9
469.90	182.22	--	12.72	12.72	-2.99	159.71	--	--	44	40	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	43.76	--	12.72	12.72	-0.72	38.35	--	--	46	48	Si	9.4
46.99	7.73	--	12.72	12.72	-0.13	6.77	--	--	46	48	Si	53
234.95	--	45.93	12.72	12.72	--	--	-0.75	40.25	48	46	Si	8.9
422.91	41.58	--	12.72	12.72	-0.68	36.45	--	--	46	48	Si	9.9
469.90	85.53	--	12.72	12.72	-1.40	74.96	--	--	46	48	Si	4.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	40.96	--	12.72	12.72	-0.67	35.90	--	--	52	52	Si	10
46.99	6.15	--	12.72	12.72	-0.10	5.39	--	--	52	52	Si	67
234.95	--	45.39	12.72	12.72	--	--	-0.74	39.78	52	52	Si	9.0
422.91	40.02	--	12.72	12.72	-0.66	35.07	--	--	52	52	Si	10
469.90	82.80	--	12.72	12.72	-1.36	72.57	--	--	52	52	Si	5.0

Trave di fondazione: 9020 [19,27], Pilastrate [19,27] Sez. R: By=50.00 cm Bz=100.00 cm L=414.09 cm Ln=413.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	210.99	--	10.18	10.18	-3.87	230.21	--	--	44	40	Si	1.6
41.30	165.36	--	10.18	10.18	-3.04	180.42	--	--	44	40	Si	2.0
206.50	35.76	26.35	10.18	10.18	-0.66	39.02	-0.48	28.75	45	30	Si	9.2
371.70	--	34.67	10.18	10.18	--	--	-0.64	37.83	40	26	Si	9.5
413.00	--	33.69	10.18	10.18	--	--	-0.62	36.76	40	44	Si	9.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	94.37	--	10.18	10.18	-1.73	102.97	--	--	46	48	Si	3.5
41.30	60.56	--	10.18	10.18	-1.11	66.07	--	--	46	48	Si	5.4
206.50	--	23.53	10.18	10.18	--	--	-0.43	25.67	48	46	Si	14
371.70	--	29.91	10.18	10.18	--	--	-0.55	32.63	48	46	Si	11
413.00	--	19.83	10.18	10.18	--	--	-0.36	21.64	48	46	Si	17

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	91.31	--	10.18	10.18	-1.68	99.63	--	--	52	52	Si	3.6
41.30	58.65	--	10.18	10.18	-1.08	64.00	--	--	52	52	Si	5.6
206.50	--	22.59	10.18	10.18	--	--	-0.41	24.65	52	52	Si	15
371.70	--	28.77	10.18	10.18	--	--	-0.53	31.40	52	52	Si	11
413.00	--	19.03	10.18	10.18	--	--	-0.35	20.76	52	52	Si	17

Trave di fondazione: 9021 [7,12], Pilastrate [7,12] Sez. R: By=50.00 cm Bz=100.00 cm L=377.00 cm Ln=377.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	61.30	--	12.72	12.72	-1.00	53.72	--	--	44	40	Si	6.7
37.70	46.08	6.52	12.72	12.72	-0.76	40.39	-0.11	5.72	45	30	Si	8.9
188.50	26.74	33.00	12.72	12.72	-0.44	23.43	-0.54	28.92	45	30	Si	12
339.30	62.76	10.53	12.72	12.72	-1.03	55.01	-0.17	9.23	44	40	Si	6.5
377.00	81.82	1.03	12.72	12.72	-1.34	71.71	-0.02	0.90	44	40	Si	5.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	9.13	--	12.72	12.72	-0.15	8.00	--	--	46	48	Si	45
37.70	--	5.71	12.72	12.72	--	--	-0.09	5.01	48	46	Si	72
188.50	--	30.96	12.72	12.72	--	--	-0.51	27.14	48	46	Si	13
339.30	--	5.57	12.72	12.72	--	--	-0.09	4.88	46	48	Si	74
377.00	9.53	--	12.72	12.72	-0.16	8.36	--	--	46	48	Si	43

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	9.00	--	12.72	12.72	-0.15	7.89	--	--	52	52	Si	46
37.70	--	5.44	12.72	12.72	--	--	-0.09	4.77	52	52	Si	75
188.50	--	30.28	12.72	12.72	--	--	-0.50	26.54	52	52	Si	14
339.30	--	5.57	12.72	12.72	--	--	-0.09	4.88	52	52	Si	74
377.00	8.02	--	12.72	12.72	-0.13	7.03	--	--	52	52	Si	51

Trave di fondazione: 9021 [12,20], Pilastrate [12,20] Sez. R: By=50.00 cm Bz=100.00 cm L=469.90 cm Ln=469.90 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	146.56	--	12.72	12.72	-2.40	128.46	--	--	44	40	Si	2.8
46.99	122.76	0.20	12.72	12.72	-2.01	107.60	-0.00	0.18	44	40	Si	3.3
234.95	78.86	27.89	12.72	12.72	-1.29	69.12	-0.46	24.44	45	30	Si	5.2
422.91	104.00	--	12.72	12.72	-1.70	91.15	--	--	44	40	Si	3.9
469.90	122.60	--	12.72	12.72	-2.01	107.45	--	--	44	40	Si	3.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	26.29	--	12.72	12.72	-0.43	23.04	--	--	46	48	Si	16
46.99	6.50	--	12.72	12.72	-0.11	5.70	--	--	46	48	Si	63
234.95	--	26.87	12.72	12.72	--	--	-0.44	23.55	48	46	Si	15
422.91	10.91	--	12.72	12.72	-0.18	9.56	--	--	46	48	Si	38
469.90	31.48	--	12.72	12.72	-0.52	27.59	--	--	46	48	Si	13

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	24.53	--	12.72	12.72	-0.40	21.50	--	--	52	52	Si	17
46.99	5.54	--	12.72	12.72	-0.09	4.86	--	--	52	52	Si	74
234.95	--	26.53	12.72	12.72	--	--	-0.43	23.26	52	52	Si	15
422.91	9.52	--	12.72	12.72	-0.16	8.34	--	--	52	52	Si	43
469.90	29.19	--	12.72	12.72	-0.48	25.58	--	--	52	52	Si	14

Trave di fondazione: 9021 [20,28], Pilastrate [20,28] Sez. R: By=50.00 cm Bz=100.00 cm L=413.00 cm Ln=413.00 cm Terreno=Terreno Milazzo Criterio: Fondazioni

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	117.34	10.04	10.18	10.18	-2.15	128.03	-0.18	10.95	44	40	Si	2.8

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
41.30	86.19	20.00	10.18	10.18	-1.58	94.04	-0.37	21.82	44	40	Si	3.8
206.50	10.32	47.32	10.18	10.18	-0.19	11.26	-0.87	51.63	45	30	Si	7.0
371.70	--	14.37	10.18	10.18	--	--	-0.26	15.68	40	26	Si	23
413.00	7.70	3.73	10.18	10.18	-0.14	8.40	-0.07	4.07	40	44	Si	43

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	4.25	10.18	10.18	--	--	-0.08	4.64	46	48	Si	78
41.30	--	18.56	10.18	10.18	--	--	-0.34	20.25	46	48	Si	18
206.50	--	43.55	10.18	10.18	--	--	-0.80	47.51	48	46	Si	7.6
371.70	--	10.75	10.18	10.18	--	--	-0.20	11.73	48	46	Si	31
413.00	7.26	--	10.18	10.18	-0.13	7.92	--	--	48	46	Si	45

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	M+	M-	Afsup	Afinf	σc+	σf+	σc-	σf-	Cb+	Cb-.	Ver.	CS
cm	kN*m	kN*m	cmq	cmq	MPa	MPa	MPa	MPa				
0.00	--	4.25	10.18	10.18	--	--	-0.08	4.64	52	52	Si	78
41.30	--	18.56	10.18	10.18	--	--	-0.34	20.25	52	52	Si	18
206.50	--	42.29	10.18	10.18	--	--	-0.78	46.14	52	52	Si	7.8
371.70	--	10.17	10.18	10.18	--	--	-0.19	11.10	52	52	Si	32
413.00	7.26	--	10.18	10.18	-0.13	7.92	--	--	52	52	Si	45

Verifica dei pilastri (Stati limite esercizio)

Scenario di calcolo: **SLC_SVO_A2_STR+GEO 2018**

Simbologia

Terreno — Nome della stratigrafia per travi Winkler
L [cm] — Lunghezza teorica elemento (distanza tra i nodi)
Ln [cm] — Lunghezza netta elemento (tiene conto dei conci rigidi)
L2,L3 [cm] — Lunghezze libere di inflessione
Sez. R: Sezione Rettangolare
- By[cm]: Larghezza (asse locale y)
- Bz[cm]: Larghezza (asse locale z)

Sez. T: Sezione a T (rovescia e non)
- Ba[cm]: Larghezza base inferiore
- Ha[cm]: Altezza inferiore
- Bs[cm]: Larghezza superiore
- Hs[cm]: Altezza superiore

Sez. L: Sezione ad L (rovescia e non)
- Ba[cm]: Larghezza base inferiore
- Ha[cm]: Altezza inferiore
- Bs[cm]: Larghezza superiore
- Hs[cm]: Altezza superiore

Sez. C: Sezione circolare
- R[cm]: Raggio

Sez. G: Sezione generica
- B[cm]: Larghezza
- H[cm]: Altezza

X [cm] — Punto di verifica
σca [MPa] — Tensione ammissibile nel cls
σfa [MPa] — Tensione ammissibile nell'acciaio
σcta [MPa] — Tensione ammissibile a trazione (quando richiesto dalla verifica)
M- [kN*m] — Momento negativo massimo di calcolo
M+ [kN*m] — Momento positivo massimo di calcolo
M [kN*m] — Momento di calcolo (travi a flessione, pilastri circolari
My [kN*m] — Momento calcolo per verifiche a pressoflessione
Mz [kN*m] — Momento calcolo per verifiche a pressoflessione (Sez. L,Pilastri)

N [kN]	Sforzo normale corrispondente ad My (e Mz per Sez. L,Pilastri)
Afsup [cmq]	Area di ferro superiore
Afinf [cmq]	Area di ferro inferiore
Afsin [cmq]	Area di ferro sinistra (Sez. L)
Afdes [cmq]	Area di ferro destra (Sez. L)
σc- [MPa]	Tensione nel cls compresso per effetto di M-
σcy [MPa]	Tensione nel cls compresso per effetto di (N,My) in caso di pressoflessione retta
σcz [MPa]	Tensione nel cls compresso per effetto di (N,Mz) in caso di pressoflessione retta
σc+ [MPa]	Tensione nel cls compresso per effetto di M+
σct- [MPa]	Tensione nel cls teso per effetto di M-
σct+ [MPa]	Tensione nel cls teso per effetto di M+
σf- [MPa]	Tensione nell'acciaio per effetto di M-
σf+ [MPa]	Tensione nell'acciaio per effetto di M+
σfy [MPa]	Tensione nel acciaio per effetto di (N,My) in caso di pressoflessione retta
σfz [MPa]	Tensione nel acciaio per effetto di (N,Mz) in caso di pressoflessione retta
Cb-	Combinazione di carico generatore di M-
Cb+	Combinazione di carico generatore di M+
σc [MPa]	Tensione nel cls per effetto di N My
σf [MPa]	Tensione nell'acciaio per effetto di N My
Cb	Combinazione di carico generatore di N My
Act [m^2]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso
$S_{r,max}$ [cm]	Distanza massima delle fessure
σsfmed [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm_Freq [mm]	Apertura ammissibile delle fessure per combinazione Frequente
Wamm_Qp [mm]	Apertura ammissibile delle fessure per combinazione Quasi Permanente
Wamm_Rara [mm]	Apertura ammissibile delle fessure per combinazione Rara
Cs	Coefficiente di sicurezza definito come minimo di σAmm/σ tra acciaio e calcestruzzo oppure Wamm/Wk

Pilastro: 2 [2,102] Sez. R: By=125.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 12.06	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 12.06	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
44	161.92	5291.25	0.031	50.691	142.913

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-136.70	-71.30	229.00	-10.73	248.45	45	Si	1.4
439.00	-120.76	-20.36	6.03	-1.62	22.70	44	Si	9.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-121.16	5.20	-7.85	-0.59	-0.44	46	Si	19
439.00	-80.00	-11.76	2.35	-0.91	10.72	46	Si	12

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-117.84	4.88	-7.32	-0.57	-0.57	52	Si	20
439.00	-76.68	-11.19	2.29	-0.86	10.10	52	Si	13

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-117.84	4.88	-7.32	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-117.84	4.88	-7.32	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-76.68	-11.19	2.29	0.06	18.10	45.26	21.87	8.52	0.005	0.009	52(Qp)	Si	33
439.00	-80.00	-11.76	2.35	0.06	18.12	45.29	21.91	9.06	0.006	0.010	46(Fr)	Si	41

Pilastro: 3 [3,103] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	151.84	3386.40	0.045	50.691	118.064

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-109.35	-49.58	20.26	-6.86	164.78	45	Si	2.2
439.00	-83.01	-1.67	75.32	-3.53	89.93	45	Si	4.0
439.00	-114.61	-4.09	79.11	-4.02	87.04	44	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-134.49	4.52	-46.44	-2.52	30.18	46	Si	4.5
439.00	-108.15	-7.66	20.36	-1.67	12.90	46	Si	6.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-130.32	4.29	-45.11	-2.43	29.26	52	Si	4.6
439.00	-103.98	-7.33	19.83	-1.61	12.56	52	Si	6.9

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-130.32	4.29	-45.11	0.04	11.69	29.22	21.20	16.24	0.010	0.017	52(Qp)	Si	18
0.00	-134.49	4.52	-46.44	0.04	11.68	29.20	21.19	16.69	0.010	0.017	46(Fr)	Si	23
439.00	-103.98	-7.33	19.83	0.02	7.80	19.49	21.08	7.21	0.004	0.007	52(Qp)	Si	41
439.00	-108.15	-7.66	20.36	0.02	7.78	19.46	21.03	7.39	0.004	0.008	46(Fr)	Si	53

Pilastro: 4 [4,104] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	362.05	3386.40	0.107	50.691	76.458

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-263.21	-41.37	-0.02	-4.79	61.91	45	Si	3.1
0.00	-336.36	-40.44	-8.98	-5.01	44.02	44	Si	3.0
439.00	-236.87	-23.93	105.69	-7.61	120.53	45	Si	2.0
439.00	-310.02	-26.74	105.57	-7.70	100.46	44	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-322.53	0.49	-47.18	-2.41	-0.56	46	Si	4.6
439.00	-286.40	-8.90	12.32	-1.96	-4.26	48	Si	5.7
439.00	-296.19	-9.30	12.31	-2.02	-4.47	46	Si	5.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-312.74	0.34	-45.96	-2.33	-0.57	52	Si	4.8
439.00	-286.40	-8.90	12.32	-1.96	-4.26	52	Si	5.7

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-312.74	0.34	-45.96	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-312.74	0.34	-45.96	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-286.40	-8.90	12.32	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-296.19	-9.30	12.31	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 4 [104,204] Sez. R: By=80.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
375.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	168.73	3386.40	0.050	43.301	112.000

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-123.50	-33.12	59.81	-6.95	133.78	45	Si	2.1

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
375.00	-135.85	-23.90	28.94	-4.14	63.11	30	Si	3.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-144.11	21.06	-12.77	-3.00	36.91	46	Si	3.7
375.00	-121.61	-20.87	26.58	-3.67	55.21	46	Si	3.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-139.36	20.17	-12.73	-2.89	35.29	52	Si	3.9
375.00	-116.86	-19.86	25.79	-3.51	52.57	52	Si	3.2

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-139.36	20.17	-12.73	0.04	12.10	30.25	21.55	24.40	0.015	0.026	52(Qp)	Si	12
0.00	-144.11	21.06	-12.77	0.04	12.11	30.28	21.59	25.75	0.016	0.027	46(Fr)	Si	15
375.00	-116.86	-19.86	25.79	0.05	12.42	31.05	22.43	33.43	0.021	0.036	52(Qp)	Si	8.2
375.00	-121.61	-20.87	26.58	0.05	12.43	31.07	22.45	35.32	0.023	0.039	46(Fr)	Si	10

Pilastro: 5 [5,105] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	349.84	2539.80	0.138	50.691	67.361

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-265.67	-34.19	46.03	-8.03	93.06	45	Si	1.9
439.00	-245.91	-11.59	36.55	-4.09	23.92	45	Si	3.7
439.00	-312.34	-13.38	34.04	-4.25	14.82	44	Si	3.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-296.61	-0.79	14.54	-2.07	-11.40	51	Si	5.4
0.00	-305.55	-0.63	15.02	-2.12	-11.90	46	Si	5.3
439.00	-276.85	-3.14	-10.43	-2.00	-10.09	48	Si	5.6
439.00	-285.79	-3.40	-10.77	-2.08	-10.25	46	Si	5.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-296.61	-0.79	14.54	-2.07	-11.40	52	Si	5.4
439.00	-276.85	-3.14	-10.43	-2.00	-10.09	52	Si	5.6

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-296.61	-0.79	14.54	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-296.61	-0.79	14.54	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-276.85	-3.14	-10.43	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-285.79	-3.40	-10.77	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 5 [105,205] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
375.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	168.48	2539.80	0.066	43.301	97.067

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-123.71	-26.42	30.10	-6.00	94.01	45	Si	2.5
375.00	-106.83	-9.54	42.38	-4.46	70.48	45	Si	3.4
375.00	-144.31	-13.83	41.20	-4.91	64.13	44	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-139.47	8.68	0.83	-1.43	-0.44	46	Si	7.8
375.00	-122.60	-9.29	-3.83	-1.60	4.46	46	Si	7.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-134.54	8.21	0.77	-1.37	-0.66	52	Si	8.2
375.00	-117.67	-8.70	-3.67	-1.51	3.88	52	Si	7.4

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-134.54	8.21	0.77	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-134.54	8.21	0.77	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
375.00	-117.67	-8.70	-3.67	0.01	7.19	17.98	16.12	2.03	0.001	0.002	52(Qp)	Si	>100
375.00	-122.60	-9.29	-3.83	0.01	7.63	19.08	16.16	2.51	0.001	0.002	46(Fr)	Si	>100

Pilastro: 6 [6,106] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq

Zona	Armature		
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	261.45	2539.80	0.103	50.691	77.919

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-195.23	-36.53	52.06	-9.06	136.37	45	Si	1.6
0.00	-245.20	-35.66	58.25	-9.26	123.98	44	Si	1.6
439.00	-175.48	-9.73	28.06	-3.25	22.55	45	Si	4.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-225.86	-1.34	28.07	-2.40	2.35	51	Si	4.7
0.00	-232.53	-1.22	28.93	-2.46	2.27	46	Si	4.6
439.00	-212.78	-3.78	-26.11	-2.49	5.00	46	Si	4.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-225.86	-1.34	28.07	-2.40	2.35	52	Si	4.7
439.00	-206.11	-3.53	-25.42	-2.41	4.78	52	Si	4.7

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-225.86	-1.34	28.07	0.01	4.12	10.30	15.41	1.65	0.001	0.001	52(Qp)	Si	>100
0.00	-225.86	-1.34	28.07	0.01	4.12	10.30	15.41	1.65	0.001	0.001	51(Fr)	Si	>100
439.00	-206.11	-3.53	-25.42	0.01	4.25	10.62	15.71	2.91	0.001	0.002	52(Qp)	Si	>100
439.00	-212.78	-3.78	-26.11	0.01	4.24	10.59	15.70	3.00	0.001	0.002	46(Fr)	Si	>100

Pilastro: 6 [106,206] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
375.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	92.99	2539.80	0.037	43.301	130.655

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-67.56	-25.40	40.71	-6.85	132.27	45	Si	2.2
375.00	-50.69	-11.28	33.77	-4.20	80.70	45	Si	3.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-82.17	8.28	22.23	-2.76	35.20	46	Si	4.1
375.00	-65.30	-7.53	-27.72	-3.12	51.17	46	Si	3.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-79.65	7.89	21.67	-2.66	33.99	52	Si	4.2
375.00	-62.77	-7.12	-26.89	-3.00	49.39	52	Si	3.7

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-79.65	7.89	21.67	0.03	12.17	30.41	19.11	17.17	0.009	0.016	52(Qp)	Si	19
0.00	-82.17	8.28	22.23	0.03	12.17	30.43	19.11	17.79	0.010	0.017	46(Fr)	Si	24
375.00	-62.77	-7.12	-26.89	0.04	13.29	33.22	19.57	25.02	0.014	0.024	52(Qp)	Si	13
375.00	-65.30	-7.53	-27.72	0.04	13.28	33.21	19.57	25.82	0.014	0.025	46(Fr)	Si	16

Pilastro: 7 [7,107] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	110.33	3386.40	0.033	50.691	138.503

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-79.14	-53.49	9.26	-6.67	183.27	45	Si	2.0
0.00	-102.29	-52.48	15.86	-6.95	175.27	44	Si	2.1
439.00	-52.80	-2.63	44.46	-2.32	54.44	45	Si	6.4
439.00	-75.95	-5.32	39.95	-2.43	42.75	44	Si	6.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-97.71	-2.21	30.35	-1.55	15.76	46	Si	7.3
439.00	-71.37	-3.69	-20.80	-1.29	13.32	46	Si	8.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-94.66	-2.34	29.42	-1.52	15.59	52	Si	7.4
439.00	-68.32	-3.34	-20.18	-1.23	12.72	52	Si	9.1

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-94.66	-2.34	29.42	0.03	11.09	27.74	20.76	8.17	0.005	0.008	52(Qp)	Si	36
0.00	-97.71	-2.21	30.35	0.03	11.08	27.70	20.75	8.32	0.005	0.008	46(Fr)	Si	48
439.00	-68.32	-3.34	-20.18	0.03	11.05	27.64	20.73	7.18	0.004	0.007	52(Qp)	Si	42
439.00	-71.37	-3.69	-20.80	0.03	11.02	27.56	20.71	7.44	0.004	0.007	46(Fr)	Si	53

Pilastro: 8 [8,108] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm

L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	131.97	2539.80	0.052	50.691	109.674

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-80.20	-18.91	43.17	-6.50	123.55	45	Si	2.3
439.00	-60.45	-24.30	16.67	-5.16	109.53	45	Si	2.9
439.00	-90.24	-25.84	15.54	-5.25	100.14	44	Si	2.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-116.25	3.74	-5.78	-1.15	-1.04	51	Si	9.8
0.00	-120.18	3.91	-5.82	-1.18	-1.11	46	Si	9.5
439.00	-96.49	-4.50	0.60	-0.89	-1.89	48	Si	13
439.00	-100.43	-4.71	0.46	-0.92	-2.04	46	Si	12

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-116.25	3.74	-5.78	-1.15	-1.04	52	Si	9.8
439.00	-96.49	-4.50	0.60	-0.89	-1.89	52	Si	13

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-116.25	3.74	-5.78	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-116.25	3.74	-5.78	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-96.49	-4.50	0.60	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-100.43	-4.71	0.46	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 9 [9,109] Sez. R: By=30.00 cm Bz=70.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	238.28	2963.10	0.080	50.691	88.160

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-166.69	-19.35	11.44	-2.39	13.05	45	Si	6.3

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
439.00	-143.65	-81.60	32.25	-9.14	169.97	45	Si	1.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-219.41	30.64	-2.86	-2.14	3.23	46	Si	5.2
439.00	-190.08	-11.89	-1.33	-1.26	-5.15	48	Si	8.9
439.00	-196.36	-12.23	-1.33	-1.30	-5.39	46	Si	8.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-213.12	29.62	-2.77	-2.07	3.04	52	Si	5.4
439.00	-190.08	-11.89	-1.33	-1.26	-5.15	52	Si	8.9

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-213.12	29.62	-2.77	0.00	3.89	9.73	15.58	1.76	0.001	0.001	52(Qp)	Si	>100
0.00	-219.41	30.64	-2.86	0.01	3.94	9.85	15.64	1.90	0.001	0.001	46(Fr)	Si	>100
439.00	-190.08	-11.89	-1.33	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-196.36	-12.23	-1.33	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 9 [109,209] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	131.29	2963.10	0.044	43.301	118.767

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-95.29	-44.97	16.54	-4.80	82.70	45	Si	3.1
375.00	-102.05	-17.94	38.36	-5.99	126.59	44	Si	2.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-117.43	11.52	-2.79	-1.07	0.44	46	Si	10
375.00	-97.75	-13.68	10.21	-1.98	18.40	46	Si	5.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-113.94	11.15	-2.65	-1.03	0.35	52	Si	11
375.00	-94.25	-13.13	9.87	-1.91	17.75	52	Si	5.9

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-113.94	11.15	-2.65	0.00	2.38	5.95	13.55	0.35	0.000	0.000	52(Qp)	Si	>100
0.00	-117.43	11.52	-2.79	0.00	2.45	6.12	13.64	0.44	0.000	0.000	46(Fr)	Si	>100
375.00	-94.25	-13.13	9.87	0.03	11.55	28.88	18.92	8.54	0.005	0.008	52(Qp)	Si	38
375.00	-97.75	-13.68	10.21	0.03	11.55	28.87	18.92	8.82	0.005	0.008	46(Fr)	Si	49

Pilastro: 10 [10,110] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	414.76	2539.80	0.163	50.691	61.864

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-284.73	-50.12	32.07	-8.44	95.33	45	Si	1.8
0.00	-379.25	-51.93	34.05	-8.62	74.52	44	Si	1.7
439.00	-264.97	-43.91	12.23	-4.86	32.64	45	Si	3.1
439.00	-359.49	-45.65	11.01	-4.92	16.77	44	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-354.27	-7.19	7.65	-2.69	-13.15	51	Si	4.2
0.00	-367.11	-7.41	7.93	-2.79	-13.65	46	Si	4.0
439.00	-334.51	-8.74	-4.01	-2.34	-14.60	48	Si	4.8
439.00	-347.35	-9.02	-4.18	-2.43	-15.18	46	Si	4.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-354.27	-7.19	7.65	-2.69	-13.15	52	Si	4.2
439.00	-334.51	-8.74	-4.01	-2.34	-14.60	52	Si	4.8

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-354.27	-7.19	7.65	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-354.27	-7.19	7.65	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-334.51	-8.74	-4.01	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-347.35	-9.02	-4.18	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 10 [110,210] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq

Zona	Armature		
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	215.74	2539.80	0.085	43.301	85.777

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-136.42	-9.10	27.95	-4.97	80.01	45	Si	3.0
375.00	-177.61	-77.95	8.17	-7.12	127.25	44	Si	2.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-185.75	30.54	-1.34	-2.48	9.74	46	Si	4.5
375.00	-168.88	-35.56	0.20	-2.67	19.16	46	Si	4.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-178.14	29.41	-1.34	-2.40	9.56	52	Si	4.7
375.00	-161.26	-33.95	0.23	-2.55	18.33	52	Si	4.4

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-178.14	29.41	-1.34	0.01	7.65	19.13	17.23	7.85	0.004	0.007	52(Qp)	Si	46
0.00	-185.75	30.54	-1.34	0.01	7.63	19.08	17.20	8.03	0.004	0.007	46(Fr)	Si	60
375.00	-161.26	-33.95	0.23	0.02	8.80	21.99	19.01	11.01	0.006	0.010	52(Qp)	Si	30
375.00	-168.88	-35.56	0.20	0.02	8.80	21.99	19.01	11.54	0.006	0.011	46(Fr)	Si	38

Pilastro: 11 [11,111] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	449.52	2539.80	0.177	50.691	59.424

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-296.09	-22.89	49.96	-6.56	56.75	45	Si	2.3
0.00	-393.69	-22.70	56.83	-6.97	44.52	44	Si	2.1
439.00	-276.33	-21.86	28.21	-4.90	30.58	45	Si	3.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-397.21	-0.61	28.40	-3.13	-10.55	51	Si	3.6
0.00	-410.29	-0.59	29.36	-3.23	-10.93	46	Si	3.5
439.00	-377.46	-3.41	-26.97	-3.21	-7.24	48	Si	3.5
439.00	-390.53	-3.57	-27.85	-3.33	-7.50	46	Si	3.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-397.21	-0.61	28.40	-3.13	-10.55	52	Si	3.6
439.00	-377.46	-3.41	-26.97	-3.21	-7.24	52	Si	3.5

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-397.21	-0.61	28.40	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-397.21	-0.61	28.40	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-377.46	-3.41	-26.97	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-390.53	-3.57	-27.85	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 11 [111,211] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
375.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	183.86	2539.80	0.072	43.301	92.917

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-101.83	-8.99	41.97	-4.35	70.32	45	Si	3.4
375.00	-84.96	-31.82	39.41	-7.63	145.42	45	Si	2.0
375.00	-129.73	-34.54	35.88	-7.64	130.88	44	Si	2.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-166.19	8.13	17.68	-2.35	9.13	46	Si	4.8
375.00	-149.31	-8.48	-16.42	-2.29	10.82	46	Si	4.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-160.30	7.83	17.18	-2.27	8.91	52	Si	4.9
375.00	-143.42	-8.12	-15.93	-2.20	10.50	52	Si	5.1

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-	7.83	17.18	0.01	5.52	13.79	16.66	4.23	0.002	0.003	52(Qp)	Si	88

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
	160.30												
0.00	-166.19	8.13	17.68	0.01	5.50	13.74	16.63	4.30	0.002	0.003	46(Fr)	Si	>100
375.00	-143.42	-8.12	-15.93	0.01	6.17	15.43	17.20	5.70	0.003	0.005	52(Qp)	Si	63
375.00	-149.31	-8.48	-16.42	0.01	6.16	15.40	17.17	5.83	0.003	0.005	46(Fr)	Si	82

Pilastro: 12 [12,112] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	169.82	2539.80	0.067	50.691	96.683

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-101.47	-60.21	11.29	-6.43	128.49	45	Si	2.3
0.00	-144.49	-60.59	13.35	-6.70	113.60	44	Si	2.2
439.00	-81.71	-21.52	22.99	-5.33	99.76	45	Si	2.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-147.14	-8.85	7.85	-1.84	3.60	51	Si	6.1
0.00	-152.81	-8.91	8.14	-1.89	3.49	46	Si	5.9
439.00	-127.39	5.66	-11.95	-2.16	12.69	48	Si	5.2
439.00	-133.06	5.63	-12.36	-2.22	12.64	46	Si	5.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-147.14	-8.85	7.85	-1.84	3.60	52	Si	6.1
439.00	-127.39	5.66	-11.95	-2.16	12.69	52	Si	5.2

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-147.14	-8.85	7.85	0.01	3.76	9.39	15.89	3.60	0.002	0.003	52(Qp)	Si	>100
0.00	-147.14	-8.85	7.85	0.01	3.76	9.39	15.89	3.60	0.002	0.003	51(Fr)	Si	>100
439.00	-127.39	5.66	-11.95	0.02	9.11	22.78	17.98	8.22	0.004	0.007	52(Qp)	Si	42
439.00	-127.39	5.66	-11.95	0.02	9.11	22.78	17.98	8.22	0.004	0.007	48(Fr)	Si	56

Pilastro: 13 [13,113] Sez. R: By=30.00 cm Bz=70.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Zona	Armature		
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	379.42	2963.10	0.128	50.691	69.864

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-301.43	-7.46	17.28	-2.80	0.38	45	Si	5.3
0.00	-371.00	-2.75	18.11	-2.97	-5.56	44	Si	5.0
439.00	-278.38	-85.35	28.33	-8.32	109.70	45	Si	1.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-308.58	24.98	0.60	-2.12	-7.21	51	Si	5.3
0.00	-317.85	25.64	0.70	-2.19	-7.40	46	Si	5.1
439.00	-285.53	-2.08	-8.62	-1.88	-8.94	48	Si	6.0
439.00	-294.80	-1.75	-9.03	-1.94	-9.30	46	Si	5.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-308.58	24.98	0.60	-2.12	-7.21	52	Si	5.3
439.00	-285.53	-2.08	-8.62	-1.88	-8.94	52	Si	6.0

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-308.58	24.98	0.60	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-308.58	24.98	0.60	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-285.53	-2.08	-8.62	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-294.80	-1.75	-9.03	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 13 [113,213] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
44	159.87	2963.10	0.054	43.301	107.630

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-159.87	-48.89	32.72	-7.11	116.31	44	Si	2.1
375.00	-97.86	-32.35	-5.70	-2.49	32.36	30	Si	6.0
375.00	-140.18	-24.92	11.46	-2.70	23.47	44	Si	5.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-108.47	10.63	11.62	-2.00	16.98	46	Si	5.6
375.00	-88.78	-29.37	-4.94	-2.24	28.93	46	Si	5.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-105.44	10.55	11.11	-1.93	16.14	52	Si	5.8
375.00	-85.76	-28.38	-4.69	-2.15	27.79	52	Si	5.2

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-105.44	10.55	11.11	0.03	11.46	28.66	18.68	8.27	0.004	0.008	52(Qp)	Si	40
0.00	-108.47	10.63	11.62	0.03	11.50	28.74	18.77	8.91	0.005	0.008	46(Fr)	Si	49
375.00	-85.76	-28.38	-4.69	0.03	12.06	30.15	20.25	15.11	0.009	0.015	52(Qp)	Si	20
375.00	-88.78	-29.37	-4.94	0.04	12.06	30.16	20.26	15.70	0.009	0.015	46(Fr)	Si	26

Pilastro: 14 [14,37] Sez. R: By=30.00 cm Bz=60.00 cm L=80.00 cm Ln=80.00 cm L2=80.00 cm L3=80.00 cm Criterio: Pilastri tozzi

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
80.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	438.82	2539.80	0.173	9.238	60.144

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-305.16	26.25	-2.13	-2.81	-4.15	43	Si	5.3
0.00	-438.82	37.37	-3.07	-4.02	-6.19	30	Si	3.7
80.00	-267.66	-24.65	13.13	-3.69	11.91	45	Si	4.1
80.00	-365.96	-25.42	12.77	-4.04	2.38	44	Si	3.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-385.36	32.92	-2.70	-3.54	-5.37	51	Si	3.2
0.00	-398.73	34.03	-2.79	-3.66	-5.58	46	Si	3.1
80.00	-381.76	1.91	-1.48	-2.03	-24.59	48	Si	5.5
80.00	-395.13	1.80	-1.54	-2.10	-25.56	46	Si	5.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-385.36	32.92	-2.70	-3.54	-5.37	52	Si	3.2
80.00	-381.76	1.91	-1.48	-2.03	-24.59	52	Si	5.5

Pilastro: 14 [114,214] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq

Zona	Armature		
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	191.07	2539.80	0.075	43.301	91.148

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-95.20	-6.60	12.18	-2.30	23.74	45	Si	6.5
0.00	-191.07	14.89	-16.59	-3.45	21.70	30	Si	4.3
375.00	-78.32	-76.42	23.17	-9.88	216.99	45	Si	1.5
375.00	-130.86	-80.04	28.84	-11.02	215.90	44	Si	1.4

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-170.41	14.03	-14.80	-3.13	20.19	46	Si	3.6
375.00	-153.54	-16.89	17.27	-3.77	36.62	46	Si	3.0

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-163.53	13.75	-14.20	-3.02	19.69	52	Si	3.7
375.00	-146.65	-16.39	16.52	-3.62	35.39	52	Si	3.1

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-163.53	13.75	-14.20	0.02	6.80	16.99	19.65	9.77	0.005	0.009	52(Qp)	Si	32
0.00	-170.41	14.03	-14.80	0.02	6.80	17.01	19.61	9.98	0.006	0.010	46(Fr)	Si	42
375.00	-146.65	-16.39	16.52	0.03	9.69	24.21	19.57	18.59	0.010	0.018	52(Qp)	Si	17
375.00	-153.54	-16.89	17.27	0.03	9.68	24.20	19.55	19.26	0.011	0.018	46(Fr)	Si	22

Pilastro: 14 [37,114] Sez. R: By=30.00 cm Bz=60.00 cm L=359.00 cm Ln=359.00 cm L2=359.00 cm L3=359.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
359.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	372.65	2539.80	0.147	41.454	65.266

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-232.11	-27.21	18.76	-4.61	33.26	45	Si	3.2
0.00	-313.98	-28.46	18.13	-4.64	18.43	44	Si	3.2
359.00	-215.96	-55.25	30.23	-8.84	125.06	45	Si	1.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-328.56	0.53	-2.44	-1.81	-20.62	51	Si	6.2
0.00	-339.58	0.35	-2.52	-1.86	-21.42	46	Si	6.0
359.00	-312.41	-1.70	6.43	-2.14	-14.65	48	Si	5.2
359.00	-323.43	-1.46	6.67	-2.20	-15.33	46	Si	5.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-328.56	0.53	-2.44	-1.81	-20.62	52	Si	6.2
359.00	-312.41	-1.70	6.43	-2.14	-14.65	52	Si	5.2

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-328.56	0.53	-2.44	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-328.56	0.53	-2.44	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
359.00	-312.41	-1.70	6.43	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
359.00	-323.43	-1.46	6.67	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 15 [15,115] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	176.36	2539.80	0.069	50.691	94.872

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-119.50	-44.58	27.16	-7.86	139.03	45	Si	1.9
439.00	-142.62	-32.11	23.13	-6.02	87.96	44	Si	2.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-151.63	-1.57	-9.03	-1.61	-0.37	46	Si	7.0
439.00	-131.88	-1.98	21.14	-3.34	43.02	46	Si	3.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-145.99	-1.62	-8.63	-1.55	-0.38	52	Si	7.2
439.00	-126.23	-1.85	20.25	-3.20	41.20	52	Si	3.5

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-	-1.62	-8.63	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
	145.99												
0.00	-145.99	-1.62	-8.63	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-126.23	-1.85	20.25	0.03	10.18	25.45	20.80	27.00	0.016	0.027	52(Qp)	Si	11
439.00	-131.88	-1.98	21.14	0.03	10.18	25.45	20.80	28.16	0.017	0.028	46(Fr)	Si	14

Pilastro: 16 [16,116] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	295.82	2539.80	0.116	50.691	73.254

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-197.84	-8.82	25.26	-4.14	37.66	45	Si	3.6
439.00	-178.09	-63.29	15.05	-6.74	99.71	45	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-263.28	17.61	-1.37	-2.10	-6.75	51	Si	5.3
0.00	-271.42	17.88	-1.43	-2.16	-7.09	46	Si	5.2
439.00	-243.53	-12.91	0.45	-1.73	-9.00	48	Si	6.5
439.00	-251.66	-13.03	0.47	-1.77	-9.47	46	Si	6.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-263.28	17.61	-1.37	-2.10	-6.75	52	Si	5.3
439.00	-243.53	-12.91	0.45	-1.73	-9.00	52	Si	6.5

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-263.28	17.61	-1.37	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-263.28	17.61	-1.37	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-243.53	-12.91	0.45	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-251.66	-13.03	0.47	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 16 [116,216] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	127.56	2539.80	0.050	43.301	111.554

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-71.81	-6.77	33.38	-5.09	111.01	45	Si	2.9
375.00	-88.05	-81.91	5.66	-6.69	158.36	44	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-114.51	24.52	-2.50	-2.08	16.91	46	Si	5.4
375.00	-97.63	-28.68	3.48	-2.54	31.68	46	Si	4.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-110.16	23.87	-2.42	-2.03	16.78	52	Si	5.5
375.00	-93.28	-27.78	3.37	-2.46	31.14	52	Si	4.6

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-110.16	23.87	-2.42	0.02	10.41	26.02	18.19	9.71	0.005	0.009	52(Qp)	Si	35
0.00	-110.16	23.87	-2.42	0.02	10.41	26.02	18.19	9.71	0.005	0.009	51(Fr)	Si	47
375.00	-93.28	-27.78	3.37	0.03	11.98	29.96	19.03	17.96	0.010	0.017	52(Qp)	Si	18
375.00	-97.63	-28.68	3.48	0.03	11.93	29.82	19.00	18.17	0.010	0.017	46(Fr)	Si	24

Pilastro: 17 [17,35] Sez. R: By=30.00 cm Bz=70.00 cm L=267.00 cm Ln=267.00 cm L2=267.00 cm L3=267.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
267.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	319.98	2963.10	0.108	30.831	76.077

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-245.63	-30.83	23.86	-4.54	37.64	45	Si	3.3
0.00	-305.22	-26.75	29.34	-5.01	35.61	44	Si	3.0
267.00	-231.62	-53.28	13.99	-4.54	42.03	45	Si	3.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-278.48	29.41	19.43	-3.88	20.01	46	Si	2.9
267.00	-264.46	-10.44	-24.42	-3.60	18.71	46	Si	3.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-270.38	28.85	18.64	-3.76	19.24	52	Si	3.0
267.00	-256.36	-10.25	-23.49	-3.48	17.79	52	Si	3.2

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-270.38	28.85	18.64	0.01	6.84	17.09	18.19	8.81	0.005	0.008	52(Qp)	Si	39
0.00	-278.48	29.41	19.43	0.02	6.90	17.24	18.21	9.24	0.005	0.008	46(Fr)	Si	49
267.00	-256.36	-10.25	-23.49	0.02	11.01	27.52	17.37	11.81	0.006	0.010	52(Qp)	Si	30
267.00	-264.46	-10.44	-24.42	0.02	11.03	27.57	17.43	12.60	0.006	0.011	46(Fr)	Si	37

Pilastro: 17 [117,217] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	141.13	2963.10	0.048	43.301	114.554

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-134.46	-81.59	32.04	-9.14	173.50	44	Si	1.6
375.00	-109.82	37.97	-20.96	-4.94	80.25	30	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-116.86	-26.39	19.57	-4.01	57.82	46	Si	2.8
375.00	-97.17	32.89	-18.62	-4.34	70.29	46	Si	2.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-112.64	-25.34	18.94	-3.87	55.87	52	Si	2.9
375.00	-92.95	31.19	-17.84	-4.14	66.98	52	Si	2.7

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-112.64	-25.34	18.94	0.04	12.37	30.93	21.01	33.76	0.020	0.034	52(Qp)	Si	8.7
0.00	-116.86	-26.39	19.57	0.04	12.37	30.93	21.00	34.85	0.021	0.036	46(Fr)	Si	11
375.00	-92.95	31.19	-17.84	0.04	14.98	37.46	20.06	34.31	0.020	0.033	52(Qp)	Si	9.0
375.00	-97.17	32.89	-18.62	0.04	15.01	37.53	20.06	35.96	0.021	0.035	46(Fr)	Si	11

Pilastro: 17 [35,117] Sez. R: By=30.00 cm Bz=70.00 cm L=172.00 cm Ln=172.00 cm L2=172.00 cm L3=172.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
172.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	239.19	2963.10	0.081	19.861	87.991

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-184.74	-81.86	13.64	-6.36	103.69	45	Si	2.3
172.00	-175.71	-60.36	34.30	-7.99	130.56	45	Si	1.9
172.00	-220.76	-60.91	38.44	-8.45	127.95	44	Si	1.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-205.22	-6.46	-22.11	-3.12	21.65	46	Si	3.6
172.00	-196.19	7.29	9.59	-1.77	-0.26	46	Si	6.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-199.20	-6.20	-21.29	-3.00	20.47	52	Si	3.7
172.00	-190.17	7.33	9.00	-1.70	-0.41	52	Si	6.6

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-199.20	-6.20	-21.29	0.03	11.39	28.48	18.49	16.55	0.009	0.015	52(Qp)	Si	20
0.00	-205.22	-6.46	-22.11	0.03	11.41	28.53	18.54	17.55	0.009	0.016	46(Fr)	Si	25
172.00	-190.17	7.33	9.00	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
172.00	-196.19	7.29	9.59	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 18 [18,118] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	267.46	2539.80	0.105	50.691	77.040

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-178.44	-10.07	50.10	-5.21	65.41	45	Si	2.9
0.00	-230.84	-11.25	54.58	-5.62	58.55	44	Si	2.7
439.00	-158.69	-24.91	37.10	-6.67	96.66	45	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-246.24	-0.91	23.58	-2.30	-2.78	46	Si	4.9
439.00	-226.48	8.22	-16.87	-2.59	2.64	46	Si	4.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-239.16	-0.74	22.95	-2.22	-2.82	52	Si	5.0
439.00	-219.41	7.87	-16.39	-2.50	2.47	52	Si	4.5

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-239.16	-0.74	22.95	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-239.16	-0.74	22.95	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-219.41	7.87	-16.39	0.00	2.82	7.05	14.43	2.47	0.001	0.002	52(Qp)	Si	>100
439.00	-226.48	8.22	-16.87	0.00	2.85	7.11	14.47	2.64	0.001	0.002	46(Fr)	Si	>100

Pilastro: 18 [118,218] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01
375.00	AfSpigolo = 2.01	Afy = 4.02	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	126.53	2539.80	0.050	43.301	112.007

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-108.03	-26.78	39.39	-7.40	133.66	44	Si	2.0
375.00	-61.55	-18.88	29.13	-5.39	104.56	45	Si	2.8

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-114.83	-21.08	1.28	-3.29	48.83	46	Si	3.4
375.00	-97.95	23.77	-4.75	-4.00	72.54	46	Si	2.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-110.93	-20.17	1.40	-3.16	46.46	52	Si	3.5
375.00	-94.05	22.60	-4.81	-3.82	68.91	52	Si	2.9

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-110.93	-20.17	1.40	0.03	10.34	25.85	21.17	31.87	0.019	0.033	52(Qp)	Si	9.2

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
0.00	-114.83	-21.08	1.28	0.03	10.35	25.88	21.20	33.69	0.020	0.035	46(Fr)	Si	12
375.00	-94.05	22.60	-4.81	0.04	10.61	26.52	21.77	46.86	0.029	0.050	52(Qp)	Si	6.1
375.00	-97.95	23.77	-4.75	0.04	10.61	26.54	21.78	49.64	0.031	0.053	46(Fr)	Si	7.6

Pilastro: 19 [19,119] Sez. R: By=60.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	387.61	2539.80	0.153	50.691	63.994

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-270.38	-18.75	61.56	-6.63	67.87	45	Si	2.3
0.00	-353.08	-20.03	67.61	-7.15	59.26	44	Si	2.1
439.00	-250.63	-21.34	26.14	-4.49	29.67	45	Si	3.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-340.16	-3.83	34.84	-3.34	0.53	51	Si	3.4
0.00	-351.19	-4.01	35.68	-3.44	0.43	46	Si	3.3
439.00	-320.41	5.11	-28.34	-3.08	-0.69	48	Si	3.6
439.00	-331.43	5.27	-28.97	-3.17	-0.94	46	Si	3.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-340.16	-3.83	34.84	-3.34	0.53	52	Si	3.4
439.00	-320.41	5.11	-28.34	-3.08	-0.69	52	Si	3.6

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-340.16	-3.83	34.84	0.00	2.26	5.66	13.52	0.53	0.000	0.000	52(Qp)	Si	>100
0.00	-340.16	-3.83	34.84	0.00	2.26	5.66	13.52	0.53	0.000	0.000	51(Fr)	Si	>100
439.00	-320.41	5.11	-28.34	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-331.43	5.27	-28.97	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 19 [119,219] Sez. R: By=60.00 cm Bz=30.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01
375.00	AfSpigolo = 2.01	Afy = 8.04	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	120.92	2539.80	0.048	43.301	114.577

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-101.85	-22.25	53.16	-6.81	117.54	44	Si	2.2
375.00	-104.04	24.81	-30.46	-5.45	85.80	30	Si	2.7

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-110.47	-15.26	19.86	-3.35	39.09	46	Si	3.3
375.00	-93.60	21.99	-28.48	-4.94	77.75	46	Si	2.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-106.99	-14.68	19.58	-3.26	38.05	52	Si	3.4
375.00	-90.12	21.06	-27.82	-4.77	75.07	52	Si	2.3

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-106.99	-14.68	19.58	0.03	13.98	34.95	17.86	19.85	0.010	0.017	52(Qp)	Si	17
0.00	-110.47	-15.26	19.86	0.03	13.98	34.95	17.86	20.57	0.010	0.018	46(Fr)	Si	22
375.00	-90.12	21.06	-27.82	0.04	16.79	41.98	18.04	39.44	0.020	0.035	52(Qp)	Si	8.7
375.00	-93.60	21.99	-28.48	0.04	16.72	41.80	18.06	40.99	0.021	0.036	46(Fr)	Si	11

Pilastro: 20 [20,120] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	179.65	2539.80	0.071	50.691	94.000

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-117.23	-33.74	17.01	-5.22	77.43	45	Si	2.9
0.00	-162.36	-34.27	19.02	-5.40	66.61	44	Si	2.8
439.00	-97.48	-44.16	11.31	-5.18	91.14	45	Si	2.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-151.54	3.07	8.09	-1.59	-0.56	51	Si	7.1
0.00	-157.48	2.99	8.37	-1.64	-0.76	46	Si	6.8
439.00	-137.72	-11.96	-14.07	-2.91	23.76	46	Si	3.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-151.54	3.07	8.09	-1.59	-0.56	52	Si	7.1
439.00	-131.78	-11.59	-13.61	-2.82	23.39	52	Si	4.0

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-151.54	3.07	8.09	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-151.54	3.07	8.09	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-131.78	-11.59	-13.61	0.02	9.45	23.62	18.93	11.65	0.006	0.011	52(Qp)	Si	28
439.00	-137.72	-11.96	-14.07	0.02	9.42	23.55	18.86	11.71	0.006	0.011	46(Fr)	Si	37

Pilastro: 21 [21,121] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	165.17	2539.80	0.065	50.691	98.032

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-115.18	-39.64	26.85	-7.40	130.74	45	Si	2.0
439.00	-134.48	-40.80	29.83	-7.92	136.16	44	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-139.95	-2.32	-13.73	-2.22	12.22	46	Si	5.0
439.00	-120.20	-1.73	30.49	-4.75	90.35	46	Si	2.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-134.81	-2.27	-13.08	-2.12	11.37	52	Si	5.3
439.00	-115.05	-1.60	29.12	-4.53	86.10	52	Si	2.5

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-134.81	-2.27	-13.08	0.02	9.17	22.92	18.14	9.55	0.005	0.008	52(Qp)	Si	36
0.00	-139.95	-2.32	-13.73	0.02	9.20	22.99	18.23	10.36	0.005	0.009	46(Fr)	Si	44
439.00	-115.05	-1.60	29.12	0.04	10.64	26.60	21.84	62.53	0.039	0.066	52(Qp)	Si	4.5
439.00	-120.20	-1.73	30.49	0.04	10.64	26.61	21.85	65.60	0.041	0.070	46(Fr)	Si	5.7

Pilastro: 22 [22,122] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm

L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	326.83	2539.80	0.129	50.691	69.692

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-227.65	-41.44	5.07	-3.73	22.91	45	Si	4.0
0.00	-297.67	-42.13	6.47	-4.04	14.07	44	Si	3.7
439.00	-207.90	-45.21	29.10	-7.85	106.18	45	Si	1.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-286.53	-5.47	0.77	-1.68	-16.44	51	Si	6.7
0.00	-295.87	-5.57	0.95	-1.74	-16.87	46	Si	6.4
439.00	-276.11	0.35	-15.48	-2.72	-3.45	46	Si	4.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-286.53	-5.47	0.77	-1.68	-16.44	52	Si	6.7
439.00	-266.77	0.41	-14.68	-2.61	-3.60	52	Si	4.3

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-286.53	-5.47	0.77	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-286.53	-5.47	0.77	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-266.77	0.41	-14.68	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-276.11	0.35	-15.48	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 22 [122,222] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	121.80	2539.80	0.048	43.301	114.161

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-112.80	-37.02	32.18	-8.07	151.53	44	Si	1.9

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
375.00	-68.71	-27.32	5.07	-2.85	47.01	45	Si	5.2
375.00	-95.93	-28.36	5.49	-2.93	38.54	44	Si	5.1

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-106.29	3.90	14.35	-2.44	25.72	46	Si	4.6
375.00	-85.84	1.39	2.57	-0.70	-2.65	48	Si	16
375.00	-89.41	1.26	2.62	-0.72	-2.93	46	Si	16

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-102.71	3.62	13.62	-2.31	23.68	52	Si	4.9
375.00	-85.84	1.39	2.57	-0.70	-2.65	52	Si	16

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-102.71	3.62	13.62	0.03	9.88	24.71	20.07	16.53	0.009	0.016	52(Qp)	Si	19
0.00	-106.29	3.90	14.35	0.03	9.92	24.79	20.16	18.04	0.010	0.018	46(Fr)	Si	23
375.00	-85.84	1.39	2.57	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
375.00	-89.41	1.26	2.62	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

Pilastro: 23 [23,36] Sez. R: By=30.00 cm Bz=70.00 cm L=267.00 cm Ln=267.00 cm L2=267.00 cm L3=267.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
267.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	297.64	2963.10	0.100	30.831	78.880

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-229.49	-89.45	7.74	-5.93	88.51	45	Si	2.5
267.00	-215.47	-53.39	32.83	-7.21	100.80	45	Si	2.1
267.00	-270.94	-51.52	37.04	-7.52	93.58	44	Si	2.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-257.44	-36.98	-15.55	-3.79	22.22	46	Si	3.0
267.00	-243.43	13.07	17.64	-2.90	9.53	46	Si	3.9

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-249.94	-35.97	-15.09	-3.68	21.62	52	Si	3.0
267.00	-235.92	12.80	17.08	-2.81	9.30	52	Si	4.0

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-249.94	-35.97	-15.09	0.02	6.79	16.98	18.80	10.49	0.006	0.010	52(Qp)	Si	31
0.00	-257.44	-36.98	-15.55	0.02	6.79	16.97	18.79	10.77	0.006	0.010	46(Fr)	Si	41
267.00	-235.92	12.80	17.08	0.01	6.82	17.05	17.21	5.98	0.003	0.005	52(Qp)	Si	60
267.00	-243.43	13.07	17.64	0.01	6.83	17.08	17.21	6.15	0.003	0.005	46(Fr)	Si	78

Pilastro: 23 [123,223] Sez. R: By=30.00 cm Bz=70.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	140.83	2963.10	0.048	43.301	114.674

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-98.25	-59.63	24.24	-6.80	129.40	45	Si	2.2
0.00	-131.81	-59.90	27.17	-7.11	124.22	44	Si	2.1
375.00	-78.57	-48.26	22.36	-5.90	114.09	45	Si	2.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-118.61	1.33	13.09	-1.73	11.74	46	Si	6.5
375.00	-98.93	-8.89	-17.72	-2.76	39.20	46	Si	4.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-114.23	1.38	12.69	-1.68	11.60	52	Si	6.7
375.00	-94.54	-8.34	-16.97	-2.63	37.47	52	Si	4.3

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-114.23	1.38	12.69	0.03	11.48	28.69	18.72	10.72	0.006	0.010	52(Qp)	Si	31
0.00	-118.61	1.33	13.09	0.03	11.46	28.65	18.67	10.89	0.006	0.010	46(Fr)	Si	41
375.00	-94.54	-8.34	-16.97	0.04	12.32	30.81	20.89	27.40	0.016	0.028	52(Qp)	Si	11
375.00	-98.93	-8.89	-17.72	0.04	12.32	30.80	20.88	28.57	0.017	0.029	46(Fr)	Si	14

Pilastro: 23 [36,123] Sez. R: By=30.00 cm Bz=70.00 cm L=172.00 cm Ln=172.00 cm L2=172.00 cm L3=172.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
172.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	219.11	2963.10	0.074	19.861	91.935

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-169.85	-41.48	31.30	-6.42	98.09	45	Si	2.3
0.00	-210.47	-41.39	34.98	-6.81	96.13	44	Si	2.2
172.00	-160.82	-58.22	14.48	-5.10	73.23	45	Si	2.9

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-188.75	2.04	13.45	-1.90	2.27	46	Si	5.9
172.00	-179.72	-9.25	-28.64	-4.14	52.17	46	Si	2.7

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-183.34	2.03	12.95	-1.84	2.06	52	Si	6.1
172.00	-174.31	-9.24	-27.81	-4.03	50.94	52	Si	2.8

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-183.34	2.03	12.95	0.01	10.23	25.57	14.86	1.04	0.000	0.001	52(Qp)	Si	>100
0.00	-188.75	2.04	13.45	0.01	10.25	25.63	14.94	1.23	0.001	0.001	46(Fr)	Si	>100
172.00	-174.31	-9.24	-27.81	0.04	12.16	30.40	20.49	38.11	0.022	0.038	52(Qp)	Si	7.9
172.00	-179.72	-9.25	-28.64	0.04	12.16	30.39	20.49	39.13	0.023	0.039	46(Fr)	Si	10

Pilastro: 24 [24,124] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 4.02

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	153.28	2539.80	0.060	50.691	101.763

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-100.02	-36.76	27.87	-7.38	138.01	45	Si	2.0
439.00	-118.32	-34.25	24.22	-6.49	107.93	44	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-135.55	-4.62	-10.16	-1.85	5.64	46	Si	6.0
439.00	-115.80	6.83	22.88	-4.01	62.95	46	Si	2.8

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-130.54	-4.28	-9.62	-1.75	4.95	52	Si	6.4
439.00	-110.79	6.41	21.77	-3.81	59.52	52	Si	2.9

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-130.54	-4.28	-9.62	0.01	5.83	14.59	17.44	2.98	0.001	0.003	52(Qp)	Si	>100
0.00	-135.55	-4.62	-10.16	0.01	6.02	15.05	17.55	3.49	0.002	0.003	46(Fr)	Si	>100
439.00	-110.79	6.41	21.77	0.03	10.43	26.08	21.38	37.84	0.023	0.039	52(Qp)	Si	7.6
439.00	-115.80	6.83	22.88	0.03	10.44	26.10	21.39	40.01	0.024	0.042	46(Fr)	Si	9.6

Pilastro: 25 [25,125] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	426.37	2539.80	0.168	50.691	61.016

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-291.09	-47.87	10.92	-4.67	27.75	45	Si	3.2
0.00	-386.00	-52.87	11.83	-5.22	20.63	44	Si	2.9
439.00	-271.34	-36.82	31.10	-6.51	62.27	45	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-373.05	-18.68	-1.94	-2.64	-12.76	51	Si	4.2
0.00	-385.70	-19.37	-1.83	-2.71	-13.32	46	Si	4.1
439.00	-353.29	16.09	-0.96	-2.36	-13.81	48	Si	4.8
439.00	-365.94	16.64	-1.33	-2.47	-14.02	46	Si	4.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-373.05	-18.68	-1.94	-2.64	-12.76	52	Si	4.2
439.00	-353.29	16.09	-0.96	-2.36	-13.81	52	Si	4.8

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-373.05	-18.68	-1.94	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-373.05	-18.68	-1.94	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-353.29	16.09	-0.96	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
439.00	-	16.64	-1.33	0.00	0.00	0.00	0.00	0.00	0.000	0.000	46(Fr)	Si	>100

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
	365.94												

Pilastro: 25 [125,225] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 8.04

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	128.81	2539.80	0.051	43.301	111.012

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-87.79	-44.05	11.95	-4.72	80.40	45	Si	3.2
0.00	-116.61	-48.58	11.33	-4.92	77.27	44	Si	3.0
375.00	-70.91	-29.96	24.63	-5.44	96.68	45	Si	2.7
375.00	-110.90	27.70	28.34	-5.70	90.90	30	Si	2.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-116.38	-18.47	-12.45	-2.86	27.71	46	Si	3.9
375.00	-99.50	24.72	26.15	-5.20	83.71	46	Si	2.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-112.57	-17.84	-12.36	-2.80	27.61	52	Si	4.0
375.00	-95.70	23.73	25.42	-5.03	81.32	52	Si	2.2

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-112.57	-17.84	-12.36	0.02	11.17	27.93	18.29	14.96	0.008	0.013	52(Qp)	Si	23
0.00	-112.57	-17.84	-12.36	0.02	11.17	27.93	18.29	14.96	0.008	0.013	51(Fr)	Si	30
375.00	-95.70	23.73	25.42	0.04	14.58	36.46	18.98	53.54	0.029	0.049	52(Qp)	Si	6.1
375.00	-99.50	24.72	26.15	0.04	14.58	36.45	18.97	54.89	0.030	0.051	46(Fr)	Si	7.9

Pilastro: 26 [26,126] Sez. R: By=30.00 cm Bz=60.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
439.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	284.46	2539.80	0.112	50.691	74.701

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-166.71	-51.89	4.29	-4.32	57.00	45	Si	3.5
0.00	-223.08	-57.71	4.41	-4.73	50.30	44	Si	3.2
439.00	-146.95	-33.59	25.42	-6.06	86.42	45	Si	2.5

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-254.21	-25.69	-2.05	-2.47	-0.75	51	Si	4.5
0.00	-261.77	-26.51	-2.04	-2.54	-0.82	46	Si	4.4
439.00	-242.02	18.44	-8.99	-2.72	3.20	46	Si	4.1

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-254.21	-25.69	-2.05	-2.47	-0.75	52	Si	4.5
439.00	-234.45	17.88	-8.72	-2.64	3.13	52	Si	4.3

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-254.21	-25.69	-2.05	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-254.21	-25.69	-2.05	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-234.45	17.88	-8.72	0.00	3.26	8.16	14.41	3.13	0.001	0.002	52(Qp)	Si	>100
439.00	-242.02	18.44	-8.99	0.00	3.25	8.14	14.40	3.20	0.001	0.002	46(Fr)	Si	>100

Pilastro: 26 [126,226] Sez. R: By=30.00 cm Bz=60.00 cm L=375.00 cm Ln=375.00 cm L2=375.00 cm L3=375.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03
375.00	AfSpigolo = 2.01	Afy = 2.01	Afz = 6.03

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	104.13	2539.80	0.041	43.301	123.465

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-61.25	-37.02	28.94	-7.07	141.49	44	Si	2.1
375.00	-23.55	-45.26	20.19	-6.52	144.85	45	Si	2.3

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-95.82	-15.16	19.78	-3.91	58.79	46	Si	2.9
375.00	-78.95	18.36	-20.77	-4.33	73.67	46	Si	2.6

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-93.05	-14.65	19.21	-3.79	56.99	52	Si	3.0
375.00	-76.18	17.71	-20.03	-4.18	71.06	52	Si	2.7

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-93.05	-14.65	19.21	0.03	12.43	31.08	19.82	38.36	0.022	0.037	52(Qp)	Si	8.1
0.00	-95.82	-15.16	19.78	0.03	12.43	31.08	19.82	39.54	0.022	0.038	46(Fr)	Si	11
375.00	-76.18	17.71	-20.03	0.04	12.65	31.61	20.25	48.04	0.028	0.047	52(Qp)	Si	6.3
375.00	-78.95	18.36	-20.77	0.04	12.65	31.61	20.25	49.81	0.029	0.049	46(Fr)	Si	8.2

Pilastro: 27 [27,127] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	113.85	3386.40	0.034	50.691	136.346

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-106.98	-17.29	126.10	-8.03	193.51	44	Si	1.9
439.00	-56.59	-31.90	0.62	-3.70	101.39	45	Si	3.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-98.54	-9.18	24.93	-2.10	23.15	46	Si	5.3
439.00	-72.20	15.59	-4.23	-2.02	35.25	46	Si	5.5

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-95.38	-8.68	24.26	-2.01	22.03	52	Si	5.6
439.00	-69.04	14.81	-4.09	-1.92	33.40	52	Si	5.8

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-95.38	-8.68	24.26	0.04	11.24	28.09	20.89	10.11	0.006	0.010	52(Qp)	Si	29
0.00	-98.54	-9.18	24.93	0.04	11.28	28.19	20.93	10.68	0.006	0.011	46(Fr)	Si	37
439.00	-69.04	14.81	-4.09	0.05	12.57	31.42	22.83	23.60	0.015	0.026	52(Qp)	Si	11
439.00	-72.20	15.59	-4.23	0.05	12.57	31.43	22.84	24.97	0.016	0.028	46(Fr)	Si	14

Pilastro: 28 [28,128] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	113.02	3386.40	0.033	50.691	136.846

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-83.16	-11.85	3.33	-1.51	17.50	44	Si	9.9
439.00	-32.03	-34.77	46.79	-6.69	166.87	45	Si	2.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-103.22	-2.83	13.30	-0.92	1.49	46	Si	12
439.00	-76.88	10.80	-11.62	-1.76	21.90	46	Si	6.4

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-99.96	-2.51	13.04	-0.88	1.29	52	Si	13
439.00	-73.62	10.16	-11.36	-1.67	20.55	52	Si	6.7

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-99.96	-2.51	13.04	0.00	3.48	8.70	15.28	1.29	0.001	0.001	52(Qp)	Si	>100
0.00	-103.22	-2.83	13.30	0.00	3.61	9.02	15.48	1.49	0.001	0.001	46(Fr)	Si	>100
439.00	-73.62	10.16	-11.36	0.04	12.09	30.21	21.51	12.63	0.008	0.013	52(Qp)	Si	23
439.00	-76.88	10.80	-11.62	0.04	12.11	30.27	21.58	13.65	0.008	0.014	46(Fr)	Si	28

Pilastro: 29 [29,129] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	121.08	3386.40	0.036	50.691	132.211

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-83.57	-10.57	132.74	-7.36	200.79	45	Si	1.8
0.00	-110.65	-12.04	132.26	-7.54	190.68	44	Si	1.9
439.00	-57.23	-35.52	5.71	-4.41	119.37	45	Si	3.0
439.00	-84.31	-32.81	14.64	-4.60	105.12	44	Si	3.2

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-104.29	-2.07	8.04	-0.72	-1.22	51	Si	15
0.00	-107.86	-2.27	7.98	-0.75	-1.28	46	Si	15
439.00	-81.52	7.11	23.11	-1.80	20.73	46	Si	6.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-104.29	-2.07	8.04	-0.72	-1.22	52	Si	15
439.00	-77.95	6.75	21.94	-1.70	19.51	52	Si	6.6

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-104.29	-2.07	8.04	0.00	0.00	0.00	0.00	0.00	0.000	0.000	52(Qp)	Si	>100
0.00	-104.29	-2.07	8.04	0.00	0.00	0.00	0.00	0.00	0.000	0.000	51(Fr)	Si	>100
439.00	-77.95	6.75	21.94	0.04	11.50	28.74	21.06	9.18	0.006	0.009	52(Qp)	Si	32
439.00	-81.52	7.11	23.11	0.04	11.54	28.84	21.09	9.80	0.006	0.010	46(Fr)	Si	40

Pilastro: 30 [30,130] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
26	199.91	3386.40	0.059	50.691	102.894

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-130.35	-24.05	60.85	-5.79	100.82	45	Si	2.6
0.00	-179.70	-27.18	63.06	-6.11	93.57	44	Si	2.4
439.00	-104.01	-15.30	32.35	-3.27	47.99	45	Si	4.6

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-177.62	-9.82	5.64	-1.47	0.19	46	Si	7.6
439.00	-151.28	14.29	-25.07	-2.63	23.48	46	Si	4.3

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-171.12	-9.39	5.34	-1.40	0.09	52	Si	8.0
439.00	-144.78	13.74	-23.91	-2.52	22.57	52	Si	4.4

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-171.12	-9.39	5.34	0.00	2.16	5.39	16.09	0.09	0.000	0.000	52(Qp)	Si	>100
0.00	-177.62	-9.82	5.64	0.00	2.32	5.79	16.06	0.19	0.000	0.000	46(Fr)	Si	>100
439.00	-144.78	13.74	-23.91	0.03	9.10	22.75	21.52	12.23	0.008	0.013	52(Qp)	Si	23
439.00	-151.28	14.29	-25.07	0.03	9.07	22.67	21.52	12.69	0.008	0.013	46(Fr)	Si	30

Pilastro: 31 [31,131] Sez. R: By=80.00 cm Bz=30.00 cm L=439.00 cm Ln=439.00 cm L2=439.00 cm L3=439.00 cm Criterio: Pilastri

Zona	Armature		
cm	cmq	cmq	cmq
0.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Zona	Armature		
439.00	AfSpigolo = 2.01	Afy = 6.03	Afz = 2.01

Verifica snellezza: fcd=14.11 [MPa] - **Verificato**

Cb	N	fcd*Ac	ν	λmax	λlim
	kN	kN			
30	130.98	3386.40	0.039	50.691	127.120

Combinazione Rara: σca[MPa]=14.94 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-106.36	-25.58	-34.43	-4.72	86.15	44	Si	3.2
439.00	-50.55	-23.57	42.23	-5.05	111.74	45	Si	3.0

Combinazione Freq.: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-119.31	-15.83	-15.46	-2.49	28.77	46	Si	4.5
439.00	-92.97	19.72	-24.52	-3.51	60.01	46	Si	3.2

Combinazione QP: σca[MPa]=11.21 σfa[MPa]=360.00

X	N	My	Mz	σc	σf	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	MPa	MPa			
0.00	-115.42	-15.33	-15.45	-2.43	28.28	52	Si	4.6
439.00	-89.08	19.07	-23.29	-3.37	57.96	52	Si	3.3

Verifica aperture fessure:Wamm_Freq[mm]=0.400 Wamm_Qp[mm]=0.300

X	N	My	Mz	Act	Aft	pAft	$S_{r,max}$	σfmed	Wd	Wk	Cb	Ver.	Cs
cm	kN	kN*m	kN*m	m^2	cmq	cm	cm	MPa	mm	mm			
0.00	-115.42	-15.33	-15.45	0.04	12.00	30.00	21.27	17.44	0.011	0.018	52(Qp)	Si	17
0.00	-119.31	-15.83	-15.46	0.04	11.99	29.98	21.25	17.84	0.011	0.018	46(Fr)	Si	22
439.00	-89.08	19.07	-23.29	0.05	12.65	31.62	23.04	38.95	0.026	0.044	52(Qp)	Si	6.9
439.00	-92.97	19.72	-24.52	0.05	12.64	31.61	23.03	40.12	0.026	0.045	46(Fr)	Si	8.9

Verifica Solai

Simbologia Verifiche SLU:

Xcn [cm]	Ascissa lungo la campata netta
Ms [kN*m]	Momento inviluppo superiore
Mi [kN*m]	Momento inviluppo inferiore
T [kN]	Taglio di calcolo
Mrs [kN*m]	Momento resistente superiore
Mri [kN*m]	Momento resistente inferiore
Vres [kN]	Taglio resistente
Afs	Armatura superiore
Afi	Armatura inferiore
Fascia	Tipo di fascia: FP=fascia piena, FSP=fascia semipiena o nessuna

Simbologia Verifiche SLE:

T-C	Indice travetto - Indice campata

Verifiche tensioni e fessurazioni:

Xt [cm]	Ascissa della sezione riferita al sistema del travetto
M- [kN*m]	Momento superiore massimo di calcolo
M+ [kN*m]	Momento inferiore massimo di calcolo
Cb-	Combinazione di carico relativa di M-
Cb+	Combinazione di carico relativa di M+

M [kN*m]	Momento di calcolo
σc- [MPa]	Tensione nel cls compresso per effetto di M-
σc+ [MPa]	Tensione nel cls compresso per effetto di M+
σct- [MPa]	Tensione nel cls teso per effetto di M-
σct+ [MPa]	Tensione nel cls teso per effetto di M+
σf- [MPa]	Tensione nell'acciaio per effetto di M-
σf+ [MPa]	Tensione nell'acciaio per effetto di M+
σca [MPa]	Tensione ammissibile nel cls
σfa [MPa]	Tensione ammissibile nell'acciaio
σcta [MPa]	Tensione ammissibile a trazione (quando richiesto dalla verifica)
Act [m^2]	Area di calcestruzzo teso
Aft [cmq]	Area di acciaio teso
pAft [cm]	Perimetro area di acciaio teso
$S_{r,max}$ [cm]	Distanza massima delle fessure
σsfmed [MPa]	Tensione media dell'acciaio
Wd [mm]	Apertura delle fessure
Wk [mm]	Apertura caratteristica delle fessure
Wamm [mm]	Apertura ammissibile per la combinazione

Verifiche di deformabilità:

Tipo	Appoggiata (A), Sbalzo (S)
L [cm]	Luce ideale della campata
C	Coefficiente tension stiffening (0-1) (cfr. Circ. p.to C4.1.2.2.2)
ridE	Coefficiente di riduzione del modulo Em del cls (per Em cfr NTC 11.2.10.3)
Coeff	Coefficiente per cui dividere la Luce per ottenere la freccia ammissibile
famm [cm]	L/Coeff. Valore ammissibile della freccia
f [cm]	Valore calcolato della freccia (a meno di spostamenti rigidi)
CS	famm/f coefficiente di sicurezza
Seg	Segmento di trave
x1 [cm]	Ascissa iniziale
x2 [cm]	Ascissa finale
Lt [cm]	Lunghezza del tratto di campata
Mrfs [kN*m]	Momento di prima fessurazione superiore ([1])
Mrfi [kN*m]	Momento di prima fessurazione inferiore ([1])
EJ1i [kN*cm^4]	Rigidezza flessionale sezione integra per momento inferiore([1])
EJ2i [kN*cm^4]	Rigidezza flessionale sezione fessurata per momento inferiore([1])
EJ1s [kN*cm^4]	Rigidezza flessionale sezione integra per momento superiore([1])
EJ2s [kN*cm^4]	Rigidezza flessionale sezione fessurata per momento superiore([1])

([1]): I momenti di prima fessurazione sono ottenuti considerando la resistenza a trazione pari a fctm, le rigidezze flessionali EJ1, EJ2 sono calcolate considerando il modulo elastico del calcestruzzo a trazione uguale a quello a compressione e di valore pari ad Em*ridE, l'acciaio è stato omogeneizzato a calcestruzzo con n=Eacc/(Em*ridE). Il valore di fctm è opportunamente ridotto per i relativi coefficienti di sicurezza e fattori di confidenza. Il diagramma del momento (in genere parabolico) è assunto lineare in ognuno dei tratti.

Gruppo: Solaio terrazzo

Combinazioni di carico Stato Limite Ultimo (SLU)

I carichi fissi sono ottenuti da G=G1*1.30+G2*1.50

I carichi variabili sono ottenuti da QV=Q*1.50

I carichi utente sono considerati con il loro valore nominale

Combinazioni di carico Stato Limite di Esercizio (SLE)

I carichi fissi sono ottenuti da G=G1+G2

I carichi variabili sono ottenuti da:

-QV=Q per la combinazione Rara

-QV = Q * ψ1 per la combinazione Frequente

-QV = Q * ψ2 per la combinazione Quasi Permanente

I carichi utente sono considerati con il loro valore nominale

Combinazione n. 1: QV

Tipo: STR

Condizione di carico	Fattore di combinazione
G	1
User.	1
QV	1

Combinazione n. 2: QV C.Pari

Tipo: STR

Condizione di carico	Fattore di combinazione
G	1
User.	1
QV C.Pari	1

Combinazione n. 3: QV C.Disp.

Tipo: STR

Condizione di carico	Fattore di combinazione
G	1
User.	1
QV C.Disp.	1

Combinazione n. 4: QV App.2+3k

Tipo: STR

Condizione di carico	Fattore di combinazione
G	1
User.	1
QV App.2+3k	1

Combinazione n. 5: QV App.3+3k

Tipo: STR

Condizione di carico	Fattore di combinazione
G	1
User.	1
QV App.3+3k	1

Combinazione n. 6: QV App.4+3k

Tipo: STR

Condizione di carico	Fattore di combinazione
G	1
User.	1
QV App.4+3k	1

Combinazione n. 7: QV Rara

Tipo: SLE Rara

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV Rara	1

Combinazione n. 8: QV C.Pari Rara

Tipo: SLE Rara

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV C.Pari Rara	1

Combinazione n. 9: QV C.Disp. Rara

Tipo: SLE Rara

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV C.Disp. Rara	1

Combinazione n. 10: QV App.2+3k Rara
Tipo: SLE Rara

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.2+3k Rara	1

Combinazione n. 11: QV App.3+3k Rara
Tipo: SLE Rara

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.3+3k Rara	1

Combinazione n. 12: QV App.4+3k Rara
Tipo: SLE Rara

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.4+3k Rara	1

Combinazione n. 13: QV Freq
Tipo: SLE Freq.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV Freq	1

Combinazione n. 14: QV C.Pari Freq
Tipo: SLE Freq.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV C.Pari Freq	1

Combinazione n. 15: QV C.Disp. Freq
Tipo: SLE Freq.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV C.Disp. Freq	1

Combinazione n. 16: QV App.2+3k Freq
Tipo: SLE Freq.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.2+3k Freq	1

Combinazione n. 17: QV App.3+3k Freq
Tipo: SLE Freq.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.3+3k Freq	1

Combinazione n. 18: QV App.4+3k Freq
Tipo: SLE Freq.

Condizione di carico	Fattore di combinazione
User.	1

Condizione di carico	Fattore di combinazione
G_SLE	1
QV App.4+3k Freq	1

Combinazione n. 19: QV QP
Tipo: SLE Q.Perm.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV QP	1

Combinazione n. 20: QV C.Pari QP
Tipo: SLE Q.Perm.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV C.Pari QP	1

Combinazione n. 21: QV C.Disp. QP
Tipo: SLE Q.Perm.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV C.Disp. QP	1

Combinazione n. 22: QV App.2+3k QP
Tipo: SLE Q.Perm.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.2+3k QP	1

Combinazione n. 23: QV App.3+3k QP
Tipo: SLE Q.Perm.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.3+3k QP	1

Combinazione n. 24: QV App.4+3k QP
Tipo: SLE Q.Perm.

Condizione di carico	Fattore di combinazione
User.	1
G_SLE	1
QV App.4+3k QP	1

Solaio N.: 3
Base travetto = 10.00 cm

Criterio di verifica: Solaio in c.a.		
Rck	MPa	30.00
fyk	MPa	450.00
$\varepsilon c0 *10^3$		2
$\varepsilon cu *10^3$		3.5
$\varepsilon fu *10^3$		10
Ef	MPa	2.10E05
Copriferro di calcolo	cm	3.00
Copriferro di disegno	cm	3.00
fcd		0.85
γAcc		1.15
γCls		1.5

Percentuale max acciaio	%	1.8
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		Si
Verifica aperture fessure	MPa	No
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σCls	MPa	14.94
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σCls	MPa	11.21
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coeffcienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5

TRAVETTO N.: 1

CAMPATA N.: 1

Luce Netta L 400.86 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.43	9.93	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.86	-0.00	9.56	15.50	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.51	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 2

CAMPATA N.: 1

Luce Netta L 400.84 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.42	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.84	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 3

CAMPATA N.: 1

Luce Netta L 400.82 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.41	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.82	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 4

CAMPATA N.: 1

Luce Netta L 400.80 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.40	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.80	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 5

CAMPATA N.: 1
Luce Netta L 400.78 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.39	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.78	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 6

CAMPATA N.: 1

Luce Netta L 400.77 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.38	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.77	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 7

CAMPATA N.: 1

Luce Netta L 400.75 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.37	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.75	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 287.70 cm

Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 8

CAMPATA N.: 1
Luce Netta L 400.73 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.36	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.73	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.21	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm

Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 9

CAMPATA N.: 1
Luce Netta L 400.71 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.58	4.25	10.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
200.35	9.92	0.00	2.76	6.44	20.05	16.96	1Ø10	3Ø10		Si
400.71	-0.00	9.56	15.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 287.70 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	10.20	11.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
143.85	3.29	4.61	2.04	12.30	20.18	18.27	2Ø10	3Ø10		Si
287.70	-0.00	9.13	10.56	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 379.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.52	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
189.95	9.22	0.00	2.61	6.44	20.05	16.96	1Ø10	3Ø10		Si
379.90	1.51	3.82	10.09	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

Verifiche di Deformabilità
Combinazioni di tipo: Rara

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
				cm			cm	cm	
1-1	A	7	1.00	430.86	0.50	250.0	1.72	-0.43	4.0

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
1-1	A	12	1.00	430.86	0.50	250.0	1.72	-0.07	24
1-1	A	11	1.00	430.86	0.50	250.0	1.72	-0.07	26
1-1	A	10	1.00	430.86	0.50	250.0	1.72	-0.39	4.4
1-1	A	9	1.00	430.86	0.50	250.0	1.72	-0.48	3.6
1-1	A	8	1.00	430.86	0.50	250.0	1.72	-0.06	29
1-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
1-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
1-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
1-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
1-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
1-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
1-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
1-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
1-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
1-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
1-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
1-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
2-1	A	11	1.00	430.84	0.50	250.0	1.72	-0.07	26
2-1	A	8	1.00	430.84	0.50	250.0	1.72	-0.06	29
2-1	A	12	1.00	430.84	0.50	250.0	1.72	-0.07	24
2-1	A	7	1.00	430.84	0.50	250.0	1.72	-0.43	4.0
2-1	A	9	1.00	430.84	0.50	250.0	1.72	-0.48	3.6
2-1	A	10	1.00	430.84	0.50	250.0	1.72	-0.39	4.4
2-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
2-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
2-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
2-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
2-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
2-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
2-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
2-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
2-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
2-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
2-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
2-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
3-1	A	10	1.00	430.82	0.50	250.0	1.72	-0.39	4.4
3-1	A	11	1.00	430.82	0.50	250.0	1.72	-0.07	26
3-1	A	8	1.00	430.82	0.50	250.0	1.72	-0.06	29
3-1	A	12	1.00	430.82	0.50	250.0	1.72	-0.07	24
3-1	A	7	1.00	430.82	0.50	250.0	1.72	-0.43	4.0
3-1	A	9	1.00	430.82	0.50	250.0	1.72	-0.48	3.6
3-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
3-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
3-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
3-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
3-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
3-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
3-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
3-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
3-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
3-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
3-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
3-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
4-1	A	12	1.00	430.80	0.50	250.0	1.72	-0.07	24
4-1	A	11	1.00	430.80	0.50	250.0	1.72	-0.07	26
4-1	A	10	1.00	430.80	0.50	250.0	1.72	-0.39	4.4
4-1	A	7	1.00	430.80	0.50	250.0	1.72	-0.43	4.0
4-1	A	8	1.00	430.80	0.50	250.0	1.72	-0.06	29
4-1	A	9	1.00	430.80	0.50	250.0	1.72	-0.48	3.6
4-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
4-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
4-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
4-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
4-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
4-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
4-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
4-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
4-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
4-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
4-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
4-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
5-1	A	12	1.00	430.78	0.50	250.0	1.72	-0.07	24
5-1	A	8	1.00	430.78	0.50	250.0	1.72	-0.06	29
5-1	A	7	1.00	430.78	0.50	250.0	1.72	-0.43	4.0
5-1	A	11	1.00	430.78	0.50	250.0	1.72	-0.07	26
5-1	A	9	1.00	430.78	0.50	250.0	1.72	-0.48	3.6
5-1	A	10	1.00	430.78	0.50	250.0	1.72	-0.39	4.4
5-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
5-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
5-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
5-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
5-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
5-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
5-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
5-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
5-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
5-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
5-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
5-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
6-1	A	12	1.00	430.77	0.50	250.0	1.72	-0.07	24
6-1	A	10	1.00	430.77	0.50	250.0	1.72	-0.39	4.4
6-1	A	7	1.00	430.77	0.50	250.0	1.72	-0.43	4.0
6-1	A	11	1.00	430.77	0.50	250.0	1.72	-0.07	26
6-1	A	9	1.00	430.77	0.50	250.0	1.72	-0.48	3.6
6-1	A	8	1.00	430.77	0.50	250.0	1.72	-0.06	29
6-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
6-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
6-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
6-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
6-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
6-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
6-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
6-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
6-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
6-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
6-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
6-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
7-1	A	12	1.00	430.75	0.50	250.0	1.72	-0.07	24
7-1	A	7	1.00	430.75	0.50	250.0	1.72	-0.43	4.0
7-1	A	9	1.00	430.75	0.50	250.0	1.72	-0.48	3.6
7-1	A	10	1.00	430.75	0.50	250.0	1.72	-0.39	4.4
7-1	A	8	1.00	430.75	0.50	250.0	1.72	-0.06	29
7-1	A	11	1.00	430.75	0.50	250.0	1.72	-0.07	26
7-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
7-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
7-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
7-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
7-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
7-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
7-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
7-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
7-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
7-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
7-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
7-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
8-1	A	8	1.00	430.73	0.50	250.0	1.72	-0.06	29
8-1	A	12	1.00	430.73	0.50	250.0	1.72	-0.07	24
8-1	A	11	1.00	430.73	0.50	250.0	1.72	-0.07	26

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
8-1	A	9	1.00	430.73	0.50	250.0	1.72	-0.48	3.6
8-1	A	7	1.00	430.73	0.50	250.0	1.72	-0.43	4.0
8-1	A	10	1.00	430.73	0.50	250.0	1.72	-0.39	4.4
8-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
8-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
8-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
8-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
8-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
8-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
8-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
8-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
8-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
8-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28
8-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
8-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
9-1	A	12	1.00	430.71	0.50	250.0	1.72	-0.07	24
9-1	A	8	1.00	430.71	0.50	250.0	1.72	-0.06	29
9-1	A	7	1.00	430.71	0.50	250.0	1.72	-0.43	4.0
9-1	A	10	1.00	430.71	0.50	250.0	1.72	-0.39	4.4
9-1	A	9	1.00	430.71	0.50	250.0	1.72	-0.48	3.6
9-1	A	11	1.00	430.71	0.50	250.0	1.72	-0.07	26
9-2	A	7	1.00	317.70	0.50	250.0	1.27	0.03	37
9-2	A	10	1.00	317.70	0.50	250.0	1.27	0.02	62
9-2	A	8	1.00	317.70	0.50	250.0	1.27	0.00	>100
9-2	A	11	1.00	317.70	0.50	250.0	1.27	0.02	70
9-2	A	12	1.00	317.70	0.50	250.0	1.27	0.02	68
9-2	A	9	1.00	317.70	0.50	250.0	1.27	0.05	25
9-3	A	9	1.00	409.90	0.50	250.0	1.64	-0.39	4.2
9-3	A	10	1.00	409.90	0.50	250.0	1.64	-0.06	29
9-3	A	11	1.00	409.90	0.50	250.0	1.64	-0.30	5.5
9-3	A	7	1.00	409.90	0.50	250.0	1.64	-0.33	4.9
9-3	A	8	1.00	409.90	0.50	250.0	1.64	-0.05	34
9-3	A	12	1.00	409.90	0.50	250.0	1.64	-0.06	28

Proprietà geometriche delle sezioni delle campate

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
	cm	cm	cm	cmq	cmq	cm	cm	cm	cm
1-1	0.00	15.00	15.00	--	--	--	--	--	--
1-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
1-1	45.00	129.99	84.99	2.36	2.36	10.00	21.00	50.00	4.00
1-1	129.99	175.35	45.35	1.57	2.36	10.00	21.00	50.00	4.00
1-1	175.35	339.26	163.92	0.79	2.36	10.00	21.00	50.00	4.00
1-1	339.26	385.86	46.60	1.57	2.36	10.00	21.00	50.00	4.00
1-1	385.86	415.86	30.00	2.36	2.36	50.00	25.00	--	--
1-1	415.86	430.86	15.00	--	--	--	--	--	--
1-2	430.86	445.86	15.00	--	--	--	--	--	--
1-2	445.86	475.86	30.00	2.36	2.36	50.00	25.00	--	--
1-2	475.86	484.68	8.82	2.36	2.36	10.00	21.00	50.00	4.00
1-2	484.68	703.56	218.88	1.57	2.36	10.00	21.00	50.00	4.00
1-2	703.56	733.56	30.00	1.57	2.36	50.00	25.00	--	--
1-2	733.56	748.56	15.00	--	--	--	--	--	--
1-3	748.56	763.56	15.00	--	--	--	--	--	--
1-3	763.56	775.18	11.61	3.14	2.36	50.00	25.00	--	--
1-3	775.18	793.56	18.39	2.36	2.36	50.00	25.00	--	--
1-3	793.56	835.49	41.92	2.36	2.36	10.00	21.00	50.00	4.00
1-3	835.49	877.53	42.05	1.57	2.36	10.00	21.00	50.00	4.00
1-3	877.53	1036.48	158.95	0.79	2.36	10.00	21.00	50.00	4.00
1-3	1036.48	1113.46	76.98	1.57	2.36	10.00	21.00	50.00	4.00
1-3	1113.46	1143.46	30.00	2.36	2.36	50.00	25.00	--	--
1-3	1143.46	1158.46	15.00	--	--	--	--	--	--
2-1	0.00	15.00	15.00	--	--	--	--	--	--
2-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
2-1	45.00	129.99	84.99	2.36	2.36	10.00	21.00	50.00	4.00
2-1	129.99	175.34	45.35	1.57	2.36	10.00	21.00	50.00	4.00
2-1	175.34	339.25	163.91	0.79	2.36	10.00	21.00	50.00	4.00
2-1	339.25	385.84	46.60	1.57	2.36	10.00	21.00	50.00	4.00
2-1	385.84	415.84	30.00	2.36	2.36	50.00	25.00	--	--
2-1	415.84	430.84	15.00	--	--	--	--	--	--
2-2	430.84	445.84	15.00	--	--	--	--	--	--
2-2	445.84	475.84	30.00	2.36	2.36	50.00	25.00	--	--
2-2	475.84	484.64	8.80	2.36	2.36	10.00	21.00	50.00	4.00
2-2	484.64	703.54	218.90	1.57	2.36	10.00	21.00	50.00	4.00
2-2	703.54	733.54	30.00	1.57	2.36	50.00	25.00	--	--
2-2	733.54	748.54	15.00	--	--	--	--	--	--
2-3	748.54	763.54	15.00	--	--	--	--	--	--
2-3	763.54	775.16	11.61	3.14	2.36	50.00	25.00	--	--
2-3	775.16	793.54	18.39	2.36	2.36	50.00	25.00	--	--
2-3	793.54	835.47	41.92	2.36	2.36	10.00	21.00	50.00	4.00
2-3	835.47	877.51	42.05	1.57	2.36	10.00	21.00	50.00	4.00
2-3	877.51	1036.46	158.95	0.79	2.36	10.00	21.00	50.00	4.00
2-3	1036.46	1113.44	76.98	1.57	2.36	10.00	21.00	50.00	4.00
2-3	1113.44	1143.44	30.00	2.36	2.36	50.00	25.00	--	--
2-3	1143.44	1158.44	15.00	--	--	--	--	--	--
3-1	0.00	15.00	15.00	--	--	--	--	--	--
3-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
3-1	45.00	129.98	84.98	2.36	2.36	10.00	21.00	50.00	4.00
3-1	129.98	175.33	45.35	1.57	2.36	10.00	21.00	50.00	4.00
3-1	175.33	339.23	163.90	0.79	2.36	10.00	21.00	50.00	4.00
3-1	339.23	385.82	46.59	1.57	2.36	10.00	21.00	50.00	4.00
3-1	385.82	415.82	30.00	2.36	2.36	50.00	25.00	--	--
3-1	415.82	430.82	15.00	--	--	--	--	--	--
3-2	430.82	445.82	15.00	--	--	--	--	--	--
3-2	445.82	475.82	30.00	2.36	2.36	50.00	25.00	--	--
3-2	475.82	484.60	8.78	2.36	2.36	10.00	21.00	50.00	4.00
3-2	484.60	703.52	218.92	1.57	2.36	10.00	21.00	50.00	4.00
3-2	703.52	733.52	30.00	1.57	2.36	50.00	25.00	--	--
3-2	733.52	748.52	15.00	--	--	--	--	--	--
3-3	748.52	763.52	15.00	--	--	--	--	--	--
3-3	763.52	775.14	11.61	3.14	2.36	50.00	25.00	--	--
3-3	775.14	793.52	18.39	2.36	2.36	50.00	25.00	--	--
3-3	793.52	835.45	41.93	2.36	2.36	10.00	21.00	50.00	4.00
3-3	835.45	877.49	42.04	1.57	2.36	10.00	21.00	50.00	4.00
3-3	877.49	1036.44	158.95	0.79	2.36	10.00	21.00	50.00	4.00
3-3	1036.44	1113.42	76.98	1.57	2.36	10.00	21.00	50.00	4.00
3-3	1113.42	1143.42	30.00	2.36	2.36	50.00	25.00	--	--
3-3	1143.42	1158.42	15.00	--	--	--	--	--	--
4-1	0.00	15.00	15.00	--	--	--	--	--	--
4-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
4-1	45.00	129.97	84.97	2.36	2.36	10.00	21.00	50.00	4.00
4-1	129.97	175.32	45.35	1.57	2.36	10.00	21.00	50.00	4.00
4-1	175.32	339.21	163.89	0.79	2.36	10.00	21.00	50.00	4.00
4-1	339.21	385.80	46.59	1.57	2.36	10.00	21.00	50.00	4.00
4-1	385.80	415.80	30.00	2.36	2.36	50.00	25.00	--	--
4-1	415.80	430.80	15.00	--	--	--	--	--	--
4-2	430.80	445.80	15.00	--	--	--	--	--	--
4-2	445.80	475.80	30.00	2.36	2.36	50.00	25.00	--	--
4-2	475.80	484.56	8.75	2.36	2.36	10.00	21.00	50.00	4.00
4-2	484.56	703.50	218.95	1.57	2.36	10.00	21.00	50.00	4.00
4-2	703.50	733.50	30.00	1.57	2.36	50.00	25.00	--	--
4-2	733.50	748.50	15.00	--	--	--	--	--	--
4-3	748.50	763.50	15.00	--	--	--	--	--	--
4-3	763.50	775.12	11.62	3.14	2.36	50.00	25.00	--	--
4-3	775.12	793.50	18.38	2.36	2.36	50.00	25.00	--	--
4-3	793.50	835.43	41.93	2.36	2.36	10.00	21.00	50.00	4.00
4-3	835.43	877.47	42.04	1.57	2.36	10.00	21.00	50.00	4.00
4-3	877.47	1036.43	158.95	0.79	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
4-3	1036.43	1113.40	76.98	1.57	2.36	10.00	21.00	50.00	4.00
4-3	1113.40	1143.40	30.00	2.36	2.36	50.00	25.00	--	--
4-3	1143.40	1158.40	15.00	--	--	--	--	--	--
5-1	0.00	15.00	15.00	--	--	--	--	--	--
5-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
5-1	45.00	129.96	84.96	2.36	2.36	10.00	21.00	50.00	4.00
5-1	129.96	175.31	45.35	1.57	2.36	10.00	21.00	50.00	4.00
5-1	175.31	339.20	163.88	0.79	2.36	10.00	21.00	50.00	4.00
5-1	339.20	385.78	46.59	1.57	2.36	10.00	21.00	50.00	4.00
5-1	385.78	415.78	30.00	2.36	2.36	50.00	25.00	--	--
5-1	415.78	430.78	15.00	--	--	--	--	--	--
5-2	430.78	445.78	15.00	--	--	--	--	--	--
5-2	445.78	475.78	30.00	2.36	2.36	50.00	25.00	--	--
5-2	475.78	484.52	8.73	2.36	2.36	10.00	21.00	50.00	4.00
5-2	484.52	703.48	218.97	1.57	2.36	10.00	21.00	50.00	4.00
5-2	703.48	733.48	30.00	1.57	2.36	50.00	25.00	--	--
5-2	733.48	748.48	15.00	--	--	--	--	--	--
5-3	748.48	763.48	15.00	--	--	--	--	--	--
5-3	763.48	775.10	11.62	3.14	2.36	50.00	25.00	--	--
5-3	775.10	793.48	18.38	2.36	2.36	50.00	25.00	--	--
5-3	793.48	835.41	41.93	2.36	2.36	10.00	21.00	50.00	4.00
5-3	835.41	877.45	42.04	1.57	2.36	10.00	21.00	50.00	4.00
5-3	877.45	1036.41	158.95	0.79	2.36	10.00	21.00	50.00	4.00
5-3	1036.41	1113.38	76.98	1.57	2.36	10.00	21.00	50.00	4.00
5-3	1113.38	1143.38	30.00	2.36	2.36	50.00	25.00	--	--
5-3	1143.38	1158.38	15.00	--	--	--	--	--	--
6-1	0.00	15.00	15.00	--	--	--	--	--	--
6-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
6-1	45.00	129.96	84.96	2.36	2.36	10.00	21.00	50.00	4.00
6-1	129.96	175.31	45.35	1.57	2.36	10.00	21.00	50.00	4.00
6-1	175.31	339.18	163.87	0.79	2.36	10.00	21.00	50.00	4.00
6-1	339.18	385.77	46.58	1.57	2.36	10.00	21.00	50.00	4.00
6-1	385.77	415.77	30.00	2.36	2.36	50.00	25.00	--	--
6-1	415.77	430.77	15.00	--	--	--	--	--	--
6-2	430.77	445.77	15.00	--	--	--	--	--	--
6-2	445.77	475.77	30.00	2.36	2.36	50.00	25.00	--	--
6-2	475.77	484.47	8.71	2.36	2.36	10.00	21.00	50.00	4.00
6-2	484.47	703.47	218.99	1.57	2.36	10.00	21.00	50.00	4.00
6-2	703.47	733.47	30.00	1.57	2.36	50.00	25.00	--	--
6-2	733.47	748.47	15.00	--	--	--	--	--	--
6-3	748.47	763.47	15.00	--	--	--	--	--	--
6-3	763.47	775.08	11.62	3.14	2.36	50.00	25.00	--	--
6-3	775.08	793.47	18.38	2.36	2.36	50.00	25.00	--	--
6-3	793.47	835.39	41.93	2.36	2.36	10.00	21.00	50.00	4.00
6-3	835.39	877.44	42.04	1.57	2.36	10.00	21.00	50.00	4.00
6-3	877.44	1036.39	158.95	0.79	2.36	10.00	21.00	50.00	4.00
6-3	1036.39	1113.37	76.98	1.57	2.36	10.00	21.00	50.00	4.00
6-3	1113.37	1143.37	30.00	2.36	2.36	50.00	25.00	--	--
6-3	1143.37	1158.37	15.00	--	--	--	--	--	--
7-1	0.00	15.00	15.00	--	--	--	--	--	--
7-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
7-1	45.00	129.95	84.95	2.36	2.36	10.00	21.00	50.00	4.00
7-1	129.95	175.30	45.35	1.57	2.36	10.00	21.00	50.00	4.00
7-1	175.30	339.16	163.87	0.79	2.36	10.00	21.00	50.00	4.00
7-1	339.16	385.75	46.58	1.57	2.36	10.00	21.00	50.00	4.00
7-1	385.75	415.75	30.00	2.36	2.36	50.00	25.00	--	--
7-1	415.75	430.75	15.00	--	--	--	--	--	--
7-2	430.75	445.75	15.00	--	--	--	--	--	--
7-2	445.75	475.75	30.00	2.36	2.36	50.00	25.00	--	--
7-2	475.75	484.43	8.69	2.36	2.36	10.00	21.00	50.00	4.00
7-2	484.43	703.45	219.01	1.57	2.36	10.00	21.00	50.00	4.00
7-2	703.45	733.45	30.00	1.57	2.36	50.00	25.00	--	--
7-2	733.45	748.45	15.00	--	--	--	--	--	--
7-3	748.45	763.45	15.00	--	--	--	--	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
7-3	763.45	775.06	11.62	3.14	2.36	50.00	25.00	--	--
7-3	775.06	793.45	18.38	2.36	2.36	50.00	25.00	--	--
7-3	793.45	835.38	41.93	2.36	2.36	10.00	21.00	50.00	4.00
7-3	835.38	877.42	42.04	1.57	2.36	10.00	21.00	50.00	4.00
7-3	877.42	1036.37	158.95	0.79	2.36	10.00	21.00	50.00	4.00
7-3	1036.37	1113.35	76.98	1.57	2.36	10.00	21.00	50.00	4.00
7-3	1113.35	1143.35	30.00	2.36	2.36	50.00	25.00	--	--
7-3	1143.35	1158.35	15.00	--	--	--	--	--	--
8-1	-0.00	15.00	15.00	--	--	--	--	--	--
8-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
8-1	45.00	129.94	84.94	2.36	2.36	10.00	21.00	50.00	4.00
8-1	129.94	175.29	45.35	1.57	2.36	10.00	21.00	50.00	4.00
8-1	175.29	339.15	163.86	0.79	2.36	10.00	21.00	50.00	4.00
8-1	339.15	385.73	46.58	1.57	2.36	10.00	21.00	50.00	4.00
8-1	385.73	415.73	30.00	2.36	2.36	50.00	25.00	--	--
8-1	415.73	430.73	15.00	--	--	--	--	--	--
8-2	430.73	445.73	15.00	--	--	--	--	--	--
8-2	445.73	475.73	30.00	2.36	2.36	50.00	25.00	--	--
8-2	475.73	484.39	8.66	2.36	2.36	10.00	21.00	50.00	4.00
8-2	484.39	703.43	219.04	1.57	2.36	10.00	21.00	50.00	4.00
8-2	703.43	733.43	30.00	1.57	2.36	50.00	25.00	--	--
8-2	733.43	748.43	15.00	--	--	--	--	--	--
8-3	748.43	763.43	15.00	--	--	--	--	--	--
8-3	763.43	775.05	11.62	3.14	2.36	50.00	25.00	--	--
8-3	775.05	793.43	18.38	2.36	2.36	50.00	25.00	--	--
8-3	793.43	835.36	41.93	2.36	2.36	10.00	21.00	50.00	4.00
8-3	835.36	877.40	42.04	1.57	2.36	10.00	21.00	50.00	4.00
8-3	877.40	1036.35	158.95	0.79	2.36	10.00	21.00	50.00	4.00
8-3	1036.35	1113.33	76.98	1.57	2.36	10.00	21.00	50.00	4.00
8-3	1113.33	1143.33	30.00	2.36	2.36	50.00	25.00	--	--
8-3	1143.33	1158.33	15.00	--	--	--	--	--	--
9-1	-0.00	15.00	15.00	--	--	--	--	--	--
9-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
9-1	45.00	129.94	84.94	2.36	2.36	10.00	21.00	50.00	4.00
9-1	129.94	175.28	45.35	1.57	2.36	10.00	21.00	50.00	4.00
9-1	175.28	339.13	163.85	0.79	2.36	10.00	21.00	50.00	4.00
9-1	339.13	385.71	46.57	1.57	2.36	10.00	21.00	50.00	4.00
9-1	385.71	415.71	30.00	2.36	2.36	50.00	25.00	--	--
9-1	415.71	430.71	15.00	--	--	--	--	--	--
9-2	430.71	445.71	15.00	--	--	--	--	--	--
9-2	445.71	475.71	30.00	2.36	2.36	50.00	25.00	--	--
9-2	475.71	484.35	8.64	2.36	2.36	10.00	21.00	50.00	4.00
9-2	484.35	703.41	219.06	1.57	2.36	10.00	21.00	50.00	4.00
9-2	703.41	733.41	30.00	1.57	2.36	50.00	25.00	--	--
9-2	733.41	748.41	15.00	--	--	--	--	--	--
9-3	748.41	763.41	15.00	--	--	--	--	--	--
9-3	763.41	775.03	11.62	3.14	2.36	50.00	25.00	--	--
9-3	775.03	793.41	18.38	2.36	2.36	50.00	25.00	--	--
9-3	793.41	835.34	41.93	2.36	2.36	10.00	21.00	50.00	4.00
9-3	835.34	877.38	42.04	1.57	2.36	10.00	21.00	50.00	4.00
9-3	877.38	1036.33	158.95	0.79	2.36	10.00	21.00	50.00	4.00
9-3	1036.33	1113.31	76.98	1.57	2.36	10.00	21.00	50.00	4.00
9-3	1113.31	1143.31	30.00	2.36	2.36	50.00	25.00	--	--
9-3	1143.31	1158.31	15.00	--	--	--	--	--	--

Proprietà di inerzia delle sezioni delle campate

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	cm	cm	cm	kN*m	kN*m	kN*cm^4	kN*cm^4	kN*cm^4	kN*cm^4
1-1	0.00	15.00	15.00	Tratto infinitamente rigido					
1-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	45.00	129.99	84.99	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-1	129.99	175.35	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
1-1	175.35	339.26	163.92	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-1	339.26	385.86	46.60	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	385.86	415.86	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	415.86	430.86	15.00	Tratto infinitamente rigido					
1-2	430.86	445.86	15.00	Tratto infinitamente rigido					
1-2	445.86	475.86	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-2	475.86	484.68	8.82	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-2	484.68	703.56	218.88	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-2	703.56	733.56	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
1-2	733.56	748.56	15.00	Tratto infinitamente rigido					
1-3	748.56	763.56	15.00	Tratto infinitamente rigido					
1-3	763.56	775.18	11.61	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
1-3	775.18	793.56	18.39	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-3	793.56	835.49	41.92	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-3	835.49	877.53	42.05	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-3	877.53	1036.48	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-3	1036.48	1113.46	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-3	1113.46	1143.46	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-3	1143.46	1158.46	15.00	Tratto infinitamente rigido					
2-1	0.00	15.00	15.00	Tratto infinitamente rigido					
2-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	45.00	129.99	84.99	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-1	129.99	175.34	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	175.34	339.25	163.91	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-1	339.25	385.84	46.60	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	385.84	415.84	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	415.84	430.84	15.00	Tratto infinitamente rigido					
2-2	430.84	445.84	15.00	Tratto infinitamente rigido					
2-2	445.84	475.84	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-2	475.84	484.64	8.80	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-2	484.64	703.54	218.90	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-2	703.54	733.54	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
2-2	733.54	748.54	15.00	Tratto infinitamente rigido					
2-3	748.54	763.54	15.00	Tratto infinitamente rigido					
2-3	763.54	775.16	11.61	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
2-3	775.16	793.54	18.39	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-3	793.54	835.47	41.92	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-3	835.47	877.51	42.05	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-3	877.51	1036.46	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-3	1036.46	1113.44	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-3	1113.44	1143.44	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-3	1143.44	1158.44	15.00	Tratto infinitamente rigido					
3-1	0.00	15.00	15.00	Tratto infinitamente rigido					
3-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-1	45.00	129.98	84.98	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-1	129.98	175.33	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	175.33	339.23	163.90	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-1	339.23	385.82	46.59	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	385.82	415.82	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-1	415.82	430.82	15.00	Tratto infinitamente rigido					
3-2	430.82	445.82	15.00	Tratto infinitamente rigido					
3-2	445.82	475.82	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-2	475.82	484.60	8.78	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-2	484.60	703.52	218.92	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-2	703.52	733.52	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
3-2	733.52	748.52	15.00	Tratto infinitamente rigido					

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
3-3	748.52	763.52	15.00	Tratto infinitamente rigido					
3-3	763.52	775.14	11.61	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
3-3	775.14	793.52	18.39	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-3	793.52	835.45	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-3	835.45	877.49	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-3	877.49	1036.44	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-3	1036.44	1113.42	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-3	1113.42	1143.42	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-3	1143.42	1158.42	15.00	Tratto infinitamente rigido					
4-1	0.00	15.00	15.00	Tratto infinitamente rigido					
4-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	45.00	129.97	84.97	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-1	129.97	175.32	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	175.32	339.21	163.89	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-1	339.21	385.80	46.59	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	385.80	415.80	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	415.80	430.80	15.00	Tratto infinitamente rigido					
4-2	430.80	445.80	15.00	Tratto infinitamente rigido					
4-2	445.80	475.80	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-2	475.80	484.56	8.75	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-2	484.56	703.50	218.95	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-2	703.50	733.50	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
4-2	733.50	748.50	15.00	Tratto infinitamente rigido					
4-3	748.50	763.50	15.00	Tratto infinitamente rigido					
4-3	763.50	775.12	11.62	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
4-3	775.12	793.50	18.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-3	793.50	835.43	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-3	835.43	877.47	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-3	877.47	1036.43	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-3	1036.43	1113.40	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-3	1113.40	1143.40	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-3	1143.40	1158.40	15.00	Tratto infinitamente rigido					
5-1	0.00	15.00	15.00	Tratto infinitamente rigido					
5-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-1	45.00	129.96	84.96	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-1	129.96	175.31	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	175.31	339.20	163.88	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-1	339.20	385.78	46.59	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	385.78	415.78	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-1	415.78	430.78	15.00	Tratto infinitamente rigido					
5-2	430.78	445.78	15.00	Tratto infinitamente rigido					
5-2	445.78	475.78	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-2	475.78	484.52	8.73	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-2	484.52	703.48	218.97	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-2	703.48	733.48	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
5-2	733.48	748.48	15.00	Tratto infinitamente rigido					
5-3	748.48	763.48	15.00	Tratto infinitamente rigido					
5-3	763.48	775.10	11.62	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
5-3	775.10	793.48	18.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-3	793.48	835.41	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-3	835.41	877.45	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-3	877.45	1036.41	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-3	1036.41	1113.38	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-3	1113.3	1143.3	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	8	8							
5-3	1143.38	1158.38	15.00	Tratto infinitamente rigido					
6-1	0.00	15.00	15.00	Tratto infinitamente rigido					
6-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-1	45.00	129.96	84.96	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-1	129.96	175.31	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-1	175.31	339.18	163.87	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
6-1	339.18	385.77	46.58	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-1	385.77	415.77	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-1	415.77	430.77	15.00	Tratto infinitamente rigido					
6-2	430.77	445.77	15.00	Tratto infinitamente rigido					
6-2	445.77	475.77	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-2	475.77	484.47	8.71	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-2	484.47	703.47	218.99	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-2	703.47	733.47	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
6-2	733.47	748.47	15.00	Tratto infinitamente rigido					
6-3	748.47	763.47	15.00	Tratto infinitamente rigido					
6-3	763.47	775.08	11.62	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
6-3	775.08	793.47	18.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-3	793.47	835.39	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-3	835.39	877.44	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-3	877.44	1036.39	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
6-3	1036.39	1113.37	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-3	1113.37	1143.37	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-3	1143.37	1158.37	15.00	Tratto infinitamente rigido					
7-1	0.00	15.00	15.00	Tratto infinitamente rigido					
7-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-1	45.00	129.95	84.95	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-1	129.95	175.30	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-1	175.30	339.16	163.87	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-1	339.16	385.75	46.58	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-1	385.75	415.75	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-1	415.75	430.75	15.00	Tratto infinitamente rigido					
7-2	430.75	445.75	15.00	Tratto infinitamente rigido					
7-2	445.75	475.75	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-2	475.75	484.43	8.69	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-2	484.43	703.45	219.01	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-2	703.45	733.45	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
7-2	733.45	748.45	15.00	Tratto infinitamente rigido					
7-3	748.45	763.45	15.00	Tratto infinitamente rigido					
7-3	763.45	775.06	11.62	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
7-3	775.06	793.45	18.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-3	793.45	835.38	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-3	835.38	877.42	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-3	877.42	1036.37	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-3	1036.37	1113.35	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-3	1113.35	1143.35	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-3	1143.35	1158.35	15.00	Tratto infinitamente rigido					
8-1	-0.00	15.00	15.00	Tratto infinitamente rigido					
8-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-1	45.00	129.94	84.94	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-1	129.94	175.29	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-1	175.29	339.15	163.86	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-1	339.15	385.73	46.58	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-1	385.73	415.73	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
8-1	415.73	430.73	15.00	Tratto infinitamente rigido					
8-2	430.73	445.73	15.00	Tratto infinitamente rigido					
8-2	445.73	475.73	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-2	475.73	484.39	8.66	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-2	484.39	703.43	219.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-2	703.43	733.43	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
8-2	733.43	748.43	15.00	Tratto infinitamente rigido					
8-3	748.43	763.43	15.00	Tratto infinitamente rigido					
8-3	763.43	775.05	11.62	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
8-3	775.05	793.43	18.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-3	793.43	835.36	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-3	835.36	877.40	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-3	877.40	1036.35	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-3	1036.35	1113.33	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-3	1113.33	1143.33	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-3	1143.33	1158.33	15.00	Tratto infinitamente rigido					
9-1	-0.00	15.00	15.00	Tratto infinitamente rigido					
9-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-1	45.00	129.94	84.94	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
9-1	129.94	175.28	45.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-1	175.28	339.13	163.85	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-1	339.13	385.71	46.57	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-1	385.71	415.71	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-1	415.71	430.71	15.00	Tratto infinitamente rigido					
9-2	430.71	445.71	15.00	Tratto infinitamente rigido					
9-2	445.71	475.71	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-2	475.71	484.35	8.64	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
9-2	484.35	703.41	219.06	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-2	703.41	733.41	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
9-2	733.41	748.41	15.00	Tratto infinitamente rigido					
9-3	748.41	763.41	15.00	Tratto infinitamente rigido					
9-3	763.41	775.03	11.62	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
9-3	775.03	793.41	18.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-3	793.41	835.34	41.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
9-3	835.34	877.38	42.04	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-3	877.38	1036.33	158.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-3	1036.33	1113.31	76.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-3	1113.31	1143.31	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-3	1143.31	1158.31	15.00	Tratto infinitamente rigido					

Tensioni di esercizio combinazione Rara

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	175.35	7.18	--	-2.85	149.56	--	--	14.94	360.00	9	8	Si
1-2	733.56	--	6.36	--	--	-2.88	197.08	14.94	360.00	10	11	Si
1-3	991.50	6.63	--	-2.63	138.11	--	--	14.94	360.00	9	8	Si
2-1	175.34	7.18	--	-2.85	149.55	--	--	14.94	360.00	9	8	Si
2-2	733.54	--	6.36	--	--	-2.88	197.08	14.94	360.00	10	11	Si
2-3	991.48	6.63	--	-2.63	138.11	--	--	14.94	360.00	9	8	Si
3-1	175.33	7.18	--	-2.85	149.53	--	--	14.94	360.00	9	8	Si
3-2	733.52	--	6.36	--	--	-2.88	197.08	14.94	360.00	10	11	Si
3-3	991.46	6.63	--	-2.63	138.11	--	--	14.94	360.00	9	8	Si
4-1	175.32	7.18	--	-2.85	149.52	--	--	14.94	360.00	9	8	Si
4-2	733.50	--	6.36	--	--	-2.88	197.08	14.94	360.00	10	11	Si

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
4-3	991.44	6.63	--	-2.63	138.11	--	--	14.94	360.00	9	8	Si
5-1	175.31	7.18	--	-2.85	149.51	--	--	14.94	360.00	9	8	Si
5-2	733.48	--	6.36	--	--	-2.88	197.09	14.94	360.00	10	11	Si
5-3	991.42	6.63	--	-2.63	138.10	--	--	14.94	360.00	9	8	Si
6-1	175.31	7.18	--	-2.85	149.50	--	--	14.94	360.00	9	8	Si
6-2	733.47	--	6.36	--	--	-2.88	197.09	14.94	360.00	10	11	Si
6-3	991.41	6.63	--	-2.63	138.10	--	--	14.94	360.00	9	8	Si
7-1	175.30	7.18	--	-2.85	149.48	--	--	14.94	360.00	9	8	Si
7-2	733.45	--	6.36	--	--	-2.88	197.09	14.94	360.00	10	11	Si
7-3	991.39	6.63	--	-2.63	138.10	--	--	14.94	360.00	9	8	Si
8-1	175.29	7.18	--	-2.85	149.47	--	--	14.94	360.00	9	8	Si
8-2	733.43	--	6.36	--	--	-2.88	197.09	14.94	360.00	10	11	Si
8-3	991.37	6.63	--	-2.63	138.10	--	--	14.94	360.00	9	8	Si
9-1	175.28	7.18	--	-2.85	149.46	--	--	14.94	360.00	9	8	Si
9-2	733.41	--	6.36	--	--	-2.88	197.10	14.94	360.00	10	11	Si
9-3	991.35	6.63	--	-2.63	138.10	--	--	14.94	360.00	9	8	Si

Tensioni di esercizio combinazione QP

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	175.35	5.81	--	-2.30	120.88	--	--	11.21	360.00	21	20	Si
1-2	733.56	--	5.09	--	--	-2.31	157.72	11.21	360.00	22	23	Si
1-3	991.50	5.35	--	-2.12	111.42	--	--	11.21	360.00	21	20	Si
2-1	175.34	5.81	--	-2.30	120.87	--	--	11.21	360.00	21	20	Si
2-2	733.54	--	5.09	--	--	-2.31	157.72	11.21	360.00	22	23	Si
2-3	991.48	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
3-1	175.33	5.81	--	-2.30	120.86	--	--	11.21	360.00	21	20	Si
3-2	733.52	--	5.09	--	--	-2.31	157.72	11.21	360.00	22	23	Si
3-3	991.46	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
4-1	175.32	5.81	--	-2.30	120.85	--	--	11.21	360.00	21	20	Si
4-2	733.50	--	5.09	--	--	-2.31	157.72	11.21	360.00	22	23	Si
4-3	991.44	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
5-1	175.31	5.81	--	-2.30	120.84	--	--	11.21	360.00	21	20	Si
5-2	733.48	--	5.09	--	--	-2.31	157.73	11.21	360.00	22	23	Si
5-3	991.42	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
6-1	175.31	5.80	--	-2.30	120.83	--	--	11.21	360.00	21	20	Si
6-2	733.47	--	5.09	--	--	-2.31	157.73	11.21	360.00	22	23	Si
6-3	991.41	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
7-1	175.30	5.80	--	-2.30	120.82	--	--	11.21	360.00	21	20	Si
7-2	733.45	--	5.09	--	--	-2.31	157.73	11.21	360.00	22	23	Si
7-3	991.39	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
8-1	175.29	5.80	--	-2.30	120.81	--	--	11.21	360.00	21	20	Si
8-2	733.43	--	5.09	--	--	-2.31	157.73	11.21	360.00	22	23	Si
8-3	991.37	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si
9-1	175.28	5.80	--	-2.30	120.80	--	--	11.21	360.00	21	20	Si
9-2	733.41	--	5.09	--	--	-2.31	157.73	11.21	360.00	22	23	Si
9-3	991.35	5.35	--	-2.12	111.41	--	--	11.21	360.00	21	20	Si

Verifica a decompressione o Verifica formazione fessure

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	
1-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
1-2	445.86	--	7.12	--	--	-2.69	0.00	2.13	Si
1-3	763.56	--	5.92	--	--	-1.99	0.00	2.13	Si
2-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
2-2	445.84	--	7.12	--	--	-2.69	0.00	2.13	Si
2-3	763.54	--	5.92	--	--	-1.99	0.00	2.13	Si
3-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
3-2	445.82	--	7.12	--	--	-2.69	0.00	2.13	Si
3-3	763.52	--	5.92	--	--	-1.99	0.00	2.13	Si

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
4-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
4-2	445.80	--	7.12	--	--	-2.69	0.00	2.13	Si
4-3	763.50	--	5.92	--	--	-1.99	0.00	2.13	Si
5-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
5-2	445.78	--	7.12	--	--	-2.69	0.00	2.13	Si
5-3	763.48	--	5.92	--	--	-1.99	0.00	2.13	Si
6-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
6-2	445.77	--	7.12	--	--	-2.69	0.00	2.13	Si
6-3	763.47	--	5.92	--	--	-1.99	0.00	2.13	Si
7-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
7-2	445.75	--	7.12	--	--	-2.69	0.00	2.13	Si
7-3	763.45	--	5.92	--	--	-1.99	0.00	2.13	Si
8-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
8-2	445.73	--	7.11	--	--	-2.69	0.00	2.13	Si
8-3	763.43	--	5.92	--	--	-1.99	0.00	2.13	Si
9-1	15.00	1.10	--	-0.42	0.00	--	--	2.13	Si
9-2	445.71	--	7.11	--	--	-2.69	0.00	2.13	Si
9-3	763.41	--	5.92	--	--	-1.99	0.00	2.13	Si

Solaio N.: intermedio
Base travetto = 10.00 cm

Criterio di verifica: Solaio in c.a.		
Rck	MPa	30.00
fyk	MPa	450.00
$\varepsilon c0 *10^3$		2
$\varepsilon cu *10^3$		3.5
$\varepsilon fu *10^3$		10
Ef	MPa	2.10E05
Copriferro di calcolo	cm	3.00
Copriferro di disegno	cm	3.00
fcd		0.85
γAcc		1.15
γCls		1.5
Percentuale max acciaio	%	1.8
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		Si
Verifica aperture fessure	MPa	No
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σCls	MPa	14.94
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σCls	MPa	11.21
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coeffcienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5

TRAVETTO N.: 1

CAMPATA N.: 1

Luce Netta L	529.46 cm
Altezza solaio H	25.00 cm
Altezza soletta s	4.00 cm
Tipo	Gettato in Opera
Fascia piena a sinistra	30.00 cm

Fascia piena a destra 38.02 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.16	13.35	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
264.73	15.88	0.00	3.46	0.57	19.66	15.41		3Ø10		Si
529.46	-0.00	16.39	19.68	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 396.98 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	17.13	14.75	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.49	6.04	5.27	2.58	12.30	20.18	18.27	2Ø10	3Ø10		Si
396.98	-0.00	14.12	14.46	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.56	18.19	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.75	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.52	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 2

CAMPATA N.: 1

Luce Netta L 528.94 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 37.84 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.15	13.34	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
264.47	15.85	0.00	3.45	0.57	19.66	15.41		3Ø10		Si
528.94	-0.00	16.36	19.66	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 396.99 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	17.10	14.74	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.49	6.04	5.26	2.57	12.30	20.18	18.27	2Ø10	3Ø10		Si
396.99	-0.00	14.12	14.46	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.56	18.19	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.75	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.52	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 3

CAMPATA N.: 1
Luce Netta L 528.42 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 37.67 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.13	13.33	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
264.21	15.82	0.00	3.45	0.57	19.66	15.41		3Ø10		Si
528.42	-0.00	16.33	19.65	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	17.06	14.73	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.50	6.04	5.24	2.57	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.00	-0.00	14.12	14.47	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.57	18.19	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.74	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.52	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 4

CAMPATA N.: 1

Luce Netta L 527.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 37.51 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.12	13.32	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.95	15.80	0.00	3.45	0.57	19.66	15.41		3Ø10		Si
527.90	-0.00	16.30	19.63	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.01 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	17.03	14.72	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.51	6.04	5.23	2.56	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.01	-0.00	14.13	14.48	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.57	18.19	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.74	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.51	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 5

CAMPATA N.: 1

Luce Netta L 527.39 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm

Fascia piena a destra 37.41 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.10	13.30	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.69	15.77	0.00	3.45	0.57	19.66	15.41		3Ø10		Si
527.39	-0.00	16.27	19.61	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.03 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	17.00	14.71	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.51	6.04	5.22	2.55	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.03	-0.00	14.13	14.48	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.58	18.19	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.74	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.51	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 6

CAMPATA N.: 1

Luce Netta L 526.87 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 37.32 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.99	7.09	13.29	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.43	15.74	0.00	3.44	0.57	19.66	15.41		3Ø10		Si
526.87	-0.00	16.24	19.59	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.04 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	16.97	14.71	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.52	6.04	5.20	2.54	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.04	-0.00	14.14	14.49	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.58	18.20	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.73	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.51	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 7

CAMPATA N.: 1

Luce Netta L 526.40 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 37.23 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.99	7.08	13.28	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.20	15.72	0.00	3.44	0.57	19.66	15.41		3Ø10		Si
526.40	-0.00	16.21	19.57	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	16.95	14.70	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.50	6.04	5.19	2.53	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.00	-0.00	14.14	14.49	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.58	18.20	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.73	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.51	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 8

CAMPATA N.: 1

Luce Netta L 525.89 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 37.14 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.99	7.06	13.27	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
262.95	15.69	0.00	3.44	0.57	19.66	15.41		3Ø10		Si
525.89	-0.00	16.19	19.56	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	16.92	14.69	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.50	6.04	5.18	2.52	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.00	-0.00	14.14	14.50	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.59	18.20	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.72	0.00	3.26	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.51	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 9

CAMPATA N.: 1

Luce Netta L 521.81 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm

Fascia piena a destra 36.60 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.20	6.95	13.11	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
260.90	15.54	0.00	3.48	0.57	19.66	15.41		3Ø10		Si
521.81	-0.00	16.05	19.47	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	16.78	14.64	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
198.50	6.04	5.12	2.48	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.00	-0.00	14.16	14.53	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.61	18.20	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.70	0.00	3.27	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.88	5.85	12.50	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 10

CAMPATA N.: 1

Luce Netta L 471.82 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.49	5.69	11.75	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.91	13.16	0.00	3.39	6.44	20.05	16.96	1Ø10	3Ø10		Si
471.82	-0.00	13.67	17.85	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	14.26	13.87	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
198.50	6.04	4.07	1.71	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.00	-0.00	14.50	15.00	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	14.01	18.28	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.35	0.00	3.35	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.85	5.85	12.36	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 11

CAMPATA N.: 1
Luce Netta L 421.84 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.24	4.54	10.54	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
210.92	10.83	0.00	3.20	6.44	20.05	16.96	1Ø10	3Ø10		Si
421.84	-0.00	11.44	16.13	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	11.89	13.15	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
198.50	6.04	3.05	1.79	6.44	20.05	16.96	1Ø10	3Ø10		Si
397.00	-0.00	14.81	15.45	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 3
Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	14.38	18.36	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.00	13.01	0.00	3.43	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.83	5.85	12.22	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 12

CAMPATA N.: 1

Luce Netta L 371.85 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.98	3.53	9.31	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
185.92	8.69	0.00	3.06	6.44	20.05	16.96	1Ø10	3Ø10		Si
371.85	-0.00	9.61	14.46	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	9.89	12.54	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
198.50	6.04	2.17	2.17	12.30	20.18	18.27	2Ø10	3Ø10		Si
397.00	-0.00	15.07	15.82	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	14.68	18.42	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
235.00	12.72	0.00	3.49	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.82	5.85	12.11	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 13

CAMPATA N.: 1

Luce Netta L 321.86 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm

Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.71	2.65	8.07	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
160.93	6.76	0.00	2.99	6.44	20.05	16.96	1Ø10	3Ø10		Si
321.86	-0.00	8.16	12.85	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	8.29	12.04	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
198.50	6.04	1.42	2.46	18.13	20.26	18.97	3Ø10	3Ø10		Si
397.00	-0.00	15.28	16.12	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	14.93	18.47	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
235.00	12.47	0.00	3.54	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.80	5.85	12.01	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 14

CAMPATA N.: 1

Luce Netta L 271.88 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.44	1.89	6.81	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
135.94	5.04	0.00	3.03	6.44	20.05	16.96	1Ø10	3Ø10		Si
271.88	-0.00	7.11	11.36	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	7.06	11.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
198.50	6.04	0.81	2.68	6.44	20.05	16.96	1Ø10	3Ø10		Si
397.00	-0.00	15.43	16.33	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 3

Luce Netta L 470.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	15.11	18.51	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
235.00	12.27	0.00	3.58	6.44	20.05	16.96	1Ø10	3Ø10		Si
470.00	1.79	5.85	11.93	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 15

CAMPATA N.: 1

Luce Netta L 221.89 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	0.76	1.26	4.38	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
110.94	2.16	0.46	3.24	12.30	20.18	18.27	2Ø10	3Ø10		Si
221.89	-0.00	6.52	10.04	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 397.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	6.30	11.50	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
198.50	6.90	0.00	1.00	6.44	20.05	16.96	1Ø10	3Ø10		Si
397.00	-0.00	9.41	13.17	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

Verifiche di Deformabilità
Combinazioni di tipo: Rara

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
				cm			cm	cm	
1-1	A	7	1.00	559.46	0.50	250.0	2.24	-1.41	1.6
1-1	A	12	1.00	559.46	0.50	250.0	2.24	-0.77	2.9
1-1	A	11	1.00	559.46	0.50	250.0	2.24	-0.70	3.2
1-1	A	10	1.00	559.46	0.50	250.0	2.24	-1.34	1.7

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
1-1	A	9	1.00	559.46	0.50	250.0	2.24	-1.54	1.5
1-1	A	8	1.00	559.46	0.50	250.0	2.24	-0.65	3.4
1-2	A	8	1.00	426.98	0.50	250.0	1.71	0.01	>100
1-2	A	9	1.00	426.98	0.50	250.0	1.71	0.13	14
1-2	A	7	1.00	426.98	0.50	250.0	1.71	0.09	20
1-2	A	10	1.00	426.98	0.50	250.0	1.71	0.06	29
1-2	A	12	1.00	426.98	0.50	250.0	1.71	0.04	39
1-2	A	11	1.00	426.98	0.50	250.0	1.71	0.03	54
1-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.32	6.3
1-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
1-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	10
1-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.2
1-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
1-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
2-1	A	7	1.00	558.94	0.50	250.0	2.24	-1.41	1.6
2-1	A	10	1.00	558.94	0.50	250.0	2.24	-1.33	1.7
2-1	A	8	1.00	558.94	0.50	250.0	2.24	-0.65	3.4
2-1	A	12	1.00	558.94	0.50	250.0	2.24	-0.76	2.9
2-1	A	9	1.00	558.94	0.50	250.0	2.24	-1.53	1.5
2-1	A	11	1.00	558.94	0.50	250.0	2.24	-0.69	3.2
2-2	A	7	1.00	426.99	0.50	250.0	1.71	0.08	20
2-2	A	10	1.00	426.99	0.50	250.0	1.71	0.06	29
2-2	A	9	1.00	426.99	0.50	250.0	1.71	0.13	14
2-2	A	11	1.00	426.99	0.50	250.0	1.71	0.03	54
2-2	A	8	1.00	426.99	0.50	250.0	1.71	0.01	>100
2-2	A	12	1.00	426.99	0.50	250.0	1.71	0.04	39
2-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
2-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.2
2-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
2-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.32	6.3
2-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
2-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	10
3-1	A	9	1.00	558.42	0.50	250.0	2.23	-1.52	1.5
3-1	A	10	1.00	558.42	0.50	250.0	2.23	-1.32	1.7
3-1	A	11	1.00	558.42	0.50	250.0	2.23	-0.69	3.2
3-1	A	12	1.00	558.42	0.50	250.0	2.23	-0.76	2.9
3-1	A	7	1.00	558.42	0.50	250.0	2.23	-1.40	1.6
3-1	A	8	1.00	558.42	0.50	250.0	2.23	-0.65	3.5
3-2	A	10	1.00	427.00	0.50	250.0	1.71	0.06	29
3-2	A	11	1.00	427.00	0.50	250.0	1.71	0.03	54
3-2	A	7	1.00	427.00	0.50	250.0	1.71	0.08	20
3-2	A	12	1.00	427.00	0.50	250.0	1.71	0.04	39
3-2	A	9	1.00	427.00	0.50	250.0	1.71	0.13	14
3-2	A	8	1.00	427.00	0.50	250.0	1.71	0.01	>100
3-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
3-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.2
3-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
3-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.32	6.3
3-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	10
3-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
4-1	A	10	1.00	557.91	0.50	250.0	2.23	-1.32	1.7
4-1	A	11	1.00	557.91	0.50	250.0	2.23	-0.69	3.3
4-1	A	8	1.00	557.91	0.50	250.0	2.23	-0.64	3.5
4-1	A	12	1.00	557.91	0.50	250.0	2.23	-0.76	2.9
4-1	A	9	1.00	557.91	0.50	250.0	2.23	-1.52	1.5
4-1	A	7	1.00	557.91	0.50	250.0	2.23	-1.40	1.6
4-2	A	9	1.00	427.01	0.50	250.0	1.71	0.12	14
4-2	A	11	1.00	427.01	0.50	250.0	1.71	0.03	54
4-2	A	12	1.00	427.01	0.50	250.0	1.71	0.04	39
4-2	A	8	1.00	427.01	0.50	250.0	1.71	0.01	>100
4-2	A	10	1.00	427.01	0.50	250.0	1.71	0.06	29
4-2	A	7	1.00	427.01	0.50	250.0	1.71	0.08	20
4-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
4-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
4-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.31	6.4
4-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.2
4-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	10
4-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
5-1	A	11	1.00	557.39	0.50	250.0	2.23	-0.68	3.3
5-1	A	9	1.00	557.39	0.50	250.0	2.23	-1.51	1.5
5-1	A	8	1.00	557.39	0.50	250.0	2.23	-0.64	3.5
5-1	A	7	1.00	557.39	0.50	250.0	2.23	-1.39	1.6
5-1	A	12	1.00	557.39	0.50	250.0	2.23	-0.75	3.0
5-1	A	10	1.00	557.39	0.50	250.0	2.23	-1.31	1.7
5-2	A	7	1.00	427.03	0.50	250.0	1.71	0.08	21
5-2	A	9	1.00	427.03	0.50	250.0	1.71	0.12	14
5-2	A	12	1.00	427.03	0.50	250.0	1.71	0.04	40
5-2	A	11	1.00	427.03	0.50	250.0	1.71	0.03	54
5-2	A	8	1.00	427.03	0.50	250.0	1.71	0.01	>100
5-2	A	10	1.00	427.03	0.50	250.0	1.71	0.06	30
5-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.31	6.4
5-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.2
5-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
5-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
5-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
5-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	10
6-1	A	9	1.00	556.87	0.50	250.0	2.23	-1.51	1.5
6-1	A	11	1.00	556.87	0.50	250.0	2.23	-0.68	3.3
6-1	A	8	1.00	556.87	0.50	250.0	2.23	-0.63	3.5
6-1	A	12	1.00	556.87	0.50	250.0	2.23	-0.75	3.0
6-1	A	7	1.00	556.87	0.50	250.0	2.23	-1.39	1.6
6-1	A	10	1.00	556.87	0.50	250.0	2.23	-1.31	1.7
6-2	A	11	1.00	427.04	0.50	250.0	1.71	0.03	55
6-2	A	9	1.00	427.04	0.50	250.0	1.71	0.12	14
6-2	A	10	1.00	427.04	0.50	250.0	1.71	0.06	30
6-2	A	12	1.00	427.04	0.50	250.0	1.71	0.04	40
6-2	A	8	1.00	427.04	0.50	250.0	1.71	0.01	>100
6-2	A	7	1.00	427.04	0.50	250.0	1.71	0.08	21
6-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.2
6-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
6-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
6-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
6-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.31	6.4
6-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	10
7-1	A	10	1.00	556.40	0.50	250.0	2.23	-1.30	1.7
7-1	A	12	1.00	556.40	0.50	250.0	2.23	-0.75	3.0
7-1	A	11	1.00	556.40	0.50	250.0	2.23	-0.67	3.3
7-1	A	8	1.00	556.40	0.50	250.0	2.23	-0.63	3.5
7-1	A	7	1.00	556.40	0.50	250.0	2.23	-1.38	1.6
7-1	A	9	1.00	556.40	0.50	250.0	2.23	-1.50	1.5
7-2	A	9	1.00	427.00	0.50	250.0	1.71	0.12	14
7-2	A	7	1.00	427.00	0.50	250.0	1.71	0.08	21
7-2	A	12	1.00	427.00	0.50	250.0	1.71	0.04	40
7-2	A	8	1.00	427.00	0.50	250.0	1.71	0.01	>100
7-2	A	10	1.00	427.00	0.50	250.0	1.71	0.06	30
7-2	A	11	1.00	427.00	0.50	250.0	1.71	0.03	55
7-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
7-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.31	6.4
7-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
7-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
7-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	11
7-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.3
8-1	A	8	1.00	555.90	0.50	250.0	2.22	-0.63	3.5
8-1	A	9	1.00	555.90	0.50	250.0	2.22	-1.50	1.5
8-1	A	12	1.00	555.90	0.50	250.0	2.22	-0.74	3.0
8-1	A	10	1.00	555.90	0.50	250.0	2.22	-1.30	1.7
8-1	A	11	1.00	555.90	0.50	250.0	2.22	-0.67	3.3
8-1	A	7	1.00	555.90	0.50	250.0	2.22	-1.37	1.6

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
8-2	A	11	1.00	427.00	0.50	250.0	1.71	0.03	55
8-2	A	12	1.00	427.00	0.50	250.0	1.71	0.04	40
8-2	A	10	1.00	427.00	0.50	250.0	1.71	0.06	30
8-2	A	9	1.00	427.00	0.50	250.0	1.71	0.12	14
8-2	A	7	1.00	427.00	0.50	250.0	1.71	0.08	21
8-2	A	8	1.00	427.00	0.50	250.0	1.71	0.01	>100
8-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.31	6.4
8-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
8-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.28	7.3
8-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
8-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	11
8-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
9-1	A	10	1.00	553.60	0.50	250.0	2.21	-1.27	1.7
9-1	A	12	1.00	553.60	0.50	250.0	2.21	-0.73	3.1
9-1	A	11	1.00	553.60	0.50	250.0	2.21	-0.66	3.4
9-1	A	7	1.00	553.60	0.50	250.0	2.21	-1.35	1.6
9-1	A	8	1.00	553.60	0.50	250.0	2.21	-0.61	3.6
9-1	A	9	1.00	553.60	0.50	250.0	2.21	-1.47	1.5
9-2	A	11	1.00	427.00	0.50	250.0	1.71	0.03	56
9-2	A	10	1.00	427.00	0.50	250.0	1.71	0.05	32
9-2	A	12	1.00	427.00	0.50	250.0	1.71	0.04	41
9-2	A	8	1.00	427.00	0.50	250.0	1.71	0.01	>100
9-2	A	7	1.00	427.00	0.50	250.0	1.71	0.08	21
9-2	A	9	1.00	427.00	0.50	250.0	1.71	0.12	14
9-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
9-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.27	7.3
9-3	A	9	1.00	500.00	0.50	250.0	2.00	-1.03	1.9
9-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
9-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.19	11
9-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.31	6.4
10-1	A	9	1.00	508.03	0.50	250.0	2.03	-1.01	2.0
10-1	A	8	1.00	508.03	0.50	250.0	2.03	-0.33	6.1
10-1	A	11	1.00	508.03	0.50	250.0	2.03	-0.37	5.4
10-1	A	10	1.00	508.03	0.50	250.0	2.03	-0.83	2.4
10-1	A	7	1.00	508.03	0.50	250.0	2.03	-0.91	2.2
10-1	A	12	1.00	508.03	0.50	250.0	2.03	-0.44	4.6
10-2	A	8	1.00	427.00	0.50	250.0	1.71	-0.01	>100
10-2	A	7	1.00	427.00	0.50	250.0	1.71	0.06	30
10-2	A	11	1.00	427.00	0.50	250.0	1.71	0.02	69
10-2	A	12	1.00	427.00	0.50	250.0	1.71	0.03	58
10-2	A	10	1.00	427.00	0.50	250.0	1.71	0.03	60
10-2	A	9	1.00	427.00	0.50	250.0	1.71	0.10	18
10-3	A	9	1.00	500.00	0.50	250.0	2.00	-0.99	2.0
10-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.80	2.5
10-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.16	13
10-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.29	7.0
10-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.24	8.5
10-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.88	2.3
11-1	A	12	1.00	458.05	0.50	250.0	1.83	-0.19	9.5
11-1	A	9	1.00	458.05	0.50	250.0	1.83	-0.63	2.9
11-1	A	11	1.00	458.05	0.50	250.0	1.83	-0.09	22
11-1	A	8	1.00	458.05	0.50	250.0	1.83	-0.08	24
11-1	A	10	1.00	458.05	0.50	250.0	1.83	-0.47	3.9
11-1	A	7	1.00	458.05	0.50	250.0	1.83	-0.54	3.4
11-2	A	7	1.00	427.00	0.50	250.0	1.71	0.04	41
11-2	A	8	1.00	427.00	0.50	250.0	1.71	-0.02	82
11-2	A	11	1.00	427.00	0.50	250.0	1.71	0.02	87
11-2	A	12	1.00	427.00	0.50	250.0	1.71	0.02	92
11-2	A	10	1.00	427.00	0.50	250.0	1.71	0.01	>100
11-2	A	9	1.00	427.00	0.50	250.0	1.71	0.08	22
11-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.26	7.7
11-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.85	2.3
11-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.19	10
11-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.10	20

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
11-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.78	2.6
11-3	A	9	1.00	500.00	0.50	250.0	2.00	-0.95	2.1
12-1	A	11	1.00	408.06	0.50	250.0	1.63	-0.05	34
12-1	A	9	1.00	408.06	0.50	250.0	1.63	-0.35	4.7
12-1	A	10	1.00	408.06	0.50	250.0	1.63	-0.21	7.7
12-1	A	7	1.00	408.06	0.50	250.0	1.63	-0.27	6.1
12-1	A	12	1.00	408.06	0.50	250.0	1.63	-0.06	28
12-1	A	8	1.00	408.06	0.50	250.0	1.63	-0.04	39
12-2	A	9	1.00	427.00	0.50	250.0	1.71	0.06	27
12-2	A	7	1.00	427.00	0.50	250.0	1.71	0.03	54
12-2	A	8	1.00	427.00	0.50	250.0	1.71	-0.03	58
12-2	A	10	1.00	427.00	0.50	250.0	1.71	-0.01	>100
12-2	A	12	1.00	427.00	0.50	250.0	1.71	0.01	>100
12-2	A	11	1.00	427.00	0.50	250.0	1.71	0.02	>100
12-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.15	13
12-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.76	2.6
12-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.24	8.3
12-3	A	9	1.00	500.00	0.50	250.0	2.00	-0.92	2.2
12-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.82	2.4
12-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.09	21
13-1	A	10	1.00	358.07	0.50	250.0	1.43	-0.04	34
13-1	A	11	1.00	358.07	0.50	250.0	1.43	-0.02	62
13-1	A	12	1.00	358.07	0.50	250.0	1.43	-0.03	45
13-1	A	7	1.00	358.07	0.50	250.0	1.43	-0.05	27
13-1	A	9	1.00	358.07	0.50	250.0	1.43	-0.15	9.6
13-1	A	8	1.00	358.07	0.50	250.0	1.43	-0.02	80
13-2	A	12	1.00	427.00	0.50	250.0	1.71	0.01	>100
13-2	A	8	1.00	427.00	0.50	250.0	1.71	-0.04	47
13-2	A	9	1.00	427.00	0.50	250.0	1.71	0.05	32
13-2	A	10	1.00	427.00	0.50	250.0	1.71	-0.02	73
13-2	A	11	1.00	427.00	0.50	250.0	1.71	-0.02	>100
13-2	A	7	1.00	427.00	0.50	250.0	1.71	0.03	68
13-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.23	8.9
13-3	A	9	1.00	500.00	0.50	250.0	2.00	-0.89	2.2
13-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.10	21
13-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.09	22
13-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.80	2.5
13-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.75	2.7
14-1	A	8	1.00	308.09	0.50	250.0	1.23	-0.00	>100
14-1	A	10	1.00	308.09	0.50	250.0	1.23	-0.02	71
14-1	A	12	1.00	308.09	0.50	250.0	1.23	-0.01	84
14-1	A	11	1.00	308.09	0.50	250.0	1.23	-0.01	>100
14-1	A	7	1.00	308.09	0.50	250.0	1.23	-0.03	49
14-1	A	9	1.00	308.09	0.50	250.0	1.23	-0.04	34
14-2	A	9	1.00	427.00	0.50	250.0	1.71	0.05	38
14-2	A	12	1.00	427.00	0.50	250.0	1.71	-0.01	>100
14-2	A	7	1.00	427.00	0.50	250.0	1.71	0.02	82
14-2	A	11	1.00	427.00	0.50	250.0	1.71	-0.02	81
14-2	A	8	1.00	427.00	0.50	250.0	1.71	-0.04	41
14-2	A	10	1.00	427.00	0.50	250.0	1.71	-0.03	53
14-3	A	7	1.00	500.00	0.50	250.0	2.00	-0.78	2.6
14-3	A	8	1.00	500.00	0.50	250.0	2.00	-0.09	22
14-3	A	10	1.00	500.00	0.50	250.0	2.00	-0.09	22
14-3	A	11	1.00	500.00	0.50	250.0	2.00	-0.74	2.7
14-3	A	9	1.00	500.00	0.50	250.0	2.00	-0.87	2.3
14-3	A	12	1.00	500.00	0.50	250.0	2.00	-0.21	9.6
15-1	A	10	1.00	258.10	0.50	250.0	1.03	-0.00	>100
15-1	A	8	1.00	258.10	0.50	250.0	1.03	0.01	>100
15-1	A	9	1.00	258.10	0.50	250.0	1.03	-0.01	>100
15-1	A	12	1.00	258.10	0.50	250.0	1.03	-0.00	>100
15-1	A	7	1.00	258.10	0.50	250.0	1.03	-0.00	>100
15-1	A	11	1.00	258.10	0.50	250.0	1.03	-0.00	>100
15-2	A	10	1.00	677.00	0.50	250.0	2.71	-0.05	55
15-2	A	9	1.00	677.00	0.50	250.0	2.71	-0.03	97

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
15-2	A	8	1.00	677.00	0.50	250.0	2.71	-0.05	51
15-2	A	7	1.00	677.00	0.50	250.0	2.71	-0.05	55
15-2	A	12	1.00	677.00	0.50	250.0	2.71	-0.03	85
15-2	A	11	1.00	677.00	0.50	250.0	2.71	-0.03	85

Proprietà geometriche delle sezioni delle campate

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
	cm	cm	cm	cmq	cmq	cm	cm	cm	cm
1-1	0.00	15.00	15.00	--	--	--	--	--	--
1-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
1-1	45.00	182.92	137.92	1.57	2.36	10.00	21.00	50.00	4.00
1-1	182.92	226.78	43.86	0.79	2.36	10.00	21.00	50.00	4.00
1-1	226.78	445.31	218.53	0.00	2.36	10.00	21.00	50.00	4.00
1-1	445.31	495.36	50.05	0.79	2.36	10.00	21.00	50.00	4.00
1-1	495.36	506.44	11.08	1.57	2.36	10.00	21.00	50.00	4.00
1-1	506.44	544.46	38.02	2.36	2.36	50.00	25.00	--	--
1-1	544.46	559.46	15.00	--	--	--	--	--	--
1-2	559.46	574.46	15.00	--	--	--	--	--	--
1-2	574.46	604.05	29.59	3.14	2.36	50.00	25.00	--	--
1-2	604.05	687.65	83.60	2.36	2.36	10.00	21.00	50.00	4.00
1-2	687.65	941.44	253.78	1.57	2.36	10.00	21.00	50.00	4.00
1-2	941.44	971.44	30.00	2.36	2.36	50.00	25.00	--	--
1-2	971.44	986.44	15.00	--	--	--	--	--	--
1-3	986.44	1001.44	15.00	--	--	--	--	--	--
1-3	1001.44	1024.93	23.49	2.36	2.36	50.00	25.00	--	--
1-3	1024.93	1031.44	6.51	1.57	2.36	50.00	25.00	--	--
1-3	1031.44	1041.00	9.56	1.57	2.36	10.00	21.00	50.00	4.00
1-3	1041.00	1067.56	26.56	2.36	2.36	10.00	21.00	50.00	4.00
1-3	1067.56	1142.44	74.88	1.57	2.36	10.00	21.00	50.00	4.00
1-3	1142.44	1330.66	188.22	0.79	2.36	10.00	21.00	50.00	4.00
1-3	1330.66	1441.44	110.78	1.57	2.36	10.00	21.00	50.00	4.00
1-3	1441.44	1471.44	30.00	2.36	2.36	50.00	25.00	--	--
1-3	1471.44	1486.44	15.00	--	--	--	--	--	--
2-1	0.00	15.00	15.00	--	--	--	--	--	--
2-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
2-1	45.00	182.67	137.67	1.57	2.36	10.00	21.00	50.00	4.00
2-1	182.67	226.58	43.90	0.79	2.36	10.00	21.00	50.00	4.00
2-1	226.58	444.88	218.30	0.00	2.36	10.00	21.00	50.00	4.00
2-1	444.88	494.96	50.08	0.79	2.36	10.00	21.00	50.00	4.00
2-1	494.96	506.10	11.14	1.57	2.36	10.00	21.00	50.00	4.00
2-1	506.10	543.94	37.84	2.36	2.36	50.00	25.00	--	--
2-1	543.94	558.94	15.00	--	--	--	--	--	--
2-2	558.94	573.94	15.00	--	--	--	--	--	--
2-2	573.94	603.33	29.38	3.14	2.36	50.00	25.00	--	--
2-2	603.33	686.69	83.36	2.36	2.36	10.00	21.00	50.00	4.00
2-2	686.69	940.93	254.25	1.57	2.36	10.00	21.00	50.00	4.00
2-2	940.93	970.93	30.00	2.36	2.36	50.00	25.00	--	--
2-2	970.93	985.93	15.00	--	--	--	--	--	--
2-3	985.93	1000.93	15.00	--	--	--	--	--	--
2-3	1000.93	1024.45	23.52	2.36	2.36	50.00	25.00	--	--
2-3	1024.45	1030.93	6.48	1.57	2.36	50.00	25.00	--	--
2-3	1030.93	1040.52	9.59	1.57	2.36	10.00	21.00	50.00	4.00
2-3	1040.52	1067.09	26.57	2.36	2.36	10.00	21.00	50.00	4.00
2-3	1067.09	1141.93	74.84	1.57	2.36	10.00	21.00	50.00	4.00
2-3	1141.93	1330.15	188.22	0.79	2.36	10.00	21.00	50.00	4.00
2-3	1330.15	1440.93	110.78	1.57	2.36	10.00	21.00	50.00	4.00
2-3	1440.93	1470.93	30.00	2.36	2.36	50.00	25.00	--	--
2-3	1470.93	1485.93	15.00	--	--	--	--	--	--
3-1	0.00	15.00	15.00	--	--	--	--	--	--
3-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
3-1	45.00	182.42	137.42	1.57	2.36	10.00	21.00	50.00	4.00
3-1	182.42	226.37	43.95	0.79	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
3-1	226.37	444.45	218.08	0.00	2.36	10.00	21.00	50.00	4.00
3-1	444.45	494.55	50.11	0.79	2.36	10.00	21.00	50.00	4.00
3-1	494.55	505.76	11.20	1.57	2.36	10.00	21.00	50.00	4.00
3-1	505.76	543.42	37.67	2.36	2.36	50.00	25.00	--	--
3-1	543.42	558.42	15.00	--	--	--	--	--	--
3-2	558.42	573.42	15.00	--	--	--	--	--	--
3-2	573.42	602.60	29.18	3.14	2.36	50.00	25.00	--	--
3-2	602.60	685.72	83.12	2.36	2.36	10.00	21.00	50.00	4.00
3-2	685.72	940.43	254.71	1.57	2.36	10.00	21.00	50.00	4.00
3-2	940.43	970.43	30.00	2.36	2.36	50.00	25.00	--	--
3-2	970.43	985.43	15.00	--	--	--	--	--	--
3-3	985.43	1000.43	15.00	--	--	--	--	--	--
3-3	1000.43	1023.97	23.55	2.36	2.36	50.00	25.00	--	--
3-3	1023.97	1030.43	6.45	1.57	2.36	50.00	25.00	--	--
3-3	1030.43	1040.04	9.62	1.57	2.36	10.00	21.00	50.00	4.00
3-3	1040.04	1066.63	26.58	2.36	2.36	10.00	21.00	50.00	4.00
3-3	1066.63	1141.43	74.80	1.57	2.36	10.00	21.00	50.00	4.00
3-3	1141.43	1329.65	188.22	0.79	2.36	10.00	21.00	50.00	4.00
3-3	1329.65	1440.43	110.78	1.57	2.36	10.00	21.00	50.00	4.00
3-3	1440.43	1470.43	30.00	2.36	2.36	50.00	25.00	--	--
3-3	1470.43	1485.43	15.00	--	--	--	--	--	--
4-1	0.00	15.00	15.00	--	--	--	--	--	--
4-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
4-1	45.00	182.17	137.17	1.57	2.36	10.00	21.00	50.00	4.00
4-1	182.17	226.16	43.99	0.79	2.36	10.00	21.00	50.00	4.00
4-1	226.16	444.01	217.85	0.00	2.36	10.00	21.00	50.00	4.00
4-1	444.01	494.15	50.14	0.79	2.36	10.00	21.00	50.00	4.00
4-1	494.15	505.40	11.25	1.57	2.36	10.00	21.00	50.00	4.00
4-1	505.40	542.91	37.51	2.36	2.36	50.00	25.00	--	--
4-1	542.91	557.91	15.00	--	--	--	--	--	--
4-2	557.91	572.91	15.00	--	--	--	--	--	--
4-2	572.91	601.88	28.97	3.14	2.36	50.00	25.00	--	--
4-2	601.88	602.91	1.03	2.36	2.36	50.00	25.00	--	--
4-2	602.91	684.75	81.84	2.36	2.36	10.00	21.00	50.00	4.00
4-2	684.75	939.92	255.17	1.57	2.36	10.00	21.00	50.00	4.00
4-2	939.92	969.92	30.00	2.36	2.36	50.00	25.00	--	--
4-2	969.92	984.92	15.00	--	--	--	--	--	--
4-3	984.92	999.92	15.00	--	--	--	--	--	--
4-3	999.92	1023.50	23.58	2.36	2.36	50.00	25.00	--	--
4-3	1023.50	1029.92	6.42	1.57	2.36	50.00	25.00	--	--
4-3	1029.92	1039.57	9.65	1.57	2.36	10.00	21.00	50.00	4.00
4-3	1039.57	1066.16	26.59	2.36	2.36	10.00	21.00	50.00	4.00
4-3	1066.16	1140.92	74.76	1.57	2.36	10.00	21.00	50.00	4.00
4-3	1140.92	1329.14	188.22	0.79	2.36	10.00	21.00	50.00	4.00
4-3	1329.14	1439.92	110.78	1.57	2.36	10.00	21.00	50.00	4.00
4-3	1439.92	1469.92	30.00	2.36	2.36	50.00	25.00	--	--
4-3	1469.92	1484.92	15.00	--	--	--	--	--	--
5-1	0.00	15.00	15.00	--	--	--	--	--	--
5-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
5-1	45.00	181.92	136.92	1.57	2.36	10.00	21.00	50.00	4.00
5-1	181.92	225.96	44.03	0.79	2.36	10.00	21.00	50.00	4.00
5-1	225.96	443.58	217.62	0.00	2.36	10.00	21.00	50.00	4.00
5-1	443.58	493.75	50.17	0.79	2.36	10.00	21.00	50.00	4.00
5-1	493.75	504.97	11.23	1.57	2.36	10.00	21.00	50.00	4.00
5-1	504.97	542.39	37.41	2.36	2.36	50.00	25.00	--	--
5-1	542.39	557.39	15.00	--	--	--	--	--	--
5-2	557.39	572.39	15.00	--	--	--	--	--	--
5-2	572.39	601.15	28.77	3.14	2.36	50.00	25.00	--	--
5-2	601.15	602.39	1.23	2.36	2.36	50.00	25.00	--	--
5-2	602.39	683.78	81.39	2.36	2.36	10.00	21.00	50.00	4.00
5-2	683.78	939.41	255.64	1.57	2.36	10.00	21.00	50.00	4.00
5-2	939.41	969.41	30.00	2.36	2.36	50.00	25.00	--	--
5-2	969.41	984.41	15.00	--	--	--	--	--	--
5-3	984.41	999.41	15.00	--	--	--	--	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
5-3	999.41	1023.02	23.60	2.36	2.36	50.00	25.00	--	--
5-3	1023.02	1029.41	6.40	1.57	2.36	50.00	25.00	--	--
5-3	1029.41	1039.09	9.67	1.57	2.36	10.00	21.00	50.00	4.00
5-3	1039.09	1065.69	26.60	2.36	2.36	10.00	21.00	50.00	4.00
5-3	1065.69	1140.41	74.72	1.57	2.36	10.00	21.00	50.00	4.00
5-3	1140.41	1328.63	188.22	0.79	2.36	10.00	21.00	50.00	4.00
5-3	1328.63	1439.41	110.78	1.57	2.36	10.00	21.00	50.00	4.00
5-3	1439.41	1469.41	30.00	2.36	2.36	50.00	25.00	--	--
5-3	1469.41	1484.41	15.00	--	--	--	--	--	--
6-1	0.00	15.00	15.00	--	--	--	--	--	--
6-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
6-1	45.00	181.67	136.67	1.57	2.36	10.00	21.00	50.00	4.00
6-1	181.67	225.75	44.08	0.79	2.36	10.00	21.00	50.00	4.00
6-1	225.75	443.14	217.40	0.00	2.36	10.00	21.00	50.00	4.00
6-1	443.14	493.34	50.20	0.79	2.36	10.00	21.00	50.00	4.00
6-1	493.34	504.55	11.21	1.57	2.36	10.00	21.00	50.00	4.00
6-1	504.55	541.87	37.32	2.36	2.36	50.00	25.00	--	--
6-1	541.87	556.87	15.00	--	--	--	--	--	--
6-2	556.87	571.87	15.00	--	--	--	--	--	--
6-2	571.87	600.43	28.56	3.14	2.36	50.00	25.00	--	--
6-2	600.43	601.87	1.44	2.36	2.36	50.00	25.00	--	--
6-2	601.87	682.80	80.93	2.36	2.36	10.00	21.00	50.00	4.00
6-2	682.80	938.91	256.10	1.57	2.36	10.00	21.00	50.00	4.00
6-2	938.91	968.91	30.00	2.36	2.36	50.00	25.00	--	--
6-2	968.91	983.91	15.00	--	--	--	--	--	--
6-3	983.91	998.91	15.00	--	--	--	--	--	--
6-3	998.91	1022.54	23.63	2.36	2.36	50.00	25.00	--	--
6-3	1022.54	1028.91	6.37	1.57	2.36	50.00	25.00	--	--
6-3	1028.91	1038.61	9.70	1.57	2.36	10.00	21.00	50.00	4.00
6-3	1038.61	1065.23	26.62	2.36	2.36	10.00	21.00	50.00	4.00
6-3	1065.23	1139.91	74.68	1.57	2.36	10.00	21.00	50.00	4.00
6-3	1139.91	1328.13	188.22	0.79	2.36	10.00	21.00	50.00	4.00
6-3	1328.13	1438.91	110.78	1.57	2.36	10.00	21.00	50.00	4.00
6-3	1438.91	1468.91	30.00	2.36	2.36	50.00	25.00	--	--
6-3	1468.91	1483.91	15.00	--	--	--	--	--	--
7-1	0.00	15.00	15.00	--	--	--	--	--	--
7-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
7-1	45.00	181.45	136.45	1.57	2.36	10.00	21.00	50.00	4.00
7-1	181.45	225.56	44.11	0.79	2.36	10.00	21.00	50.00	4.00
7-1	225.56	442.76	217.20	0.00	2.36	10.00	21.00	50.00	4.00
7-1	442.76	492.99	50.23	0.79	2.36	10.00	21.00	50.00	4.00
7-1	492.99	504.17	11.19	1.57	2.36	10.00	21.00	50.00	4.00
7-1	504.17	541.40	37.23	2.36	2.36	50.00	25.00	--	--
7-1	541.40	556.40	15.00	--	--	--	--	--	--
7-2	556.40	571.40	15.00	--	--	--	--	--	--
7-2	571.40	599.78	28.37	3.14	2.36	50.00	25.00	--	--
7-2	599.78	601.40	1.63	2.36	2.36	50.00	25.00	--	--
7-2	601.40	681.94	80.54	2.36	2.36	10.00	21.00	50.00	4.00
7-2	681.94	938.40	256.46	1.57	2.36	10.00	21.00	50.00	4.00
7-2	938.40	968.40	30.00	2.36	2.36	50.00	25.00	--	--
7-2	968.40	983.40	15.00	--	--	--	--	--	--
7-3	983.40	998.40	15.00	--	--	--	--	--	--
7-3	998.40	1022.06	23.65	2.36	2.36	50.00	25.00	--	--
7-3	1022.06	1028.40	6.35	1.57	2.36	50.00	25.00	--	--
7-3	1028.40	1038.12	9.72	1.57	2.36	10.00	21.00	50.00	4.00
7-3	1038.12	1064.75	26.62	2.36	2.36	10.00	21.00	50.00	4.00
7-3	1064.75	1139.40	74.66	1.57	2.36	10.00	21.00	50.00	4.00
7-3	1139.40	1327.62	188.22	0.79	2.36	10.00	21.00	50.00	4.00
7-3	1327.62	1438.40	110.78	1.57	2.36	10.00	21.00	50.00	4.00
7-3	1438.40	1468.40	30.00	2.36	2.36	50.00	25.00	--	--
7-3	1468.40	1483.40	15.00	--	--	--	--	--	--
8-1	0.00	15.00	15.00	--	--	--	--	--	--
8-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
8-1	45.00	181.20	136.20	1.57	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
8-1	181.20	225.36	44.16	0.79	2.36	10.00	21.00	50.00	4.00
8-1	225.36	442.34	216.98	0.00	2.36	10.00	21.00	50.00	4.00
8-1	442.34	492.59	50.26	0.79	2.36	10.00	21.00	50.00	4.00
8-1	492.59	503.76	11.17	1.57	2.36	10.00	21.00	50.00	4.00
8-1	503.76	540.90	37.14	2.36	2.36	50.00	25.00	--	--
8-1	540.90	555.90	15.00	--	--	--	--	--	--
8-2	555.90	570.90	15.00	--	--	--	--	--	--
8-2	570.90	599.07	28.17	3.14	2.36	50.00	25.00	--	--
8-2	599.07	600.90	1.83	2.36	2.36	50.00	25.00	--	--
8-2	600.90	680.99	80.10	2.36	2.36	10.00	21.00	50.00	4.00
8-2	680.99	937.90	256.90	1.57	2.36	10.00	21.00	50.00	4.00
8-2	937.90	967.90	30.00	2.36	2.36	50.00	25.00	--	--
8-2	967.90	982.90	15.00	--	--	--	--	--	--
8-3	982.90	997.90	15.00	--	--	--	--	--	--
8-3	997.90	1021.58	23.68	2.36	2.36	50.00	25.00	--	--
8-3	1021.58	1027.90	6.32	1.57	2.36	50.00	25.00	--	--
8-3	1027.90	1037.64	9.75	1.57	2.36	10.00	21.00	50.00	4.00
8-3	1037.64	1064.28	26.63	2.36	2.36	10.00	21.00	50.00	4.00
8-3	1064.28	1138.90	74.62	1.57	2.36	10.00	21.00	50.00	4.00
8-3	1138.90	1327.12	188.22	0.79	2.36	10.00	21.00	50.00	4.00
8-3	1327.12	1437.90	110.78	1.57	2.36	10.00	21.00	50.00	4.00
8-3	1437.90	1467.90	30.00	2.36	2.36	50.00	25.00	--	--
8-3	1467.90	1482.90	15.00	--	--	--	--	--	--
9-1	1.79	18.58	16.79	--	--	--	--	--	--
9-1	18.58	48.58	30.00	1.57	2.36	50.00	25.00	--	--
9-1	48.58	182.80	134.22	1.57	2.36	10.00	21.00	50.00	4.00
9-1	182.80	227.30	44.50	0.79	2.36	10.00	21.00	50.00	4.00
9-1	227.30	442.30	215.00	0.00	2.36	10.00	21.00	50.00	4.00
9-1	442.30	492.64	50.34	0.79	2.36	10.00	21.00	50.00	4.00
9-1	492.64	503.79	11.15	1.57	2.36	10.00	21.00	50.00	4.00
9-1	503.79	540.39	36.60	2.36	2.36	50.00	25.00	--	--
9-1	540.39	555.39	15.00	--	--	--	--	--	--
9-2	555.39	570.39	15.00	--	--	--	--	--	--
9-2	570.39	597.61	27.22	3.14	2.36	50.00	25.00	--	--
9-2	597.61	600.39	2.78	2.36	2.36	50.00	25.00	--	--
9-2	600.39	678.38	77.99	2.36	2.36	10.00	21.00	50.00	4.00
9-2	678.38	937.39	259.01	1.57	2.36	10.00	21.00	50.00	4.00
9-2	937.39	967.39	30.00	2.36	2.36	50.00	25.00	--	--
9-2	967.39	982.39	15.00	--	--	--	--	--	--
9-3	982.39	997.39	15.00	--	--	--	--	--	--
9-3	997.39	1021.20	23.81	2.36	2.36	50.00	25.00	--	--
9-3	1021.20	1027.39	6.19	1.57	2.36	50.00	25.00	--	--
9-3	1027.39	1037.26	9.87	1.57	2.36	10.00	21.00	50.00	4.00
9-3	1037.26	1063.94	26.68	2.36	2.36	10.00	21.00	50.00	4.00
9-3	1063.94	1138.39	74.45	1.57	2.36	10.00	21.00	50.00	4.00
9-3	1138.39	1326.61	188.22	0.79	2.36	10.00	21.00	50.00	4.00
9-3	1326.61	1437.39	110.78	1.57	2.36	10.00	21.00	50.00	4.00
9-3	1437.39	1467.39	30.00	2.36	2.36	50.00	25.00	--	--
9-3	1467.39	1482.39	15.00	--	--	--	--	--	--
10-1	0.00	21.21	21.21	--	--	--	--	--	--
10-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
10-1	51.21	162.08	110.87	2.36	2.36	10.00	21.00	50.00	4.00
10-1	162.08	209.94	47.86	1.57	2.36	10.00	21.00	50.00	4.00
10-1	209.94	424.21	214.27	0.79	2.36	10.00	21.00	50.00	4.00
10-1	424.21	452.10	27.88	1.57	2.36	10.00	21.00	50.00	4.00
10-1	452.10	463.03	10.93	2.36	2.36	10.00	21.00	50.00	4.00
10-1	463.03	493.03	30.00	1.57	2.36	50.00	25.00	--	--
10-1	493.03	508.03	15.00	--	--	--	--	--	--
10-2	508.03	523.03	15.00	--	--	--	--	--	--
10-2	523.03	553.03	30.00	2.36	2.36	50.00	25.00	--	--
10-2	553.03	559.61	6.58	2.36	2.36	10.00	21.00	50.00	4.00
10-2	559.61	890.03	330.42	1.57	2.36	10.00	21.00	50.00	4.00
10-2	890.03	920.03	30.00	2.36	2.36	50.00	25.00	--	--
10-2	920.03	935.03	15.00	--	--	--	--	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
10-3	935.03	950.03	15.00	--	--	--	--	--	--
10-3	950.03	976.07	26.04	2.36	2.36	50.00	25.00	--	--
10-3	976.07	980.03	3.96	1.57	2.36	50.00	25.00	--	--
10-3	980.03	992.06	12.03	1.57	2.36	10.00	21.00	50.00	4.00
10-3	992.06	1019.60	27.54	2.36	2.36	10.00	21.00	50.00	4.00
10-3	1019.60	1091.03	71.43	1.57	2.36	10.00	21.00	50.00	4.00
10-3	1091.03	1279.25	188.22	0.79	2.36	10.00	21.00	50.00	4.00
10-3	1279.25	1390.03	110.78	1.57	2.36	10.00	21.00	50.00	4.00
10-3	1390.03	1420.03	30.00	2.36	2.36	50.00	25.00	--	--
10-3	1420.03	1435.03	15.00	--	--	--	--	--	--
11-1	-0.00	21.21	21.21	--	--	--	--	--	--
11-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
11-1	51.21	143.47	92.26	2.36	2.36	10.00	21.00	50.00	4.00
11-1	143.47	189.94	46.47	1.57	2.36	10.00	21.00	50.00	4.00
11-1	189.94	383.99	194.05	0.79	2.36	10.00	21.00	50.00	4.00
11-1	383.99	412.77	28.78	1.57	2.36	10.00	21.00	50.00	4.00
11-1	412.77	430.86	18.09	2.36	2.36	50.00	25.00	--	--
11-1	430.86	443.05	12.18	1.57	2.36	50.00	25.00	--	--
11-1	443.05	458.05	15.00	--	--	--	--	--	--
11-2	458.05	473.05	15.00	--	--	--	--	--	--
11-2	473.05	491.94	18.90	2.36	2.36	50.00	25.00	--	--
11-2	491.94	503.05	11.10	1.57	2.36	50.00	25.00	--	--
11-2	503.05	595.21	92.16	1.57	2.36	10.00	21.00	50.00	4.00
11-2	595.21	833.27	238.07	0.79	2.36	10.00	21.00	50.00	4.00
11-2	833.27	840.05	6.77	1.57	2.36	10.00	21.00	50.00	4.00
11-2	840.05	870.05	30.00	2.36	2.36	50.00	25.00	--	--
11-2	870.05	885.05	15.00	--	--	--	--	--	--
11-3	885.05	900.05	15.00	--	--	--	--	--	--
11-3	900.05	928.17	28.12	2.36	2.36	50.00	25.00	--	--
11-3	928.17	930.05	1.88	1.57	2.36	50.00	25.00	--	--
11-3	930.05	944.08	14.03	1.57	2.36	10.00	21.00	50.00	4.00
11-3	944.08	972.38	28.31	2.36	2.36	10.00	21.00	50.00	4.00
11-3	972.38	1041.05	68.66	1.57	2.36	10.00	21.00	50.00	4.00
11-3	1041.05	1229.27	188.22	0.79	2.36	10.00	21.00	50.00	4.00
11-3	1229.27	1340.05	110.78	1.57	2.36	10.00	21.00	50.00	4.00
11-3	1340.05	1370.05	30.00	2.36	2.36	50.00	25.00	--	--
11-3	1370.05	1385.05	15.00	--	--	--	--	--	--
12-1	0.00	21.21	21.21	--	--	--	--	--	--
12-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
12-1	51.21	124.34	73.13	2.36	2.36	10.00	21.00	50.00	4.00
12-1	124.34	169.95	45.61	1.57	2.36	10.00	21.00	50.00	4.00
12-1	169.95	295.05	125.10	0.79	2.36	10.00	21.00	50.00	4.00
12-1	295.05	363.06	68.01	1.57	2.36	10.00	21.00	50.00	4.00
12-1	363.06	393.06	30.00	2.36	2.36	50.00	25.00	--	--
12-1	393.06	408.06	15.00	--	--	--	--	--	--
12-2	408.06	423.06	15.00	--	--	--	--	--	--
12-2	423.06	449.07	26.01	2.36	2.36	50.00	25.00	--	--
12-2	449.07	453.06	3.99	1.57	2.36	50.00	25.00	--	--
12-2	453.06	790.06	337.00	1.57	2.36	10.00	21.00	50.00	4.00
12-2	790.06	820.06	30.00	2.36	2.36	50.00	25.00	--	--
12-2	820.06	835.06	15.00	--	--	--	--	--	--
12-3	835.06	850.06	15.00	--	--	--	--	--	--
12-3	850.06	859.29	9.23	3.14	2.36	50.00	25.00	--	--
12-3	859.29	880.06	20.77	2.36	2.36	50.00	25.00	--	--
12-3	880.06	892.39	12.33	2.36	2.36	10.00	21.00	50.00	4.00
12-3	892.39	895.75	3.36	1.57	2.36	10.00	21.00	50.00	4.00
12-3	895.75	949.48	53.73	2.36	2.36	10.00	21.00	50.00	4.00
12-3	949.48	991.06	41.58	1.57	2.36	10.00	21.00	50.00	4.00
12-3	991.06	1179.28	188.22	0.79	2.36	10.00	21.00	50.00	4.00
12-3	1179.28	1290.06	110.78	1.57	2.36	10.00	21.00	50.00	4.00
12-3	1290.06	1320.06	30.00	2.36	2.36	50.00	25.00	--	--
12-3	1320.06	1335.06	15.00	--	--	--	--	--	--
13-1	-0.00	21.21	21.21	--	--	--	--	--	--
13-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
13-1	51.21	104.45	53.24	2.36	2.36	10.00	21.00	50.00	4.00
13-1	104.45	149.96	45.51	1.57	2.36	10.00	21.00	50.00	4.00
13-1	149.96	251.23	101.28	0.79	2.36	10.00	21.00	50.00	4.00
13-1	251.23	313.07	61.84	1.57	2.36	10.00	21.00	50.00	4.00
13-1	313.07	343.07	30.00	2.36	2.36	50.00	25.00	--	--
13-1	343.07	358.07	15.00	--	--	--	--	--	--
13-2	358.07	373.07	15.00	--	--	--	--	--	--
13-2	373.07	385.40	12.33	2.36	2.36	50.00	25.00	--	--
13-2	385.40	403.07	17.67	1.57	2.36	50.00	25.00	--	--
13-2	403.07	556.55	153.48	1.57	2.36	10.00	21.00	50.00	4.00
13-2	556.55	702.54	145.99	2.36	2.36	10.00	21.00	50.00	4.00
13-2	702.54	740.07	37.53	1.57	2.36	10.00	21.00	50.00	4.00
13-2	740.07	770.07	30.00	2.36	2.36	50.00	25.00	--	--
13-2	770.07	785.07	15.00	--	--	--	--	--	--
13-3	785.07	800.07	15.00	--	--	--	--	--	--
13-3	800.07	810.72	10.64	3.14	2.36	50.00	25.00	--	--
13-3	810.72	830.07	19.36	2.36	2.36	50.00	25.00	--	--
13-3	830.07	843.72	13.64	2.36	2.36	10.00	21.00	50.00	4.00
13-3	843.72	847.06	3.35	1.57	2.36	10.00	21.00	50.00	4.00
13-3	847.06	904.36	57.30	2.36	2.36	10.00	21.00	50.00	4.00
13-3	904.36	941.07	36.71	1.57	2.36	10.00	21.00	50.00	4.00
13-3	941.07	1129.29	188.22	0.79	2.36	10.00	21.00	50.00	4.00
13-3	1129.29	1240.07	110.78	1.57	2.36	10.00	21.00	50.00	4.00
13-3	1240.07	1270.07	30.00	2.36	2.36	50.00	25.00	--	--
13-3	1270.07	1285.07	15.00	--	--	--	--	--	--
14-1	-0.00	21.21	21.21	--	--	--	--	--	--
14-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
14-1	51.21	83.36	32.15	2.36	2.36	10.00	21.00	50.00	4.00
14-1	83.36	129.96	46.60	1.57	2.36	10.00	21.00	50.00	4.00
14-1	129.96	195.92	65.96	0.79	2.36	10.00	21.00	50.00	4.00
14-1	195.92	263.09	67.16	1.57	2.36	10.00	21.00	50.00	4.00
14-1	263.09	293.09	30.00	2.36	2.36	50.00	25.00	--	--
14-1	293.09	308.09	15.00	--	--	--	--	--	--
14-2	308.09	323.09	15.00	--	--	--	--	--	--
14-2	323.09	324.18	1.09	2.36	2.36	50.00	25.00	--	--
14-2	324.18	353.09	28.91	1.57	2.36	50.00	25.00	--	--
14-2	353.09	509.38	156.30	1.57	2.36	10.00	21.00	50.00	4.00
14-2	509.38	652.39	143.00	0.79	2.36	10.00	21.00	50.00	4.00
14-2	652.39	690.09	37.70	1.57	2.36	10.00	21.00	50.00	4.00
14-2	690.09	720.09	30.00	2.36	2.36	50.00	25.00	--	--
14-2	720.09	735.09	15.00	--	--	--	--	--	--
14-3	735.09	750.09	15.00	--	--	--	--	--	--
14-3	750.09	761.76	11.68	3.14	2.36	50.00	25.00	--	--
14-3	761.76	780.09	18.32	2.36	2.36	50.00	25.00	--	--
14-3	780.09	794.69	14.61	2.36	2.36	10.00	21.00	50.00	4.00
14-3	794.69	798.48	3.79	1.57	2.36	10.00	21.00	50.00	4.00
14-3	798.48	857.17	58.69	2.36	2.36	10.00	21.00	50.00	4.00
14-3	857.17	891.09	33.92	1.57	2.36	10.00	21.00	50.00	4.00
14-3	891.09	1079.31	188.22	0.79	2.36	10.00	21.00	50.00	4.00
14-3	1079.31	1190.09	110.78	1.57	2.36	10.00	21.00	50.00	4.00
14-3	1190.09	1220.09	30.00	2.36	2.36	50.00	25.00	--	--
14-3	1220.09	1235.09	15.00	--	--	--	--	--	--
15-1	-0.00	21.21	21.21	--	--	--	--	--	--
15-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
15-1	51.21	60.29	9.08	2.36	2.36	10.00	21.00	50.00	4.00
15-1	60.29	213.10	152.81	1.57	2.36	10.00	21.00	50.00	4.00
15-1	213.10	243.10	30.00	1.57	2.36	50.00	25.00	--	--
15-1	243.10	258.10	15.00	--	--	--	--	--	--
15-2	258.10	273.10	15.00	--	--	--	--	--	--
15-2	273.10	303.10	30.00	2.36	2.36	50.00	25.00	--	--
15-2	303.10	342.34	39.25	2.36	2.36	10.00	21.00	50.00	4.00
15-2	342.34	392.20	49.85	1.57	2.36	10.00	21.00	50.00	4.00
15-2	392.20	557.26	165.06	0.79	2.36	10.00	21.00	50.00	4.00
15-2	557.26	640.10	82.84	1.57	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
15-2	640.10	670.10	30.00	2.36	2.36	50.00	25.00	--	--
15-2	670.10	935.10	265.00	--	--	--	--	--	--

Proprietà di inerzia delle sezioni delle campate

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	cm	cm	cm	kN*m	kN*m	kN*cm^4	kN*cm^4	kN*cm^4	kN*cm^4
1-1	0.00	15.00	15.00	Tratto infinitamente rigido					
1-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
1-1	45.00	182.92	137.92	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	182.92	226.78	43.86	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-1	226.78	445.31	218.53	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
1-1	445.31	495.36	50.05	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-1	495.36	506.44	11.08	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	506.44	544.46	38.02	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	544.46	559.46	15.00	Tratto infinitamente rigido					
1-2	559.46	574.46	15.00	Tratto infinitamente rigido					
1-2	574.46	604.05	29.59	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
1-2	604.05	687.65	83.60	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-2	687.65	941.44	253.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-2	941.44	971.44	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-2	971.44	986.44	15.00	Tratto infinitamente rigido					
1-3	986.44	1001.44	15.00	Tratto infinitamente rigido					
1-3	1001.44	1024.93	23.49	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-3	1024.93	1031.44	6.51	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
1-3	1031.44	1041.00	9.56	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-3	1041.00	1067.56	26.56	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-3	1067.56	1142.44	74.88	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-3	1142.44	1330.66	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-3	1330.66	1441.44	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-3	1441.44	1471.44	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-3	1471.44	1486.44	15.00	Tratto infinitamente rigido					
2-1	0.00	15.00	15.00	Tratto infinitamente rigido					
2-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
2-1	45.00	182.67	137.67	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	182.67	226.58	43.90	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-1	226.58	444.88	218.30	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
2-1	444.88	494.96	50.08	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-1	494.96	506.10	11.14	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	506.10	543.94	37.84	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	543.94	558.94	15.00	Tratto infinitamente rigido					
2-2	558.94	573.94	15.00	Tratto infinitamente rigido					
2-2	573.94	603.33	29.38	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
2-2	603.33	686.69	83.36	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-2	686.69	940.93	254.25	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-2	940.93	970.93	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-2	970.93	985.93	15.00	Tratto infinitamente rigido					
2-3	985.93	1000.93	15.00	Tratto infinitamente rigido					
2-3	1000.93	1024.45	23.52	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-3	1024.45	1030.93	6.48	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
2-3	1030.93	1040.52	9.59	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-3	1040.52	1067.09	26.57	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-3	1067.09	1141.93	74.84	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-3	1141.93	1330.15	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-3	1330.15	1440.93	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-3	1440.93	1470.93	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-3	1470.93	1485.93	15.00	Tratto infinitamente rigido					
3-1	0.00	15.00	15.00	Tratto infinitamente rigido					
3-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
3-1	45.00	182.42	137.42	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	182.42	226.37	43.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-1	226.37	444.45	218.08	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
3-1	444.45	494.55	50.11	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-1	494.55	505.76	11.20	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	505.76	543.42	37.67	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-1	543.42	558.42	15.00	Tratto infinitamente rigido					
3-2	558.42	573.42	15.00	Tratto infinitamente rigido					
3-2	573.42	602.60	29.18	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
3-2	602.60	685.72	83.12	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-2	685.72	940.43	254.71	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-2	940.43	970.43	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-2	970.43	985.43	15.00	Tratto infinitamente rigido					
3-3	985.43	1000.43	15.00	Tratto infinitamente rigido					
3-3	1000.43	1023.97	23.55	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-3	1023.97	1030.43	6.45	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
3-3	1030.43	1040.04	9.62	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-3	1040.04	1066.63	26.58	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-3	1066.63	1141.43	74.80	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-3	1141.43	1329.65	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-3	1329.65	1440.43	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-3	1440.43	1470.43	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-3	1470.43	1485.43	15.00	Tratto infinitamente rigido					
4-1	0.00	15.00	15.00	Tratto infinitamente rigido					
4-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
4-1	45.00	182.17	137.17	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	182.17	226.16	43.99	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-1	226.16	444.01	217.85	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
4-1	444.01	494.15	50.14	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-1	494.15	505.40	11.25	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	505.40	542.91	37.51	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	542.91	557.91	15.00	Tratto infinitamente rigido					
4-2	557.91	572.91	15.00	Tratto infinitamente rigido					
4-2	572.91	601.88	28.97	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
4-2	601.88	602.91	1.03	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-2	602.91	684.75	81.84	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-2	684.75	939.92	255.17	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-2	939.92	969.92	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
4-2	969.92	984.92	15.00	Tratto infinitamente rigido					
4-3	984.92	999.92	15.00	Tratto infinitamente rigido					
4-3	999.92	1023.50	23.58	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-3	1023.50	1029.92	6.42	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
4-3	1029.92	1039.57	9.65	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-3	1039.57	1066.16	26.59	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-3	1066.16	1140.92	74.76	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-3	1140.92	1329.14	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-3	1329.14	1439.92	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-3	1439.92	1469.92	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-3	1469.92	1484.92	15.00	Tratto infinitamente rigido					
5-1	0.00	15.00	15.00	Tratto infinitamente rigido					
5-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
5-1	45.00	181.92	136.92	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	181.92	225.96	44.03	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-1	225.96	443.58	217.62	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
5-1	443.58	493.75	50.17	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-1	493.75	504.97	11.23	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	504.97	542.39	37.41	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-1	542.39	557.39	15.00	Tratto infinitamente rigido					
5-2	557.39	572.39	15.00	Tratto infinitamente rigido					
5-2	572.39	601.15	28.77	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
5-2	601.15	602.39	1.23	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-2	602.39	683.78	81.39	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-2	683.78	939.41	255.64	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-2	939.41	969.41	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-2	969.41	984.41	15.00	Tratto infinitamente rigido					
5-3	984.41	999.41	15.00	Tratto infinitamente rigido					
5-3	999.41	1023.02	23.60	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-3	1023.02	1029.41	6.40	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
5-3	1029.41	1039.09	9.67	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-3	1039.09	1065.69	26.60	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-3	1065.69	1140.41	74.72	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-3	1140.41	1328.63	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-3	1328.63	1439.41	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-3	1439.41	1469.41	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-3	1469.41	1484.41	15.00	Tratto infinitamente rigido					
6-1	0.00	15.00	15.00	Tratto infinitamente rigido					
6-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
6-1	45.00	181.67	136.67	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-1	181.67	225.75	44.08	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
6-1	225.75	443.14	217.40	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
6-1	443.14	493.34	50.20	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
6-1	493.34	504.55	11.21	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-1	504.55	541.87	37.32	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-1	541.87	556.87	15.00	Tratto infinitamente rigido					

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
6-2	556.87	571.87	15.00	Tratto infinitamente rigido					
6-2	571.87	600.43	28.56	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
6-2	600.43	601.87	1.44	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-2	601.87	682.80	80.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-2	682.80	938.91	256.10	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-2	938.91	968.91	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-2	968.91	983.91	15.00	Tratto infinitamente rigido					
6-3	983.91	998.91	15.00	Tratto infinitamente rigido					
6-3	998.91	1022.54	23.63	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-3	1022.54	1028.91	6.37	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
6-3	1028.91	1038.61	9.70	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-3	1038.61	1065.23	26.62	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-3	1065.23	1139.91	74.68	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-3	1139.91	1328.13	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
6-3	1328.13	1438.91	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-3	1438.91	1468.91	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-3	1468.91	1483.91	15.00	Tratto infinitamente rigido					
7-1	0.00	15.00	15.00	Tratto infinitamente rigido					
7-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
7-1	45.00	181.45	136.45	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-1	181.45	225.56	44.11	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-1	225.56	442.76	217.20	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
7-1	442.76	492.99	50.23	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-1	492.99	504.17	11.19	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-1	504.17	541.40	37.23	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-1	541.40	556.40	15.00	Tratto infinitamente rigido					
7-2	556.40	571.40	15.00	Tratto infinitamente rigido					
7-2	571.40	599.78	28.37	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
7-2	599.78	601.40	1.63	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-2	601.40	681.94	80.54	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-2	681.94	938.40	256.46	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-2	938.40	968.40	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-2	968.40	983.40	15.00	Tratto infinitamente rigido					
7-3	983.40	998.40	15.00	Tratto infinitamente rigido					
7-3	998.40	1022.06	23.65	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-3	1022.06	1028.40	6.35	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
7-3	1028.40	1038.12	9.72	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-3	1038.12	1064.75	26.62	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-3	1064.75	1139.40	74.66	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-3	1139.40	1327.62	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-3	1327.62	1438.40	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-3	1438.40	1468.40	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-3	1468.40	1483.40	15.00	Tratto infinitamente rigido					
8-1	0.00	15.00	15.00	Tratto infinitamente rigido					
8-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
8-1	45.00	181.20	136.20	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
8-1	181.20	225.36	44.16	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-1	225.36	442.34	216.98	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
8-1	442.34	492.59	50.26	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-1	492.59	503.76	11.17	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-1	503.76	540.90	37.14	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-1	540.90	555.90	15.00	Tratto infinitamente rigido					
8-2	555.90	570.90	15.00	Tratto infinitamente rigido					
8-2	570.90	599.07	28.17	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
8-2	599.07	600.90	1.83	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-2	600.90	680.99	80.10	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-2	680.99	937.90	256.90	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-2	937.90	967.90	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-2	967.90	982.90	15.00	Tratto infinitamente rigido					
8-3	982.90	997.90	15.00	Tratto infinitamente rigido					
8-3	997.90	1021.58	23.68	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-3	1021.58	1027.90	6.32	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
8-3	1027.90	1037.64	9.75	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-3	1037.64	1064.28	26.63	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-3	1064.28	1138.90	74.62	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-3	1138.90	1327.12	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-3	1327.12	1437.90	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-3	1437.90	1467.90	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-3	1467.90	1482.90	15.00	Tratto infinitamente rigido					
9-1	1.79	18.58	16.79	Tratto infinitamente rigido					
9-1	18.58	48.58	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
9-1	48.58	182.80	134.22	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-1	182.80	227.30	44.50	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-1	227.30	442.30	215.00	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
9-1	442.30	492.64	50.34	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-1	492.64	503.79	11.15	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-1	503.79	540.39	36.60	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-1	540.39	555.39	15.00	Tratto infinitamente rigido					
9-2	555.39	570.39	15.00	Tratto infinitamente rigido					
9-2	570.39	597.61	27.22	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
9-2	597.61	600.39	2.78	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-2	600.39	678.38	77.99	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
9-2	678.38	937.39	259.01	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-2	937.39	967.39	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-2	967.39	982.39	15.00	Tratto infinitamente rigido					
9-3	982.39	997.39	15.00	Tratto infinitamente rigido					
9-3	997.39	1021.20	23.81	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-3	1021.20	1027.39	6.19	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
9-3	1027.39	1037.26	9.87	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-3	1037.26	1063.94	26.68	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
9-3	1063.94	1138.39	74.45	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-3	1138.39	1326.61	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-3	1326.61	1437.39	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-3	1437.3	1467.3	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	9	9							
9-3	1467.39	1482.39	15.00	Tratto infinitamente rigido					
10-1	0.00	21.21	21.21	Tratto infinitamente rigido					
10-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-1	51.21	162.08	110.87	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-1	162.08	209.94	47.86	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-1	209.94	424.21	214.27	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
10-1	424.21	452.10	27.88	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-1	452.10	463.03	10.93	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-1	463.03	493.03	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
10-1	493.03	508.03	15.00	Tratto infinitamente rigido					
10-2	508.03	523.03	15.00	Tratto infinitamente rigido					
10-2	523.03	553.03	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-2	553.03	559.61	6.58	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-2	559.61	890.03	330.42	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-2	890.03	920.03	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-2	920.03	935.03	15.00	Tratto infinitamente rigido					
10-3	935.03	950.03	15.00	Tratto infinitamente rigido					
10-3	950.03	976.07	26.04	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-3	976.07	980.03	3.96	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
10-3	980.03	992.06	12.03	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-3	992.06	1019.60	27.54	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-3	1019.60	1091.03	71.43	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-3	1091.03	1279.25	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
10-3	1279.25	1390.03	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-3	1390.03	1420.03	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-3	1420.03	1435.03	15.00	Tratto infinitamente rigido					
11-1	-0.00	21.21	21.21	Tratto infinitamente rigido					
11-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-1	51.21	143.47	92.26	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
11-1	143.47	189.94	46.47	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-1	189.94	383.99	194.05	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
11-1	383.99	412.77	28.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-1	412.77	430.86	18.09	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-1	430.86	443.05	12.18	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
11-1	443.05	458.05	15.00	Tratto infinitamente rigido					
11-2	458.05	473.05	15.00	Tratto infinitamente rigido					
11-2	473.05	491.94	18.90	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-2	491.94	503.05	11.10	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
11-2	503.05	595.21	92.16	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-2	595.21	833.27	238.07	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
11-2	833.27	840.05	6.77	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-2	840.05	870.05	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-2	870.05	885.05	15.00	Tratto infinitamente rigido					
11-3	885.05	900.05	15.00	Tratto infinitamente rigido					
11-3	900.05	928.17	28.12	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-3	928.17	930.05	1.88	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
11-3	930.05	944.08	14.03	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-3	944.08	972.38	28.31	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
11-3	972.38	1041.05	68.66	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-3	1041.05	1229.27	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
11-3	1229.27	1340.05	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-3	1340.05	1370.05	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
11-3	1370.05	1385.05	15.00	Tratto infinitamente rigido					
12-1	0.00	21.21	21.21	Tratto infinitamente rigido					
12-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-1	51.21	124.34	73.13	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
12-1	124.34	169.95	45.61	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-1	169.95	295.05	125.10	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
12-1	295.05	363.06	68.01	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-1	363.06	393.06	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-1	393.06	408.06	15.00	Tratto infinitamente rigido					
12-2	408.06	423.06	15.00	Tratto infinitamente rigido					
12-2	423.06	449.07	26.01	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-2	449.07	453.06	3.99	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
12-2	453.06	790.06	337.00	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-2	790.06	820.06	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-2	820.06	835.06	15.00	Tratto infinitamente rigido					
12-3	835.06	850.06	15.00	Tratto infinitamente rigido					
12-3	850.06	859.29	9.23	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
12-3	859.29	880.06	20.77	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-3	880.06	892.39	12.33	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
12-3	892.39	895.75	3.36	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-3	895.75	949.48	53.73	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
12-3	949.48	991.06	41.58	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-3	991.06	1179.28	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
12-3	1179.28	1290.06	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-3	1290.06	1320.06	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-3	1320.06	1335.06	15.00	Tratto infinitamente rigido					
13-1	-0.00	21.21	21.21	Tratto infinitamente rigido					
13-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-1	51.21	104.45	53.24	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-1	104.45	149.96	45.51	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-1	149.96	251.23	101.28	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
13-1	251.23	313.07	61.84	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-1	313.07	343.07	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-1	343.07	358.07	15.00	Tratto infinitamente rigido					
13-2	358.07	373.07	15.00	Tratto infinitamente rigido					
13-2	373.07	385.40	12.33	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-2	385.40	403.07	17.67	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
13-2	403.07	556.55	153.48	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-2	556.55	702.54	145.99	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-2	702.54	740.07	37.53	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-2	740.07	770.07	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-2	770.07	785.07	15.00	Tratto infinitamente rigido					
13-3	785.07	800.07	15.00	Tratto infinitamente rigido					
13-3	800.07	810.72	10.64	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
13-3	810.72	830.07	19.36	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-3	830.07	843.72	13.64	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-3	843.72	847.06	3.35	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-3	847.06	904.36	57.30	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-3	904.36	941.07	36.71	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-3	941.07	1129.29	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
13-3	1129.29	1240.07	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-3	1240.07	1270.07	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-3	1270.07	1285.07	15.00	Tratto infinitamente rigido					
14-1	-0.00	21.21	21.21	Tratto infinitamente rigido					
14-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
14-1	51.21	83.36	32.15	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
14-1	83.36	129.96	46.60	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-1	129.96	195.92	65.96	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
14-1	195.92	263.09	67.16	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-1	263.09	293.09	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-1	293.09	308.09	15.00	Tratto infinitamente rigido					
14-2	308.09	323.09	15.00	Tratto infinitamente rigido					
14-2	323.09	324.18	1.09	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-2	324.18	353.09	28.91	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
14-2	353.09	509.38	156.30	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-2	509.38	652.39	143.00	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
14-2	652.39	690.09	37.70	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-2	690.09	720.09	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-2	720.09	735.09	15.00	Tratto infinitamente rigido					
14-3	735.09	750.09	15.00	Tratto infinitamente rigido					
14-3	750.09	761.76	11.68	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
14-3	761.76	780.09	18.32	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-3	780.09	794.69	14.61	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
14-3	794.69	798.48	3.79	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-3	798.48	857.17	58.69	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
14-3	857.17	891.09	33.92	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-3	891.09	1079.31	188.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
14-3	1079.31	1190.09	110.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-3	1190.09	1220.09	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-3	1220.09	1235.09	15.00	Tratto infinitamente rigido					
15-1	-0.00	21.21	21.21	Tratto infinitamente rigido					
15-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
15-1	51.21	60.29	9.08	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
15-1	60.29	213.10	152.81	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
15-1	213.10	243.10	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
15-1	243.10	258.10	15.00	Tratto infinitamente rigido					
15-2	258.10	273.10	15.00	Tratto infinitamente rigido					
15-2	273.10	303.10	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
15-2	303.10	342.34	39.25	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
15-2	342.34	392.20	49.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
15-2	392.20	557.26	165.06	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
15-2	557.26	640.10	82.84	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
15-2	640.10	670.10	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
15-2	670.10	935.10	265.00	Tratto infinitamente rigido					

Tensioni di esercizio combinazione Rara

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	226.78	11.56	--	-4.69	240.26	--	--	14.94	360.00	9	8	Si
1-2	937.21	--	6.72	--	--	-6.47	219.55	14.94	360.00	10	11	Si
1-3	1024.93	--	6.68	--	--	-3.02	206.84	14.94	360.00	12	11	Si
2-1	226.58	11.54	--	-4.68	239.84	--	--	14.94	360.00	9	8	Si
2-2	936.68	--	6.72	--	--	-6.47	219.55	14.94	360.00	10	11	Si
2-3	1024.45	--	6.68	--	--	-3.02	206.85	14.94	360.00	12	11	Si
3-1	226.37	11.52	--	-4.67	239.42	--	--	14.94	360.00	9	8	Si
3-2	936.16	--	6.72	--	--	-6.47	219.55	14.94	360.00	10	11	Si
3-3	1023.97	--	6.68	--	--	-3.02	206.85	14.94	360.00	12	11	Si
4-1	226.16	11.50	--	-4.67	238.99	--	--	14.94	360.00	9	8	Si
4-2	935.64	--	6.72	--	--	-6.47	219.56	14.94	360.00	10	11	Si
4-3	1023.5	--	6.68	--	--	-3.02	206.85	14.94	360.00	12	11	Si

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	0											
5-1	225.96	11.48	--	-4.66	238.57	--	--	14.94	360.00	9	8	Si
5-2	935.12	--	6.72	--	--	-6.47	219.56	14.94	360.00	10	11	Si
5-3	1023.02	--	6.68	--	--	-3.02	206.86	14.94	360.00	12	11	Si
6-1	225.75	11.46	--	-4.65	238.15	--	--	14.94	360.00	9	8	Si
6-2	934.59	--	6.72	--	--	-6.47	219.56	14.94	360.00	10	11	Si
6-3	1022.54	--	6.68	--	--	-3.02	206.86	14.94	360.00	12	11	Si
7-1	225.56	11.44	--	-4.64	237.77	--	--	14.94	360.00	9	8	Si
7-2	934.07	--	6.72	--	--	-6.47	219.56	14.94	360.00	10	11	Si
7-3	1022.06	--	6.68	--	--	-3.02	206.86	14.94	360.00	12	11	Si
8-1	225.36	11.42	--	-4.63	237.36	--	--	14.94	360.00	9	8	Si
8-2	933.55	--	6.72	--	--	-6.47	219.56	14.94	360.00	10	11	Si
8-3	1021.58	--	6.68	--	--	-3.02	206.87	14.94	360.00	12	11	Si
9-1	227.30	11.33	--	-4.60	235.44	--	--	14.94	360.00	9	8	Si
9-2	932.97	--	6.72	--	--	-6.47	219.57	14.94	360.00	10	11	Si
9-3	1021.20	--	6.68	--	--	-3.02	206.88	14.94	360.00	12	11	Si
10-1	493.03	--	9.53	--	--	-4.32	295.32	14.94	360.00	12	10	Si
10-2	559.61	--	6.73	--	--	-6.48	220.07	14.94	360.00	11	10	Si
10-3	976.07	--	6.69	--	--	-3.03	207.16	14.94	360.00	12	11	Si
11-1	443.05	--	7.97	--	--	-3.61	246.92	14.94	360.00	12	10	Si
11-2	833.27	--	6.73	--	--	-6.48	219.89	14.94	360.00	10	11	Si
11-3	930.05	--	6.47	--	--	-6.23	211.61	14.94	360.00	12	11	Si
12-1	393.06	--	6.68	--	--	-2.53	139.73	14.94	360.00	12	10	Si
12-2	820.06	--	10.51	--	--	-3.98	219.89	14.94	360.00	12	11	Si
12-3	1132.06	9.31	--	-3.69	193.75	--	--	14.94	360.00	9	8	Si
13-1	343.07	--	5.67	--	--	-2.14	118.51	14.94	360.00	9	10	Si
13-2	770.07	--	10.67	--	--	-4.04	223.05	14.94	360.00	12	11	Si
13-3	810.72	--	9.15	--	--	-3.46	191.31	14.94	360.00	12	11	Si
14-1	293.09	--	4.92	--	--	-1.86	102.98	14.94	360.00	9	10	Si
14-2	720.09	--	10.78	--	--	-4.08	225.39	14.94	360.00	12	11	Si
14-3	761.76	--	9.15	--	--	-3.46	191.43	14.94	360.00	12	11	Si
15-1	243.10	--	4.57	--	--	-2.07	141.47	14.94	360.00	11	7	Si
15-2	670.10	--	6.58	--	--	-2.49	137.65	14.94	360.00	9	8	Si

Tensioni di esercizio combinazione QP

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	226.78	9.78	--	-3.97	203.22	--	--	11.21	360.00	21	20	Si
1-2	604.05	--	7.82	--	--	-6.57	172.78	11.21	360.00	23	22	Si
1-3	1283.44	7.97	--	-3.16	165.88	--	--	11.21	360.00	21	20	Si
2-1	226.58	9.76	--	-3.96	202.86	--	--	11.21	360.00	21	20	Si
2-2	603.33	--	7.82	--	--	-6.57	172.77	11.21	360.00	23	22	Si
2-3	1282.93	7.97	--	-3.16	165.84	--	--	11.21	360.00	21	20	Si
3-1	226.37	9.74	--	-3.95	202.49	--	--	11.21	360.00	21	20	Si
3-2	602.60	--	7.82	--	--	-6.56	172.75	11.21	360.00	23	22	Si
3-3	1282.43	7.96	--	-3.16	165.80	--	--	11.21	360.00	21	20	Si
4-1	226.16	9.73	--	-3.95	202.13	--	--	11.21	360.00	21	20	Si
4-2	602.91	--	7.74	--	--	-6.50	170.95	11.21	360.00	23	22	Si
4-3	1281.92	7.96	--	-3.16	165.75	--	--	11.21	360.00	21	20	Si
5-1	225.96	9.71	--	-3.94	201.76	--	--	11.21	360.00	21	20	Si
5-2	602.39	--	7.72	--	--	-6.48	170.58	11.21	360.00	23	22	Si
5-3	1281.4	7.96	--	-3.16	165.71	--	--	11.21	360.00	21	20	Si

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	1											
6-1	225.75	9.69	--	-3.93	201.39	--	--	11.21	360.00	21	20	Si
6-2	601.87	--	7.71	--	--	-6.47	170.21	11.21	360.00	23	22	Si
6-3	1280.91	7.96	--	-3.16	165.67	--	--	11.21	360.00	21	20	Si
7-1	225.56	9.68	--	-3.93	201.07	--	--	11.21	360.00	21	20	Si
7-2	601.40	--	7.69	--	--	-6.46	169.87	11.21	360.00	23	22	Si
7-3	1280.40	7.96	--	-3.16	165.63	--	--	11.21	360.00	21	20	Si
8-1	225.36	9.66	--	-3.92	200.71	--	--	11.21	360.00	21	20	Si
8-2	600.90	--	7.68	--	--	-6.44	169.51	11.21	360.00	23	22	Si
8-3	1279.90	7.96	--	-3.16	165.59	--	--	11.21	360.00	21	20	Si
9-1	227.30	9.58	--	-3.89	199.03	--	--	11.21	360.00	21	20	Si
9-2	600.39	--	7.60	--	--	-6.38	167.81	11.21	360.00	23	22	Si
9-3	1279.39	7.95	--	-3.15	165.39	--	--	11.21	360.00	21	20	Si
10-1	493.03	--	8.04	--	--	-3.64	249.09	11.21	360.00	24	22	Si
10-2	559.61	--	5.73	--	--	-5.51	187.21	11.21	360.00	23	22	Si
10-3	976.07	--	5.30	--	--	-2.40	164.26	11.21	360.00	24	23	Si
11-1	443.05	--	6.69	--	--	-3.03	207.14	11.21	360.00	24	22	Si
11-2	833.27	--	5.43	--	--	-5.23	177.65	11.21	360.00	22	23	Si
11-3	930.05	--	5.18	--	--	-4.99	169.29	11.21	360.00	24	23	Si
12-1	393.06	--	5.57	--	--	-2.11	116.40	11.21	360.00	24	22	Si
12-2	820.06	--	8.54	--	--	-3.23	178.51	11.21	360.00	24	23	Si
12-3	1132.06	7.47	--	-2.97	155.57	--	--	11.21	360.00	21	20	Si
13-1	343.07	--	4.68	--	--	-1.77	97.88	11.21	360.00	21	22	Si
13-2	770.07	--	8.69	--	--	-3.29	181.79	11.21	360.00	24	23	Si
13-3	810.72	--	7.45	--	--	-2.82	155.80	11.21	360.00	24	23	Si
14-1	293.09	--	4.03	--	--	-1.52	84.22	11.21	360.00	21	22	Si
14-2	720.09	--	8.81	--	--	-3.33	184.28	11.21	360.00	24	23	Si
14-3	761.76	--	7.49	--	--	-2.83	156.55	11.21	360.00	24	23	Si
15-1	243.10	--	3.93	--	--	-1.78	121.71	11.21	360.00	23	19	Si
15-2	670.10	--	5.58	--	--	-2.11	116.78	11.21	360.00	21	20	Si

Verifica a decompressione o Verifica formazione fessure

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	
1-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
1-2	574.46	--	11.97	--	--	-4.02	0.00	2.13	Si
1-3	1001.44	--	9.42	--	--	-3.56	0.00	2.13	Si
2-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
2-2	573.94	--	11.94	--	--	-4.01	0.00	2.13	Si
2-3	1000.93	--	9.42	--	--	-3.57	0.00	2.13	Si
3-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
3-2	573.42	--	11.92	--	--	-4.00	0.00	2.13	Si
3-3	1000.43	--	9.42	--	--	-3.57	0.00	2.13	Si
4-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
4-2	572.91	--	11.90	--	--	-4.00	0.00	2.13	Si
4-3	999.92	--	9.43	--	--	-3.57	0.00	2.13	Si
5-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
5-2	572.39	--	11.88	--	--	-3.99	0.00	2.13	Si
5-3	999.41	--	9.43	--	--	-3.57	0.00	2.13	Si
6-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
6-2	571.87	--	11.86	--	--	-3.98	0.00	2.13	Si
6-3	998.91	--	9.43	--	--	-3.57	0.00	2.13	Si
7-1	15.00	1.39	--	-0.54	0.00	--	--	2.13	Si
7-2	571.40	--	11.84	--	--	-3.98	0.00	2.13	Si
7-3	998.40	--	9.44	--	--	-3.57	0.00	2.13	Si
8-1	15.00	1.39	--	-0.54	0.00	--	--	2.13	Si
8-2	570.90	--	11.82	--	--	-3.97	0.00	2.13	Si

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
8-3	997.90	--	9.44	--	--	-3.57	0.00	2.13	Si
9-1	18.58	1.54	--	-0.59	0.00	--	--	2.13	Si
9-2	570.39	--	11.72	--	--	-3.94	0.00	2.13	Si
9-3	997.39	--	9.46	--	--	-3.58	0.00	2.13	Si
10-1	21.21	1.74	--	-0.66	0.00	--	--	2.13	Si
10-2	523.03	--	9.96	--	--	-3.77	0.00	2.13	Si
10-3	950.03	--	9.74	--	--	-3.69	0.00	2.13	Si
11-1	21.21	1.56	--	-0.59	0.00	--	--	2.13	Si
11-2	473.05	--	8.29	--	--	-3.14	0.00	2.13	Si
11-3	900.05	--	10.01	--	--	-3.79	0.00	2.13	Si
12-1	21.21	1.38	--	-0.52	0.00	--	--	2.13	Si
12-2	423.06	--	6.89	--	--	-2.61	0.00	2.13	Si
12-3	850.06	--	10.23	--	--	-3.44	0.00	2.13	Si
13-1	21.21	1.19	--	-0.45	0.00	--	--	2.13	Si
13-2	373.07	--	5.76	--	--	-2.18	0.00	2.13	Si
13-3	800.07	--	10.41	--	--	-3.50	0.00	2.13	Si
14-1	21.21	1.01	--	-0.38	0.00	--	--	2.13	Si
14-2	323.09	--	4.90	--	--	-1.85	0.00	2.13	Si
14-3	750.09	--	10.54	--	--	-3.54	0.00	2.13	Si
15-1	21.21	0.53	--	-0.20	0.00	--	--	2.13	Si
15-2	273.10	--	4.41	--	--	-1.67	0.00	2.13	Si

Solaio N.: Corpo scala
Base travetto = 10.00 cm

Criterio di verifica: Solaio in c.a.		
Rck	MPa	30.00
fyk	MPa	450.00
$\varepsilon c0 *10^3$		2
$\varepsilon cu *10^3$		3.5
$\varepsilon fu *10^3$		10
Ef	MPa	2.10E05
Copriferro di calcolo	cm	3.00
Copriferro di disegno	cm	3.00
fcd		0.85
γAcc		1.15
γCls		1.5
Percentuale max acciaio	%	1.8
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		Si
Verifica aperture fessure	MPa	No
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σCls	MPa	14.94
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σCls	MPa	11.21
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coeffcienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5

TRAVETTO N.: 1

CAMPATA N.: 1

Luce Netta L	250.37 cm
Altezza solaio H	25.00 cm
Altezza soletta s	4.00 cm
Tipo	Gettato in Opera

Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
125.19	3.20	0.00	0.00	0.57	19.66	15.41		3Ø10		Si
250.37	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 2

CAMPATA N.: 1
Luce Netta L 250.29 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
125.14	3.20	0.00	0.00	0.57	19.66	15.41		3Ø10		Si
250.29	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 3

CAMPATA N.: 1
Luce Netta L 250.20 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
125.10	3.20	0.00	0.00	0.57	19.66	15.41		3Ø10		Si
250.20	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 4

CAMPATA N.: 1
Luce Netta L 250.12 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
125.06	3.20	0.00	0.00	0.57	19.66	15.41		3Ø10		Si
250.12	-0.00	1.60	7.67	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 5

CAMPATA N.: 1

Luce Netta L 250.03 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	1.60	7.66	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
125.01	3.19	0.00	0.00	0.57	19.66	15.41		3Ø10		Si
250.03	-0.00	1.60	7.66	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

Verifiche di Deformabilità
Combinazioni di tipo: Rara

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
				cm			cm	cm	
1-1	A	7	1.00	280.37	0.50	250.0	1.12	-0.01	84
1-1	A	12	1.00	280.37	0.50	250.0	1.12	-0.01	84
1-1	A	11	1.00	280.37	0.50	250.0	1.12	-0.01	84
1-1	A	10	1.00	280.37	0.50	250.0	1.12	-0.01	84
1-1	A	9	1.00	280.37	0.50	250.0	1.12	-0.01	84
1-1	A	8	1.00	280.37	0.50	250.0	1.12	-0.01	84
2-1	A	8	1.00	280.29	0.50	250.0	1.12	-0.01	84
2-1	A	11	1.00	280.29	0.50	250.0	1.12	-0.01	84
2-1	A	7	1.00	280.29	0.50	250.0	1.12	-0.01	84
2-1	A	10	1.00	280.29	0.50	250.0	1.12	-0.01	84
2-1	A	12	1.00	280.29	0.50	250.0	1.12	-0.01	84
2-1	A	9	1.00	280.29	0.50	250.0	1.12	-0.01	84
3-1	A	9	1.00	280.20	0.50	250.0	1.12	-0.01	84
3-1	A	8	1.00	280.20	0.50	250.0	1.12	-0.01	84
3-1	A	12	1.00	280.20	0.50	250.0	1.12	-0.01	84
3-1	A	7	1.00	280.20	0.50	250.0	1.12	-0.01	84
3-1	A	10	1.00	280.20	0.50	250.0	1.12	-0.01	84
3-1	A	11	1.00	280.20	0.50	250.0	1.12	-0.01	84
4-1	A	8	1.00	280.12	0.50	250.0	1.12	-0.01	85
4-1	A	7	1.00	280.12	0.50	250.0	1.12	-0.01	85
4-1	A	9	1.00	280.12	0.50	250.0	1.12	-0.01	85
4-1	A	10	1.00	280.12	0.50	250.0	1.12	-0.01	85
4-1	A	12	1.00	280.12	0.50	250.0	1.12	-0.01	85
4-1	A	11	1.00	280.12	0.50	250.0	1.12	-0.01	85
5-1	A	10	1.00	280.03	0.50	250.0	1.12	-0.01	85
5-1	A	9	1.00	280.03	0.50	250.0	1.12	-0.01	85
5-1	A	7	1.00	280.03	0.50	250.0	1.12	-0.01	85
5-1	A	8	1.00	280.03	0.50	250.0	1.12	-0.01	85
5-1	A	12	1.00	280.03	0.50	250.0	1.12	-0.01	85
5-1	A	11	1.00	280.03	0.50	250.0	1.12	-0.01	85

Proprietà geometriche delle sezioni delle campate

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
	cm	cm	cm	cmq	cmq	cm	cm	cm	cm
1-1	0.00	15.00	15.00	--	--	--	--	--	--
1-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
1-1	45.00	67.54	22.54	2.36	2.36	10.00	21.00	50.00	4.00
1-1	67.54	115.15	47.61	1.57	2.36	10.00	21.00	50.00	4.00
1-1	115.15	212.83	97.68	0.00	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
1-1	212.83	235.37	22.54	1.57	2.36	10.00	21.00	50.00	4.00
1-1	235.37	265.37	30.00	2.36	2.36	50.00	25.00	--	--
1-1	265.37	280.37	15.00	--	--	--	--	--	--
2-1	0.00	15.00	15.00	--	--	--	--	--	--
2-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
2-1	45.00	67.50	22.50	2.36	2.36	10.00	21.00	50.00	4.00
2-1	67.50	115.11	47.61	1.57	2.36	10.00	21.00	50.00	4.00
2-1	115.11	212.79	97.67	0.00	2.36	10.00	21.00	50.00	4.00
2-1	212.79	235.29	22.50	1.57	2.36	10.00	21.00	50.00	4.00
2-1	235.29	265.29	30.00	2.36	2.36	50.00	25.00	--	--
2-1	265.29	280.29	15.00	--	--	--	--	--	--
3-1	0.00	15.00	15.00	--	--	--	--	--	--
3-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
3-1	45.00	67.46	22.46	2.36	2.36	10.00	21.00	50.00	4.00
3-1	67.46	115.08	47.62	1.57	2.36	10.00	21.00	50.00	4.00
3-1	115.08	212.74	97.66	0.00	2.36	10.00	21.00	50.00	4.00
3-1	212.74	235.20	22.46	1.57	2.36	10.00	21.00	50.00	4.00
3-1	235.20	265.20	30.00	2.36	2.36	50.00	25.00	--	--
3-1	265.20	280.20	15.00	--	--	--	--	--	--
4-1	0.00	15.00	15.00	--	--	--	--	--	--
4-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
4-1	45.00	67.42	22.42	2.36	2.36	10.00	21.00	50.00	4.00
4-1	67.42	115.05	47.62	1.57	2.36	10.00	21.00	50.00	4.00
4-1	115.05	212.69	97.65	0.00	2.36	10.00	21.00	50.00	4.00
4-1	212.69	235.12	22.42	1.57	2.36	10.00	21.00	50.00	4.00
4-1	235.12	265.12	30.00	2.36	2.36	50.00	25.00	--	--
4-1	265.12	280.12	15.00	--	--	--	--	--	--
5-1	-0.00	15.00	15.00	--	--	--	--	--	--
5-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
5-1	45.00	67.38	22.38	2.36	2.36	10.00	21.00	50.00	4.00
5-1	67.38	115.01	47.63	1.57	2.36	10.00	21.00	50.00	4.00
5-1	115.01	212.65	97.63	0.00	2.36	10.00	21.00	50.00	4.00
5-1	212.65	235.03	22.38	1.57	2.36	10.00	21.00	50.00	4.00
5-1	235.03	265.03	30.00	2.36	2.36	50.00	25.00	--	--
5-1	265.03	280.03	15.00	--	--	--	--	--	--

Proprietà di inerzia delle sezioni delle campate

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	cm	cm	cm	kN*m	kN*m	kN*cm^4	kN*cm^4	kN*cm^4	kN*cm^4
1-1	0.00	15.00	15.00	Tratto infinitamente rigido					
1-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	45.00	67.54	22.54	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-1	67.54	115.15	47.61	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	115.15	212.83	97.68	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
1-1	212.83	235.37	22.54	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	235.37	265.37	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	265.37	280.37	15.00	Tratto infinitamente rigido					
2-1	0.00	15.00	15.00	Tratto infinitamente rigido					
2-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	45.00	67.50	22.50	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-1	67.50	115.11	47.61	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	115.11	212.79	97.67	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
2-1	212.79	235.29	22.50	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	235.29	265.29	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	265.29	280.29	15.00	Tratto infinitamente rigido					
3-1	0.00	15.00	15.00	Tratto infinitamente rigido					
3-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-1	45.00	67.46	22.46	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-1	67.46	115.08	47.62	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	115.08	212.74	97.66	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
3-1	212.74	235.20	22.46	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	235.20	265.20	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
3-1	265.20	280.20	15.00	Tratto infinitamente rigido					
4-1	0.00	15.00	15.00	Tratto infinitamente rigido					
4-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	45.00	67.42	22.42	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-1	67.42	115.05	47.62	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	115.05	212.69	97.65	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
4-1	212.69	235.12	22.42	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	235.12	265.12	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	265.12	280.12	15.00	Tratto infinitamente rigido					
5-1	-0.00	15.00	15.00	Tratto infinitamente rigido					
5-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-1	45.00	67.38	22.38	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-1	67.38	115.01	47.63	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	115.01	212.65	97.63	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
5-1	212.65	235.03	22.38	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	235.03	265.03	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-1	265.03	280.03	15.00	Tratto infinitamente rigido					

Tensioni di esercizio combinazione Rara

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	15.00	--	2.74	--	--	-1.04	57.40	14.94	360.00	7	7	Si
2-1	15.00	--	2.74	--	--	-1.04	57.36	14.94	360.00	7	7	Si
3-1	265.20	--	2.74	--	--	-1.04	57.32	14.94	360.00	7	7	Si
4-1	15.00	--	2.74	--	--	-1.04	57.28	14.94	360.00	7	7	Si
5-1	15.00	--	2.74	--	--	-1.04	57.24	14.94	360.00	7	7	Si

Tensioni di esercizio combinazione QP

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	15.00	--	2.74	--	--	-1.04	57.40	11.21	360.00	19	19	Si
2-1	15.00	--	2.74	--	--	-1.04	57.36	11.21	360.00	19	19	Si
3-1	265.20	--	2.74	--	--	-1.04	57.32	11.21	360.00	19	19	Si
4-1	15.00	--	2.74	--	--	-1.04	57.28	11.21	360.00	19	19	Si
5-1	15.00	--	2.74	--	--	-1.04	57.24	11.21	360.00	19	19	Si

Verifica a decompressione o Verifica formazione fessure

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	
1-1	15.00	--	2.74	--	--	-1.04	0.00	2.13	Si
2-1	15.00	--	2.74	--	--	-1.04	0.00	2.13	Si
3-1	15.00	--	2.74	--	--	-1.04	0.00	2.13	Si
4-1	15.00	--	2.74	--	--	-1.04	0.00	2.13	Si
5-1	15.00	--	2.74	--	--	-1.04	0.00	2.13	Si

Solaio N.: Copertura 1
Base travetto = 10.00 cm

Criterio di verifica: Solaio in c.a.		
Rck	MPa	30.00
fyk	MPa	450.00
$\varepsilon c0 *10^3$		2
$\varepsilon cu *10^3$		3.5
$\varepsilon fu *10^3$		10
Ef	MPa	2.10E05
Copriferro di calcolo	cm	3.00
Copriferro di disegno	cm	3.00

fcd		0.85
γAcc		1.15
γCls		1.5
Percentuale max acciaio	%	1.8
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		Si
Verifica aperture fessure	MPa	No
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σCls	MPa	14.94
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σCls	MPa	11.21
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coeffcienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5

TRAVETTO N.: 1

CAMPATA N.: 1

Luce Netta L 529.46 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 47.23 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.01	7.42	13.42	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
264.73	15.26	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
529.46	-0.00	19.71	20.91	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 426.98 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	20.06	18.57	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.49	8.59	0.81	5.00	12.30	20.18	18.27	2Ø10	3Ø10		Si
426.98	1.51	4.83	10.10	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 2

CAMPATA N.: 1

Luce Netta L 528.94 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 47.06 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.01	7.41	13.40	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
264.47	15.23	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
528.94	-0.00	19.68	20.89	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 426.99 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	20.03	18.56	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.49	8.60	0.79	4.99	12.30	20.18	18.27	2Ø10	3Ø10		Si
426.99	1.51	4.83	10.10	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 3

CAMPATA N.: 1

Luce Netta L 528.42 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 46.90 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.01	7.39	13.39	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
264.21	15.20	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
528.42	-0.00	19.66	20.87	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	20.01	18.55	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.50	8.60	0.78	4.99	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.00	1.52	4.83	10.10	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 4

CAMPATA N.: 1

Luce Netta L 527.90 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm

Fascia piena a destra 46.73 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.01	7.38	13.37	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
263.95	15.17	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
527.90	-0.00	19.63	20.85	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 427.01 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	19.98	18.55	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.51	8.61	0.76	4.98	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.01	1.52	4.83	10.11	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 5

CAMPATA N.: 1

Luce Netta L 527.39 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 46.57 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.36	13.36	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.69	15.14	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
527.39	-0.00	19.61	20.83	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2

Luce Netta L 427.03 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	19.95	18.54	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.51	8.62	0.74	4.97	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.03	1.52	4.83	10.11	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 6

CAMPATA N.: 1

Luce Netta L 526.87 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera

Fascia piena a sinistra 30.00 cm
Fascia piena a destra 46.40 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.35	13.35	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.43	15.11	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
526.87	-0.00	19.58	20.82	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.04 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	19.92	18.54	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.52	8.62	0.73	4.97	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.04	1.52	4.83	10.11	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 7

CAMPATA N.: 1
Luce Netta L 526.40 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 46.25 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.34	13.33	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
263.20	15.08	0.00	4.08	0.57	19.66	15.41		3Ø10		Si
526.40	-0.00	19.56	20.80	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	19.90	18.53	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.50	8.63	0.72	4.96	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.00	1.52	4.83	10.11	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 8

CAMPATA N.: 1
Luce Netta L 525.89 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm

Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 46.09 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.00	7.32	13.32	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
262.95	15.05	0.00	4.07	0.57	19.66	15.41		3Ø10		Si
525.89	-0.00	19.53	20.78	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	19.87	18.52	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.50	8.63	0.70	4.96	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.00	1.52	4.83	10.12	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 9

CAMPATA N.: 1
Luce Netta L 521.81 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 45.23 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.21	7.21	13.15	14.29	20.18	53.42	2Ø10	3Ø10	FP	Si
260.90	14.88	0.00	4.12	0.57	19.66	15.41		3Ø10		Si
521.81	-0.00	19.41	20.70	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	19.74	18.49	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.50	8.66	0.63	4.93	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.00	1.52	4.83	10.13	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 10

CAMPATA N.: 1
Luce Netta L 471.82 cm
Altezza solaio H 25.00 cm

Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.47	5.89	11.62	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
235.91	12.20	0.00	4.16	6.44	20.05	16.96	1Ø10	3Ø10		Si
471.82	-0.00	17.32	19.15	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	17.50	17.99	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.50	9.18	0.00	4.42	12.30	20.18	18.27	2Ø10	3Ø10		Si
427.00	1.55	4.83	10.36	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 11

CAMPATA N.: 1
Luce Netta L 421.84 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	2.16	4.71	10.21	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
210.92	9.55	0.00	4.13	6.44	20.05	16.96	1Ø10	3Ø10		Si
421.84	-0.00	15.44	17.53	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	15.44	17.52	26.21	20.30	59.76	4Ø10	3Ø10	FP	Si
213.50	9.62	0.00	3.95	6.44	20.05	16.96	1Ø10	3Ø10		Si
427.00	1.58	4.83	10.55	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 12

CAMPATA N.: 1
Luce Netta L 371.85 cm

Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.85	3.66	8.73	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
185.92	7.10	0.00	4.19	6.44	20.05	16.96	1Ø10	3Ø10		Si
371.85	-0.00	13.97	16.01	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	13.80	17.15	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
213.50	9.93	0.00	3.58	6.44	20.05	16.96	1Ø10	3Ø10		Si
427.00	1.60	4.83	10.69	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 13

CAMPATA N.: 1
Luce Netta L 321.86 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.52	2.74	7.18	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
160.93	4.85	1.20	4.40	12.30	20.18	18.27	2Ø10	3Ø10		Si
321.86	-0.00	12.91	14.62	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	12.58	16.87	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
213.50	10.11	0.00	3.31	6.44	20.05	16.96	1Ø10	3Ø10		Si
427.00	1.61	4.83	10.76	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 14

CAMPATA N.: 1

Luce Netta L 271.88 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	1.17	1.96	5.51	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
135.94	3.35	2.57	4.81	18.13	20.26	18.97	3Ø10	3Ø10		Si
271.88	-0.00	12.26	13.45	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	11.78	16.69	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
213.50	10.16	0.00	3.12	6.44	20.05	16.96	1Ø10	3Ø10		Si
427.00	1.62	4.83	10.78	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

TRAVETTO N.: 15

CAMPATA N.: 1
Luce Netta L 221.89 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	0.78	1.30	3.66	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
110.94	2.23	3.88	5.55	23.90	20.30	18.97	4Ø10	3Ø10		Si
221.89	-0.00	12.01	12.60	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

CAMPATA N.: 2
Luce Netta L 427.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	11.41	16.61	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
213.50	10.05	0.00	3.04	6.44	20.05	16.96	1Ø10	3Ø10		Si
427.00	1.61	4.83	10.74	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

Verifiche di Deformabilità
Combinazioni di tipo: Rara

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
				cm			cm	cm	
1-1	A	7	1.00	559.46	0.50	250.0	2.24	-1.22	1.8
1-1	A	12	1.00	559.46	0.50	250.0	2.24	-0.48	4.7
1-1	A	11	1.00	559.46	0.50	250.0	2.24	-0.48	4.7
1-1	A	10	1.00	559.46	0.50	250.0	2.24	-1.22	1.8
1-1	A	9	1.00	559.46	0.50	250.0	2.24	-1.44	1.6
1-1	A	8	1.00	559.46	0.50	250.0	2.24	-0.24	9.2
1-2	A	8	1.00	456.98	0.50	250.0	1.83	-0.42	4.4
1-2	A	9	1.00	456.98	0.50	250.0	1.83	0.09	20
1-2	A	7	1.00	456.98	0.50	250.0	1.83	-0.15	12
1-2	A	12	1.00	456.98	0.50	250.0	1.83	-0.03	53
1-2	A	10	1.00	456.98	0.50	250.0	1.83	-0.15	12
1-2	A	11	1.00	456.98	0.50	250.0	1.83	-0.03	53
2-1	A	9	1.00	558.94	0.50	250.0	2.24	-1.43	1.6
2-1	A	10	1.00	558.94	0.50	250.0	2.24	-1.22	1.8
2-1	A	7	1.00	558.94	0.50	250.0	2.24	-1.22	1.8
2-1	A	12	1.00	558.94	0.50	250.0	2.24	-0.48	4.7
2-1	A	8	1.00	558.94	0.50	250.0	2.24	-0.24	9.3
2-1	A	11	1.00	558.94	0.50	250.0	2.24	-0.48	4.7
2-2	A	11	1.00	456.99	0.50	250.0	1.83	-0.03	53
2-2	A	7	1.00	456.99	0.50	250.0	1.83	-0.15	12
2-2	A	12	1.00	456.99	0.50	250.0	1.83	-0.03	53
2-2	A	9	1.00	456.99	0.50	250.0	1.83	0.09	20
2-2	A	8	1.00	456.99	0.50	250.0	1.83	-0.42	4.4
2-2	A	10	1.00	456.99	0.50	250.0	1.83	-0.15	12
3-1	A	8	1.00	558.42	0.50	250.0	2.23	-0.24	9.4
3-1	A	9	1.00	558.42	0.50	250.0	2.23	-1.43	1.6
3-1	A	11	1.00	558.42	0.50	250.0	2.23	-0.47	4.7
3-1	A	12	1.00	558.42	0.50	250.0	2.23	-0.47	4.7
3-1	A	7	1.00	558.42	0.50	250.0	2.23	-1.21	1.8
3-1	A	10	1.00	558.42	0.50	250.0	2.23	-1.21	1.8
3-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.15	12
3-2	A	9	1.00	457.00	0.50	250.0	1.83	0.09	20
3-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.03	53
3-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.15	12
3-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.42	4.4
3-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.03	53
4-1	A	9	1.00	557.91	0.50	250.0	2.23	-1.42	1.6
4-1	A	11	1.00	557.91	0.50	250.0	2.23	-0.47	4.8
4-1	A	8	1.00	557.91	0.50	250.0	2.23	-0.23	9.5
4-1	A	10	1.00	557.91	0.50	250.0	2.23	-1.21	1.9
4-1	A	12	1.00	557.91	0.50	250.0	2.23	-0.47	4.8
4-1	A	7	1.00	557.91	0.50	250.0	2.23	-1.21	1.9
4-2	A	7	1.00	457.01	0.50	250.0	1.83	-0.15	12
4-2	A	9	1.00	457.01	0.50	250.0	1.83	0.09	20
4-2	A	12	1.00	457.01	0.50	250.0	1.83	-0.03	53
4-2	A	8	1.00	457.01	0.50	250.0	1.83	-0.42	4.4
4-2	A	11	1.00	457.01	0.50	250.0	1.83	-0.03	53
4-2	A	10	1.00	457.01	0.50	250.0	1.83	-0.15	12
5-1	A	8	1.00	557.39	0.50	250.0	2.23	-0.23	9.7
5-1	A	12	1.00	557.39	0.50	250.0	2.23	-0.47	4.8
5-1	A	10	1.00	557.39	0.50	250.0	2.23	-1.20	1.9
5-1	A	7	1.00	557.39	0.50	250.0	2.23	-1.20	1.9
5-1	A	9	1.00	557.39	0.50	250.0	2.23	-1.42	1.6
5-1	A	11	1.00	557.39	0.50	250.0	2.23	-0.47	4.8
5-2	A	7	1.00	457.03	0.50	250.0	1.83	-0.15	12
5-2	A	9	1.00	457.03	0.50	250.0	1.83	0.09	21
5-2	A	12	1.00	457.03	0.50	250.0	1.83	-0.03	52
5-2	A	11	1.00	457.03	0.50	250.0	1.83	-0.03	52
5-2	A	10	1.00	457.03	0.50	250.0	1.83	-0.15	12
5-2	A	8	1.00	457.03	0.50	250.0	1.83	-0.42	4.4
6-1	A	8	1.00	556.87	0.50	250.0	2.23	-0.23	9.8
6-1	A	11	1.00	556.87	0.50	250.0	2.23	-0.46	4.8
6-1	A	9	1.00	556.87	0.50	250.0	2.23	-1.41	1.6

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
6-1	A	10	1.00	556.87	0.50	250.0	2.23	-1.19	1.9
6-1	A	7	1.00	556.87	0.50	250.0	2.23	-1.19	1.9
6-1	A	12	1.00	556.87	0.50	250.0	2.23	-0.46	4.8
6-2	A	8	1.00	457.04	0.50	250.0	1.83	-0.42	4.4
6-2	A	7	1.00	457.04	0.50	250.0	1.83	-0.16	12
6-2	A	10	1.00	457.04	0.50	250.0	1.83	-0.16	12
6-2	A	11	1.00	457.04	0.50	250.0	1.83	-0.03	52
6-2	A	12	1.00	457.04	0.50	250.0	1.83	-0.03	52
6-2	A	9	1.00	457.04	0.50	250.0	1.83	0.09	21
7-1	A	9	1.00	556.40	0.50	250.0	2.23	-1.40	1.6
7-1	A	11	1.00	556.40	0.50	250.0	2.23	-0.46	4.8
7-1	A	10	1.00	556.40	0.50	250.0	2.23	-1.19	1.9
7-1	A	7	1.00	556.40	0.50	250.0	2.23	-1.19	1.9
7-1	A	12	1.00	556.40	0.50	250.0	2.23	-0.46	4.8
7-1	A	8	1.00	556.40	0.50	250.0	2.23	-0.22	9.9
7-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.42	4.4
7-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.16	12
7-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.04	52
7-2	A	9	1.00	457.00	0.50	250.0	1.83	0.09	21
7-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.04	52
7-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.16	12
8-1	A	11	1.00	555.90	0.50	250.0	2.22	-0.46	4.9
8-1	A	10	1.00	555.90	0.50	250.0	2.22	-1.18	1.9
8-1	A	8	1.00	555.90	0.50	250.0	2.22	-0.22	10
8-1	A	9	1.00	555.90	0.50	250.0	2.22	-1.40	1.6
8-1	A	12	1.00	555.90	0.50	250.0	2.22	-0.46	4.9
8-1	A	7	1.00	555.90	0.50	250.0	2.22	-1.18	1.9
8-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.16	12
8-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.16	12
8-2	A	9	1.00	457.00	0.50	250.0	1.83	0.09	21
8-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.04	52
8-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.42	4.3
8-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.04	52
9-1	A	9	1.00	553.60	0.50	250.0	2.21	-1.37	1.6
9-1	A	8	1.00	553.60	0.50	250.0	2.21	-0.20	11
9-1	A	7	1.00	553.60	0.50	250.0	2.21	-1.16	1.9
9-1	A	11	1.00	553.60	0.50	250.0	2.21	-0.44	5.0
9-1	A	12	1.00	553.60	0.50	250.0	2.21	-0.44	5.0
9-1	A	10	1.00	553.60	0.50	250.0	2.21	-1.16	1.9
9-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.04	51
9-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.04	51
9-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.16	11
9-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.42	4.3
9-2	A	9	1.00	457.00	0.50	250.0	1.83	0.08	22
9-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.16	11
10-1	A	12	1.00	508.03	0.50	250.0	2.03	-0.17	12
10-1	A	9	1.00	508.03	0.50	250.0	2.03	-0.90	2.3
10-1	A	7	1.00	508.03	0.50	250.0	2.03	-0.70	2.9
10-1	A	10	1.00	508.03	0.50	250.0	2.03	-0.70	2.9
10-1	A	8	1.00	508.03	0.50	250.0	2.03	-0.06	35
10-1	A	11	1.00	508.03	0.50	250.0	2.03	-0.17	12
10-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.05	38
10-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.47	3.9
10-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.05	38
10-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.26	7.1
10-2	A	9	1.00	457.00	0.50	250.0	1.83	0.03	53
10-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.26	7.1
11-1	A	12	1.00	458.05	0.50	250.0	1.83	-0.06	31
11-1	A	10	1.00	458.05	0.50	250.0	1.83	-0.34	5.3
11-1	A	8	1.00	458.05	0.50	250.0	1.83	-0.02	79
11-1	A	9	1.00	458.05	0.50	250.0	1.83	-0.51	3.6
11-1	A	7	1.00	458.05	0.50	250.0	1.83	-0.34	5.3
11-1	A	11	1.00	458.05	0.50	250.0	1.83	-0.06	31
11-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.51	3.6

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
11-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.34	5.4
11-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.06	31
11-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.06	31
11-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.34	5.4
11-2	A	9	1.00	457.00	0.50	250.0	1.83	-0.02	79
12-1	A	12	1.00	408.06	0.50	250.0	1.63	-0.03	57
12-1	A	8	1.00	408.06	0.50	250.0	1.63	0.02	71
12-1	A	9	1.00	408.06	0.50	250.0	1.63	-0.23	7.0
12-1	A	11	1.00	408.06	0.50	250.0	1.63	-0.03	57
12-1	A	7	1.00	408.06	0.50	250.0	1.63	-0.06	27
12-1	A	10	1.00	408.06	0.50	250.0	1.63	-0.06	27
12-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.41	4.5
12-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.07	27
12-2	A	9	1.00	457.00	0.50	250.0	1.83	-0.04	47
12-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.41	4.5
12-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.07	27
12-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.53	3.4
13-1	A	12	1.00	358.07	0.50	250.0	1.43	-0.01	>100
13-1	A	10	1.00	358.07	0.50	250.0	1.43	-0.02	81
13-1	A	11	1.00	358.07	0.50	250.0	1.43	-0.01	>100
13-1	A	9	1.00	358.07	0.50	250.0	1.43	-0.04	33
13-1	A	7	1.00	358.07	0.50	250.0	1.43	-0.02	81
13-1	A	8	1.00	358.07	0.50	250.0	1.43	0.03	51
13-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.55	3.3
13-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.46	4.0
13-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.46	4.0
13-2	A	9	1.00	457.00	0.50	250.0	1.83	-0.05	34
13-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.07	24
13-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.07	24
14-1	A	9	1.00	308.09	0.50	250.0	1.23	-0.02	75
14-1	A	11	1.00	308.09	0.50	250.0	1.23	0.01	>100
14-1	A	10	1.00	308.09	0.50	250.0	1.23	0.01	88
14-1	A	7	1.00	308.09	0.50	250.0	1.23	0.01	88
14-1	A	8	1.00	308.09	0.50	250.0	1.23	0.03	43
14-1	A	12	1.00	308.09	0.50	250.0	1.23	0.01	>100
14-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.08	23
14-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.49	3.7
14-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.49	3.7
14-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.08	23
14-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.56	3.3
14-2	A	9	1.00	457.00	0.50	250.0	1.83	-0.06	28
15-1	A	8	1.00	258.10	0.50	250.0	1.03	0.03	39
15-1	A	9	1.00	258.10	0.50	250.0	1.03	0.00	>100
15-1	A	10	1.00	258.10	0.50	250.0	1.03	0.02	59
15-1	A	7	1.00	258.10	0.50	250.0	1.03	0.02	59
15-1	A	11	1.00	258.10	0.50	250.0	1.03	0.01	>100
15-1	A	12	1.00	258.10	0.50	250.0	1.03	0.01	>100
15-2	A	10	1.00	457.00	0.50	250.0	1.83	-0.51	3.6
15-2	A	9	1.00	457.00	0.50	250.0	1.83	-0.07	25
15-2	A	11	1.00	457.00	0.50	250.0	1.83	-0.08	23
15-2	A	7	1.00	457.00	0.50	250.0	1.83	-0.51	3.6
15-2	A	8	1.00	457.00	0.50	250.0	1.83	-0.55	3.3
15-2	A	12	1.00	457.00	0.50	250.0	1.83	-0.08	23

Proprietà geometriche delle sezioni delle campate

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
	cm	cm	cm	cmq	cmq	cm	cm	cm	cm
1-1	0.00	15.00	15.00	--	--	--	--	--	--
1-1	15.00	26.24	11.24	2.36	2.36	50.00	25.00	--	--
1-1	26.24	45.00	18.76	1.57	2.36	50.00	25.00	--	--
1-1	45.00	184.48	139.48	1.57	2.36	10.00	21.00	50.00	4.00
1-1	184.48	226.78	42.31	0.79	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
1-1	226.78	454.01	227.23	0.00	2.36	10.00	21.00	50.00	4.00
1-1	454.01	497.23	43.22	0.79	2.36	10.00	21.00	50.00	4.00
1-1	497.23	526.88	29.65	1.57	2.36	50.00	25.00	--	--
1-1	526.88	544.46	17.58	2.36	2.36	50.00	25.00	--	--
1-1	544.46	559.46	15.00	--	--	--	--	--	--
1-2	559.46	574.46	15.00	--	--	--	--	--	--
1-2	574.46	596.46	22.00	3.14	2.36	50.00	25.00	--	--
1-2	596.46	604.46	8.00	2.36	2.36	50.00	25.00	--	--
1-2	604.46	635.18	30.72	2.36	2.36	10.00	21.00	50.00	4.00
1-2	635.18	685.01	49.83	1.57	2.36	10.00	21.00	50.00	4.00
1-2	685.01	706.96	21.96	2.36	2.36	10.00	21.00	50.00	4.00
1-2	706.96	971.44	264.47	1.57	2.36	10.00	21.00	50.00	4.00
1-2	971.44	1001.44	30.00	2.36	2.36	50.00	25.00	--	--
1-2	1001.44	1016.44	15.00	--	--	--	--	--	--
2-1	0.00	15.00	15.00	--	--	--	--	--	--
2-1	15.00	25.90	10.90	2.36	2.36	50.00	25.00	--	--
2-1	25.90	45.00	19.10	1.57	2.36	50.00	25.00	--	--
2-1	45.00	184.23	139.23	1.57	2.36	10.00	21.00	50.00	4.00
2-1	184.23	226.58	42.35	0.79	2.36	10.00	21.00	50.00	4.00
2-1	226.58	453.57	226.99	0.00	2.36	10.00	21.00	50.00	4.00
2-1	453.57	496.88	43.31	0.79	2.36	10.00	21.00	50.00	4.00
2-1	496.88	526.48	29.60	1.57	2.36	50.00	25.00	--	--
2-1	526.48	543.94	17.46	2.36	2.36	50.00	25.00	--	--
2-1	543.94	558.94	15.00	--	--	--	--	--	--
2-2	558.94	573.94	15.00	--	--	--	--	--	--
2-2	573.94	595.78	21.84	3.14	2.36	50.00	25.00	--	--
2-2	595.78	603.94	8.16	2.36	2.36	50.00	25.00	--	--
2-2	603.94	634.38	30.44	2.36	2.36	10.00	21.00	50.00	4.00
2-2	634.38	684.20	49.82	1.57	2.36	10.00	21.00	50.00	4.00
2-2	684.20	706.11	21.92	2.36	2.36	10.00	21.00	50.00	4.00
2-2	706.11	970.93	264.82	1.57	2.36	10.00	21.00	50.00	4.00
2-2	970.93	1000.93	30.00	2.36	2.36	50.00	25.00	--	--
2-2	1000.93	1015.93	15.00	--	--	--	--	--	--
3-1	0.00	15.00	15.00	--	--	--	--	--	--
3-1	15.00	25.57	10.57	2.36	2.36	50.00	25.00	--	--
3-1	25.57	45.00	19.43	1.57	2.36	50.00	25.00	--	--
3-1	45.00	183.98	138.98	1.57	2.36	10.00	21.00	50.00	4.00
3-1	183.98	226.37	42.39	0.79	2.36	10.00	21.00	50.00	4.00
3-1	226.37	453.12	226.75	0.00	2.36	10.00	21.00	50.00	4.00
3-1	453.12	496.53	43.41	0.79	2.36	10.00	21.00	50.00	4.00
3-1	496.53	526.08	29.56	1.57	2.36	50.00	25.00	--	--
3-1	526.08	543.42	17.34	2.36	2.36	50.00	25.00	--	--
3-1	543.42	558.42	15.00	--	--	--	--	--	--
3-2	558.42	573.42	15.00	--	--	--	--	--	--
3-2	573.42	595.10	21.68	3.14	2.36	50.00	25.00	--	--
3-2	595.10	603.42	8.32	2.36	2.36	50.00	25.00	--	--
3-2	603.42	633.58	30.16	2.36	2.36	10.00	21.00	50.00	4.00
3-2	633.58	683.39	49.81	1.57	2.36	10.00	21.00	50.00	4.00
3-2	683.39	705.26	21.87	2.36	2.36	10.00	21.00	50.00	4.00
3-2	705.26	970.43	265.16	1.57	2.36	10.00	21.00	50.00	4.00
3-2	970.43	1000.43	30.00	2.36	2.36	50.00	25.00	--	--
3-2	1000.43	1015.43	15.00	--	--	--	--	--	--
4-1	0.00	15.00	15.00	--	--	--	--	--	--
4-1	15.00	25.23	10.23	2.36	2.36	50.00	25.00	--	--
4-1	25.23	45.00	19.77	1.57	2.36	50.00	25.00	--	--
4-1	45.00	183.73	138.73	1.57	2.36	10.00	21.00	50.00	4.00
4-1	183.73	226.16	42.43	0.79	2.36	10.00	21.00	50.00	4.00
4-1	226.16	452.67	226.51	0.00	2.36	10.00	21.00	50.00	4.00
4-1	452.67	496.17	43.51	0.79	2.36	10.00	21.00	50.00	4.00
4-1	496.17	525.68	29.51	1.57	2.36	50.00	25.00	--	--
4-1	525.68	542.91	17.22	2.36	2.36	50.00	25.00	--	--
4-1	542.91	557.91	15.00	--	--	--	--	--	--
4-2	557.91	572.91	15.00	--	--	--	--	--	--
4-2	572.91	594.42	21.52	3.14	2.36	50.00	25.00	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
4-2	594.42	602.91	8.48	2.36	2.36	50.00	25.00	--	--
4-2	602.91	632.78	29.88	2.36	2.36	10.00	21.00	50.00	4.00
4-2	632.78	682.58	49.80	1.57	2.36	10.00	21.00	50.00	4.00
4-2	682.58	704.41	21.83	2.36	2.36	10.00	21.00	50.00	4.00
4-2	704.41	969.92	265.51	1.57	2.36	10.00	21.00	50.00	4.00
4-2	969.92	999.92	30.00	2.36	2.36	50.00	25.00	--	--
4-2	999.92	1014.92	15.00	--	--	--	--	--	--
5-1	0.00	15.00	15.00	--	--	--	--	--	--
5-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
5-1	45.00	183.48	138.48	1.57	2.36	10.00	21.00	50.00	4.00
5-1	183.48	225.96	42.47	0.79	2.36	10.00	21.00	50.00	4.00
5-1	225.96	452.22	226.26	0.00	2.36	10.00	21.00	50.00	4.00
5-1	452.22	495.82	43.60	0.79	2.36	10.00	21.00	50.00	4.00
5-1	495.82	525.28	29.46	1.57	2.36	50.00	25.00	--	--
5-1	525.28	542.39	17.10	2.36	2.36	50.00	25.00	--	--
5-1	542.39	557.39	15.00	--	--	--	--	--	--
5-2	557.39	572.39	15.00	--	--	--	--	--	--
5-2	572.39	593.74	21.36	3.14	2.36	50.00	25.00	--	--
5-2	593.74	602.39	8.64	2.36	2.36	50.00	25.00	--	--
5-2	602.39	631.98	29.60	2.36	2.36	10.00	21.00	50.00	4.00
5-2	631.98	681.77	49.79	1.57	2.36	10.00	21.00	50.00	4.00
5-2	681.77	703.56	21.79	2.36	2.36	10.00	21.00	50.00	4.00
5-2	703.56	969.41	265.85	1.57	2.36	10.00	21.00	50.00	4.00
5-2	969.41	999.41	30.00	2.36	2.36	50.00	25.00	--	--
5-2	999.41	1014.41	15.00	--	--	--	--	--	--
6-1	0.00	15.00	15.00	--	--	--	--	--	--
6-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
6-1	45.00	183.23	138.23	1.57	2.36	10.00	21.00	50.00	4.00
6-1	183.23	225.75	42.52	0.79	2.36	10.00	21.00	50.00	4.00
6-1	225.75	451.77	226.02	0.00	2.36	10.00	21.00	50.00	4.00
6-1	451.77	495.47	43.70	0.79	2.36	10.00	21.00	50.00	4.00
6-1	495.47	524.89	29.42	1.57	2.36	50.00	25.00	--	--
6-1	524.89	541.87	16.98	2.36	2.36	50.00	25.00	--	--
6-1	541.87	556.87	15.00	--	--	--	--	--	--
6-2	556.87	571.87	15.00	--	--	--	--	--	--
6-2	571.87	593.07	21.20	3.14	2.36	50.00	25.00	--	--
6-2	593.07	601.87	8.80	2.36	2.36	50.00	25.00	--	--
6-2	601.87	631.19	29.32	2.36	2.36	10.00	21.00	50.00	4.00
6-2	631.19	680.97	49.78	1.57	2.36	10.00	21.00	50.00	4.00
6-2	680.97	702.71	21.74	2.36	2.36	10.00	21.00	50.00	4.00
6-2	702.71	968.91	266.20	1.57	2.36	10.00	21.00	50.00	4.00
6-2	968.91	998.91	30.00	2.36	2.36	50.00	25.00	--	--
6-2	998.91	1013.91	15.00	--	--	--	--	--	--
7-1	0.00	15.00	15.00	--	--	--	--	--	--
7-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
7-1	45.00	183.01	138.01	1.57	2.36	10.00	21.00	50.00	4.00
7-1	183.01	225.56	42.55	0.79	2.36	10.00	21.00	50.00	4.00
7-1	225.56	451.38	225.82	0.00	2.36	10.00	21.00	50.00	4.00
7-1	451.38	495.15	43.77	0.79	2.36	10.00	21.00	50.00	4.00
7-1	495.15	524.53	29.38	1.57	2.36	50.00	25.00	--	--
7-1	524.53	541.40	16.87	2.36	2.36	50.00	25.00	--	--
7-1	541.40	556.40	15.00	--	--	--	--	--	--
7-2	556.40	571.40	15.00	--	--	--	--	--	--
7-2	571.40	592.45	21.05	3.14	2.36	50.00	25.00	--	--
7-2	592.45	601.40	8.95	2.36	2.36	50.00	25.00	--	--
7-2	601.40	630.47	29.06	2.36	2.36	10.00	21.00	50.00	4.00
7-2	630.47	680.24	49.77	1.57	2.36	10.00	21.00	50.00	4.00
7-2	680.24	701.95	21.71	2.36	2.36	10.00	21.00	50.00	4.00
7-2	701.95	968.40	266.45	1.57	2.36	10.00	21.00	50.00	4.00
7-2	968.40	998.40	30.00	2.36	2.36	50.00	25.00	--	--
7-2	998.40	1013.40	15.00	--	--	--	--	--	--
8-1	0.00	15.00	15.00	--	--	--	--	--	--
8-1	15.00	45.00	30.00	1.57	2.36	50.00	25.00	--	--
8-1	45.00	182.76	137.76	1.57	2.36	10.00	21.00	50.00	4.00

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
8-1	182.76	225.36	42.59	0.79	2.36	10.00	21.00	50.00	4.00
8-1	225.36	450.94	225.58	0.00	2.36	10.00	21.00	50.00	4.00
8-1	450.94	494.81	43.87	0.79	2.36	10.00	21.00	50.00	4.00
8-1	494.81	524.14	29.34	1.57	2.36	50.00	25.00	--	--
8-1	524.14	540.90	16.75	2.36	2.36	50.00	25.00	--	--
8-1	540.90	555.90	15.00	--	--	--	--	--	--
8-2	555.90	570.90	15.00	--	--	--	--	--	--
8-2	570.90	591.79	20.89	3.14	2.36	50.00	25.00	--	--
8-2	591.79	600.90	9.11	2.36	2.36	50.00	25.00	--	--
8-2	600.90	629.69	28.79	2.36	2.36	10.00	21.00	50.00	4.00
8-2	629.69	679.45	49.77	1.57	2.36	10.00	21.00	50.00	4.00
8-2	679.45	701.12	21.66	2.36	2.36	10.00	21.00	50.00	4.00
8-2	701.12	967.90	266.78	1.57	2.36	10.00	21.00	50.00	4.00
8-2	967.90	997.90	30.00	2.36	2.36	50.00	25.00	--	--
8-2	997.90	1012.90	15.00	--	--	--	--	--	--
9-1	1.79	18.58	16.79	--	--	--	--	--	--
9-1	18.58	48.58	30.00	1.57	2.36	50.00	25.00	--	--
9-1	48.58	184.38	135.80	1.57	2.36	10.00	21.00	50.00	4.00
9-1	184.38	227.30	42.93	0.79	2.36	10.00	21.00	50.00	4.00
9-1	227.30	450.80	223.50	0.00	2.36	10.00	21.00	50.00	4.00
9-1	450.80	495.16	44.36	0.79	2.36	10.00	21.00	50.00	4.00
9-1	495.16	524.20	29.04	1.57	2.36	50.00	25.00	--	--
9-1	524.20	540.39	16.19	2.36	2.36	50.00	25.00	--	--
9-1	540.39	555.39	15.00	--	--	--	--	--	--
9-2	555.39	570.39	15.00	--	--	--	--	--	--
9-2	570.39	590.54	20.15	3.14	2.36	50.00	25.00	--	--
9-2	590.54	600.39	9.85	2.36	2.36	50.00	25.00	--	--
9-2	600.39	627.88	27.49	2.36	2.36	10.00	21.00	50.00	4.00
9-2	627.88	677.61	49.72	1.57	2.36	10.00	21.00	50.00	4.00
9-2	677.61	699.07	21.46	2.36	2.36	10.00	21.00	50.00	4.00
9-2	699.07	967.39	268.32	1.57	2.36	10.00	21.00	50.00	4.00
9-2	967.39	997.39	30.00	2.36	2.36	50.00	25.00	--	--
9-2	997.39	1012.39	15.00	--	--	--	--	--	--
10-1	0.00	21.21	21.21	--	--	--	--	--	--
10-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
10-1	51.21	162.66	111.45	2.36	2.36	10.00	21.00	50.00	4.00
10-1	162.66	209.94	47.28	1.57	2.36	10.00	21.00	50.00	4.00
10-1	209.94	355.11	145.17	0.79	2.36	10.00	21.00	50.00	4.00
10-1	355.11	425.51	70.40	1.57	2.36	10.00	21.00	50.00	4.00
10-1	425.51	431.16	5.65	2.36	2.36	10.00	21.00	50.00	4.00
10-1	431.16	463.03	31.87	1.57	2.36	10.00	21.00	50.00	4.00
10-1	463.03	493.03	30.00	2.36	2.36	50.00	25.00	--	--
10-1	493.03	508.03	15.00	--	--	--	--	--	--
10-2	508.03	523.03	15.00	--	--	--	--	--	--
10-2	523.03	549.35	26.32	3.14	2.36	50.00	25.00	--	--
10-2	549.35	553.03	3.68	2.36	2.36	50.00	25.00	--	--
10-2	553.03	598.61	45.58	2.36	2.36	10.00	21.00	50.00	4.00
10-2	598.61	605.10	6.49	1.57	2.36	10.00	21.00	50.00	4.00
10-2	605.10	693.15	88.05	2.36	2.36	10.00	21.00	50.00	4.00
10-2	693.15	779.23	86.08	1.57	2.36	10.00	21.00	50.00	4.00
10-2	779.23	825.19	45.95	0.79	2.36	10.00	21.00	50.00	4.00
10-2	825.19	920.03	94.85	1.57	2.36	10.00	21.00	50.00	4.00
10-2	920.03	950.03	30.00	2.36	2.36	50.00	25.00	--	--
10-2	950.03	965.03	15.00	--	--	--	--	--	--
11-1	-0.00	21.21	21.21	--	--	--	--	--	--
11-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
11-1	51.21	144.12	92.91	2.36	2.36	10.00	21.00	50.00	4.00
11-1	144.12	189.94	45.82	1.57	2.36	10.00	21.00	50.00	4.00
11-1	189.94	299.34	109.39	0.79	2.36	10.00	21.00	50.00	4.00
11-1	299.34	382.12	82.79	1.57	2.36	10.00	21.00	50.00	4.00
11-1	382.12	388.53	6.41	2.36	2.36	10.00	21.00	50.00	4.00
11-1	388.53	413.05	24.52	1.57	2.36	10.00	21.00	50.00	4.00
11-1	413.05	443.05	30.00	2.36	2.36	50.00	25.00	--	--
11-1	443.05	458.05	15.00	--	--	--	--	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
11-2	458.05	473.05	15.00	--	--	--	--	--	--
11-2	473.05	487.40	14.36	3.14	2.36	50.00	25.00	--	--
11-2	487.40	503.05	15.64	2.36	2.36	50.00	25.00	--	--
11-2	503.05	527.45	24.41	2.36	2.36	10.00	21.00	50.00	4.00
11-2	527.45	533.96	6.51	1.57	2.36	10.00	21.00	50.00	4.00
11-2	533.96	617.56	83.60	2.36	2.36	10.00	21.00	50.00	4.00
11-2	617.56	643.85	26.29	1.57	2.36	10.00	21.00	50.00	4.00
11-2	643.85	775.20	131.35	0.79	2.36	10.00	21.00	50.00	4.00
11-2	775.20	870.05	94.85	1.57	2.36	10.00	21.00	50.00	4.00
11-2	870.05	900.05	30.00	2.36	2.36	50.00	25.00	--	--
11-2	900.05	915.05	15.00	--	--	--	--	--	--
12-1	0.00	21.21	21.21	--	--	--	--	--	--
12-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
12-1	51.21	125.08	73.87	2.36	2.36	10.00	21.00	50.00	4.00
12-1	125.08	169.95	44.87	1.57	2.36	10.00	21.00	50.00	4.00
12-1	169.95	288.22	118.27	0.79	2.36	10.00	21.00	50.00	4.00
12-1	288.22	336.56	48.33	1.57	2.36	10.00	21.00	50.00	4.00
12-1	336.56	363.80	27.24	2.36	2.36	10.00	21.00	50.00	4.00
12-1	363.80	393.06	29.26	1.57	2.36	50.00	25.00	--	--
12-1	393.06	408.06	15.00	--	--	--	--	--	--
12-2	408.06	423.06	15.00	--	--	--	--	--	--
12-2	423.06	449.44	26.38	2.36	2.36	50.00	25.00	--	--
12-2	449.44	453.06	3.62	1.57	2.36	50.00	25.00	--	--
12-2	453.06	466.96	13.90	1.57	2.36	10.00	21.00	50.00	4.00
12-2	466.96	504.88	37.92	2.36	2.36	10.00	21.00	50.00	4.00
12-2	504.88	593.86	88.98	1.57	2.36	10.00	21.00	50.00	4.00
12-2	593.86	725.21	131.35	0.79	2.36	10.00	21.00	50.00	4.00
12-2	725.21	820.06	94.85	1.57	2.36	10.00	21.00	50.00	4.00
12-2	820.06	850.06	30.00	2.36	2.36	50.00	25.00	--	--
12-2	850.06	865.06	15.00	--	--	--	--	--	--
13-1	0.00	21.21	21.21	--	--	--	--	--	--
13-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
13-1	51.21	105.30	54.09	2.36	2.36	10.00	21.00	50.00	4.00
13-1	105.30	287.35	182.05	1.57	2.36	10.00	21.00	50.00	4.00
13-1	287.35	313.07	25.72	2.36	2.36	10.00	21.00	50.00	4.00
13-1	313.07	343.07	30.00	1.57	2.36	50.00	25.00	--	--
13-1	343.07	358.07	15.00	--	--	--	--	--	--
13-2	358.07	373.07	15.00	--	--	--	--	--	--
13-2	373.07	392.03	18.96	2.36	2.36	50.00	25.00	--	--
13-2	392.03	403.07	11.04	1.57	2.36	50.00	25.00	--	--
13-2	403.07	409.33	6.26	1.57	2.36	10.00	21.00	50.00	4.00
13-2	409.33	441.57	32.25	2.36	2.36	10.00	21.00	50.00	4.00
13-2	441.57	501.17	59.60	1.57	2.36	10.00	21.00	50.00	4.00
13-2	501.17	675.23	174.05	0.79	2.36	10.00	21.00	50.00	4.00
13-2	675.23	770.07	94.85	1.57	2.36	10.00	21.00	50.00	4.00
13-2	770.07	800.07	30.00	2.36	2.36	50.00	25.00	--	--
13-2	800.07	815.07	15.00	--	--	--	--	--	--
14-1	0.00	21.21	21.21	--	--	--	--	--	--
14-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--
14-1	51.21	263.09	211.88	2.36	2.36	10.00	21.00	50.00	4.00
14-1	263.09	293.09	30.00	1.57	2.36	50.00	25.00	--	--
14-1	293.09	308.09	15.00	--	--	--	--	--	--
14-2	308.09	323.09	15.00	--	--	--	--	--	--
14-2	323.09	337.05	13.97	2.36	2.36	50.00	25.00	--	--
14-2	337.05	353.09	16.03	1.57	2.36	50.00	25.00	--	--
14-2	353.09	354.55	1.47	1.57	2.36	10.00	21.00	50.00	4.00
14-2	354.55	382.82	28.27	2.36	2.36	10.00	21.00	50.00	4.00
14-2	382.82	451.19	68.36	1.57	2.36	10.00	21.00	50.00	4.00
14-2	451.19	625.24	174.05	0.79	2.36	10.00	21.00	50.00	4.00
14-2	625.24	720.09	94.85	1.57	2.36	10.00	21.00	50.00	4.00
14-2	720.09	750.09	30.00	2.36	2.36	50.00	25.00	--	--
14-2	750.09	765.09	15.00	--	--	--	--	--	--
15-1	-0.00	21.21	21.21	--	--	--	--	--	--
15-1	21.21	51.21	30.00	2.36	2.36	50.00	25.00	--	--

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
15-1	51.21	125.99	74.78	2.36	2.36	10.00	21.00	50.00	4.00
15-1	125.99	183.34	57.35	3.14	2.36	10.00	21.00	50.00	4.00
15-1	183.34	213.10	29.76	2.36	2.36	10.00	21.00	50.00	4.00
15-1	213.10	243.10	30.00	1.57	2.36	50.00	25.00	--	--
15-1	243.10	258.10	15.00	--	--	--	--	--	--
15-2	258.10	273.10	15.00	--	--	--	--	--	--
15-2	273.10	284.73	11.63	2.36	2.36	50.00	25.00	--	--
15-2	284.73	302.33	17.60	1.57	2.36	50.00	25.00	--	--
15-2	302.33	328.51	26.18	2.36	2.36	10.00	21.00	50.00	4.00
15-2	328.51	401.20	72.69	1.57	2.36	10.00	21.00	50.00	4.00
15-2	401.20	575.25	174.05	0.79	2.36	10.00	21.00	50.00	4.00
15-2	575.25	670.10	94.85	1.57	2.36	10.00	21.00	50.00	4.00
15-2	670.10	700.10	30.00	2.36	2.36	50.00	25.00	--	--
15-2	700.10	715.10	15.00	--	--	--	--	--	--

Proprietà di inerzia delle sezioni delle campate

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	cm	cm	cm	kN*m	kN*m	kN*cm^4	kN*cm^4	kN*cm^4	kN*cm^4
1-1	0.00	15.00	15.00	Tratto infinitamente rigido					
1-1	15.00	26.24	11.24	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	26.24	45.00	18.76	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
1-1	45.00	184.48	139.48	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	184.48	226.78	42.31	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-1	226.78	454.01	227.23	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
1-1	454.01	497.23	43.22	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
1-1	497.23	526.88	29.65	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
1-1	526.88	544.46	17.58	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	544.46	559.46	15.00	Tratto infinitamente rigido					
1-2	559.46	574.46	15.00	Tratto infinitamente rigido					
1-2	574.46	596.46	22.00	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
1-2	596.46	604.46	8.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-2	604.46	635.18	30.72	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-2	635.18	685.01	49.83	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-2	685.01	706.96	21.96	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-2	706.96	971.44	264.47	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-2	971.44	1001.44	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-2	1001.44	1016.44	15.00	Tratto infinitamente rigido					
2-1	0.00	15.00	15.00	Tratto infinitamente rigido					
2-1	15.00	25.90	10.90	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	25.90	45.00	19.10	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
2-1	45.00	184.23	139.23	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-1	184.23	226.58	42.35	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-1	226.58	453.57	226.99	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
2-1	453.57	496.88	43.31	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
2-1	496.88	526.48	29.60	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
2-1	526.48	543.94	17.46	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-1	543.94	558.94	15.00	Tratto infinitamente rigido					
2-2	558.94	573.94	15.00	Tratto infinitamente rigido					
2-2	573.94	595.78	21.84	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
2-2	595.78	603.94	8.16	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-2	603.94	634.38	30.44	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-2	634.38	684.20	49.82	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-2	684.20	706.11	21.92	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
2-2	706.11	970.93	264.82	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
2-2	970.93	1000.93	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
2-2	1000.93	1015.93	15.00	Tratto infinitamente rigido					
3-1	0.00	15.00	15.00	Tratto infinitamente rigido					
3-1	15.00	25.57	10.57	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
3-1	25.57	45.00	19.43	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
3-1	45.00	183.98	138.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-1	183.98	226.37	42.39	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-1	226.37	453.12	226.75	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
3-1	453.12	496.53	43.41	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
3-1	496.53	526.08	29.56	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
3-1	526.08	543.42	17.34	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-1	543.42	558.42	15.00	Tratto infinitamente rigido					
3-2	558.42	573.42	15.00	Tratto infinitamente rigido					
3-2	573.42	595.10	21.68	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
3-2	595.10	603.42	8.32	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-2	603.42	633.58	30.16	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-2	633.58	683.39	49.81	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-2	683.39	705.26	21.87	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
3-2	705.26	970.43	265.16	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
3-2	970.43	1000.43	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
3-2	1000.43	1015.43	15.00	Tratto infinitamente rigido					
4-1	0.00	15.00	15.00	Tratto infinitamente rigido					
4-1	15.00	25.23	10.23	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	25.23	45.00	19.77	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
4-1	45.00	183.73	138.73	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-1	183.73	226.16	42.43	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-1	226.16	452.67	226.51	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
4-1	452.67	496.17	43.51	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
4-1	496.17	525.68	29.51	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
4-1	525.68	542.91	17.22	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-1	542.91	557.91	15.00	Tratto infinitamente rigido					
4-2	557.91	572.91	15.00	Tratto infinitamente rigido					
4-2	572.91	594.42	21.52	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
4-2	594.42	602.91	8.48	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-2	602.91	632.78	29.88	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-2	632.78	682.58	49.80	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-2	682.58	704.41	21.83	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
4-2	704.41	969.92	265.51	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
4-2	969.92	999.92	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
4-2	999.92	1014.92	15.00	Tratto infinitamente rigido					
5-1	0.00	15.00	15.00	Tratto infinitamente rigido					
5-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
5-1	45.00	183.48	138.48	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-1	183.48	225.96	42.47	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-1	225.96	452.22	226.26	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
5-1	452.22	495.82	43.60	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
5-1	495.82	525.28	29.46	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
5-1	525.28	542.39	17.10	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-1	542.39	557.39	15.00	Tratto infinitamente rigido					
5-2	557.39	572.39	15.00	Tratto infinitamente rigido					
5-2	572.39	593.74	21.36	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
5-2	593.74	602.39	8.64	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-2	602.39	631.98	29.60	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-2	631.98	681.77	49.79	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-2	681.77	703.56	21.79	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
5-2	703.56	969.41	265.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
5-2	969.41	999.41	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
5-2	999.41	1014.41	15.00	Tratto infinitamente rigido					
6-1	0.00	15.00	15.00	Tratto infinitamente rigido					
6-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
6-1	45.00	183.23	138.23	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-1	183.23	225.75	42.52	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
6-1	225.75	451.77	226.02	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
6-1	451.77	495.47	43.70	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
6-1	495.47	524.89	29.42	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
6-1	524.89	541.87	16.98	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-1	541.87	556.87	15.00	Tratto infinitamente rigido					
6-2	556.87	571.87	15.00	Tratto infinitamente rigido					
6-2	571.87	593.07	21.20	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
6-2	593.07	601.87	8.80	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-2	601.87	631.19	29.32	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-2	631.19	680.97	49.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-2	680.97	702.71	21.74	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
6-2	702.71	968.91	266.20	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
6-2	968.91	998.91	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
6-2	998.91	1013.91	15.00	Tratto infinitamente rigido					
7-1	0.00	15.00	15.00	Tratto infinitamente rigido					
7-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
7-1	45.00	183.01	138.01	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-1	183.01	225.56	42.55	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-1	225.56	451.38	225.82	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
7-1	451.38	495.15	43.77	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
7-1	495.15	524.53	29.38	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
7-1	524.53	541.40	16.87	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-1	541.40	556.40	15.00	Tratto infinitamente rigido					
7-2	556.40	571.40	15.00	Tratto infinitamente rigido					
7-2	571.40	592.45	21.05	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
7-2	592.45	601.40	8.95	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-2	601.40	630.47	29.06	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-2	630.47	680.24	49.77	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-2	680.24	701.95	21.71	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
7-2	701.95	968.40	266.45	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
7-2	968.40	998.40	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
7-2	998.40	1013.40	15.00	Tratto infinitamente rigido					
8-1	0.00	15.00	15.00	Tratto infinitamente rigido					
8-1	15.00	45.00	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
8-1	45.00	182.76	137.76	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-1	182.76	225.36	42.59	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-1	225.36	450.94	225.58	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
8-1	450.94	494.81	43.87	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
8-1	494.81	524.14	29.34	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
8-1	524.14	540.90	16.75	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-1	540.90	555.90	15.00	Tratto infinitamente rigido					
8-2	555.90	570.90	15.00	Tratto infinitamente rigido					
8-2	570.90	591.79	20.89	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
8-2	591.79	600.90	9.11	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-2	600.90	629.69	28.79	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-2	629.69	679.45	49.77	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-2	679.45	701.12	21.66	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
8-2	701.12	967.90	266.78	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
8-2	967.90	997.90	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
8-2	997.90	1012.90	15.00	Tratto infinitamente rigido					
9-1	1.79	18.58	16.79	Tratto infinitamente rigido					
9-1	18.58	48.58	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
9-1	48.58	184.38	135.80	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-1	184.38	227.30	42.93	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-1	227.30	450.80	223.50	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
9-1	450.80	495.16	44.36	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
9-1	495.16	524.20	29.04	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
9-1	524.20	540.39	16.19	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-1	540.39	555.39	15.00	Tratto infinitamente rigido					
9-2	555.39	570.39	15.00	Tratto infinitamente rigido					
9-2	570.39	590.54	20.15	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
9-2	590.54	600.39	9.85	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-2	600.39	627.88	27.49	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
9-2	627.88	677.61	49.72	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-2	677.61	699.07	21.46	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
9-2	699.07	967.39	268.32	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
9-2	967.39	997.39	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
9-2	997.39	1012.39	15.00	Tratto infinitamente rigido					
10-1	0.00	21.21	21.21	Tratto infinitamente rigido					
10-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-1	51.21	162.66	111.45	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-1	162.66	209.94	47.28	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-1	209.94	355.11	145.17	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
10-1	355.11	425.51	70.40	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-1	425.51	431.16	5.65	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-1	431.16	463.03	31.87	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-1	463.03	493.03	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-1	493.03	508.03	15.00	Tratto infinitamente rigido					
10-2	508.03	523.03	15.00	Tratto infinitamente rigido					
10-2	523.03	549.35	26.32	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
10-2	549.35	553.03	3.68	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-2	553.03	598.61	45.58	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-2	598.61	605.10	6.49	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-2	605.10	693.15	88.05	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
10-2	693.15	779.23	86.08	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-2	779.23	825.19	45.95	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
10-2	825.19	920.03	94.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
10-2	920.03	950.03	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
10-2	950.03	965.03	15.00	Tratto infinitamente rigido					
11-1	-0.00	21.21	21.21	Tratto infinitamente rigido					
11-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-1	51.21	144.12	92.91	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
11-1	144.12	189.94	45.82	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-1	189.94	299.34	109.39	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
11-1	299.34	382.12	82.79	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-1	382.12	388.53	6.41	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
11-1	388.53	413.05	24.52	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-1	413.05	443.05	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-1	443.05	458.05	15.00	Tratto infinitamente rigido					
11-2	458.05	473.05	15.00	Tratto infinitamente rigido					
11-2	473.05	487.40	14.36	14.04	13.96	2.15E08	1.92E07	2.15E08	2.48E07
11-2	487.40	503.05	15.64	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-2	503.05	527.45	24.41	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
11-2	527.45	533.96	6.51	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-2	533.96	617.56	83.60	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
11-2	617.56	643.85	26.29	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-2	643.85	775.20	131.35	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
11-2	775.20	870.05	94.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
11-2	870.05	900.05	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
11-2	900.05	915.05	15.00	Tratto infinitamente rigido					
12-1	0.00	21.21	21.21	Tratto infinitamente rigido					
12-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-1	51.21	125.08	73.87	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
12-1	125.08	169.95	44.87	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-1	169.95	288.22	118.27	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
12-1	288.22	336.56	48.33	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-1	336.56	363.80	27.24	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
12-1	363.80	393.06	29.26	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
12-1	393.06	408.06	15.00	Tratto infinitamente rigido					
12-2	408.06	423.06	15.00	Tratto infinitamente rigido					
12-2	423.06	449.44	26.38	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-2	449.44	453.06	3.62	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
12-2	453.06	466.96	13.90	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-2	466.96	504.88	37.92	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
12-2	504.88	593.86	88.98	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-2	593.86	725.21	131.35	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
12-2	725.21	820.06	94.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
12-2	820.06	850.06	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
12-2	850.06	865.06	15.00	Tratto infinitamente rigido					
13-1	0.00	21.21	21.21	Tratto infinitamente rigido					
13-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-1	51.21	105.30	54.09	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-1	105.30	287.35	182.05	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-1	287.35	313.07	25.72	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-1	313.07	343.07	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
13-1	343.07	358.07	15.00	Tratto infinitamente rigido					
13-2	358.07	373.07	15.00	Tratto infinitamente rigido					
13-2	373.07	392.03	18.96	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-2	392.03	403.07	11.04	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
13-2	403.07	409.33	6.26	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-2	409.33	441.57	32.25	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
13-2	441.57	501.17	59.60	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-2	501.17	675.23	174.05	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
13-2	675.23	770.07	94.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
13-2	770.07	800.07	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
13-2	800.07	815.07	15.00	Tratto infinitamente rigido					
14-1	0.00	21.21	21.21	Tratto infinitamente rigido					
14-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-1	51.21	263.09	211.88	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
14-1	263.09	293.09	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
14-1	293.09	308.09	15.00	Tratto infinitamente rigido					
14-2	308.09	323.09	15.00	Tratto infinitamente rigido					
14-2	323.09	337.05	13.97	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-2	337.05	353.09	16.03	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
14-2	353.09	354.55	1.47	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-2	354.55	382.82	28.27	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
14-2	382.82	451.19	68.36	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-2	451.19	625.24	174.05	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
14-2	625.24	720.09	94.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
14-2	720.09	750.09	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
14-2	750.09	765.09	15.00	Tratto infinitamente rigido					
15-1	-0.00	21.21	21.21	Tratto infinitamente rigido					
15-1	21.21	51.21	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
15-1	51.21	125.99	74.78	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
15-1	125.99	183.34	57.35	8.15	4.30	8.64E07	1.92E07	8.64E07	1.92E07
15-1	183.34	213.10	29.76	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
15-1	213.10	243.10	30.00	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
15-1	243.10	258.10	15.00	Tratto infinitamente rigido					
15-2	258.10	273.10	15.00	Tratto infinitamente rigido					
15-2	273.10	284.73	11.63	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
15-2	284.73	302.33	17.60	13.76	13.85	2.12E08	1.92E07	2.12E08	1.33E07
15-2	302.33	328.51	26.18	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
15-2	328.51	401.20	72.69	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
15-2	401.20	575.25	174.05	7.81	4.27	8.48E07	1.92E07	8.48E07	6.06E06
15-2	575.25	670.10	94.85	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
15-2	670.10	700.10	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
15-2	700.10	715.10	15.00	Tratto infinitamente rigido					

Tensioni di esercizio combinazione Rara

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	544.46	--	13.79	--	--	-5.22	288.33	14.94	360.00	11	7	Si
1-2	635.18	--	7.77	--	--	-7.49	254.14	14.94	360.00	8	9	Si
2-1	543.94	--	13.77	--	--	-5.21	287.95	14.94	360.00	11	7	Si
2-2	634.38	--	7.78	--	--	-7.49	254.16	14.94	360.00	8	9	Si
3-1	543.42	--	13.75	--	--	-5.20	287.58	14.94	360.00	11	7	Si
3-2	633.58	--	7.78	--	--	-7.49	254.17	14.94	360.00	8	9	Si
4-1	542.91	--	13.73	--	--	-5.20	287.20	14.94	360.00	11	7	Si

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
4-2	632.78	--	7.78	--	--	-7.49	254.19	14.94	360.00	8	9	Si
5-1	542.39	--	13.71	--	--	-5.19	286.83	14.94	360.00	11	7	Si
5-2	631.98	--	7.78	--	--	-7.49	254.21	14.94	360.00	8	9	Si
6-1	541.87	--	13.70	--	--	-5.18	286.46	14.94	360.00	11	7	Si
6-2	631.19	--	7.78	--	--	-7.49	254.23	14.94	360.00	8	9	Si
7-1	541.40	--	13.68	--	--	-5.18	286.10	14.94	360.00	11	7	Si
7-2	630.47	--	7.78	--	--	-7.49	254.24	14.94	360.00	8	9	Si
8-1	540.90	--	13.66	--	--	-5.17	285.73	14.94	360.00	11	7	Si
8-2	629.69	--	7.78	--	--	-7.49	254.26	14.94	360.00	8	9	Si
9-1	540.39	--	13.58	--	--	-5.14	283.99	14.94	360.00	11	7	Si
9-2	627.88	--	7.78	--	--	-7.49	254.34	14.94	360.00	8	9	Si
10-1	493.03	--	12.12	--	--	-4.59	253.42	14.94	360.00	11	7	Si
10-2	523.03	--	12.24	--	--	-4.11	193.80	14.94	360.00	11	7	Si
11-1	443.05	--	10.80	--	--	-4.09	225.89	14.94	360.00	11	7	Si
11-2	487.40	--	9.18	--	--	-3.47	191.95	14.94	360.00	11	7	Si
12-1	393.06	--	9.77	--	--	-4.43	302.79	14.94	360.00	11	7	Si
12-2	449.44	--	6.74	--	--	-3.05	208.78	14.94	360.00	11	7	Si
13-1	343.07	--	9.03	--	--	-4.09	279.85	14.94	360.00	11	7	Si
13-2	392.03	--	6.74	--	--	-3.05	208.78	14.94	360.00	11	7	Si
14-1	293.09	--	8.58	--	--	-3.88	265.75	14.94	360.00	11	7	Si
14-2	337.05	--	6.74	--	--	-3.05	208.78	14.94	360.00	11	7	Si
15-1	243.10	--	8.40	--	--	-3.80	260.26	14.94	360.00	11	7	Si
15-2	284.73	--	6.74	--	--	-3.05	208.78	14.94	360.00	11	7	Si

Tensioni di esercizio combinazione QP

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	544.46	--	11.31	--	--	-4.28	236.44	11.21	360.00	23	19	Si
1-2	604.46	--	8.55	--	--	-7.17	188.72	11.21	360.00	23	19	Si
2-1	543.94	--	11.29	--	--	-4.27	236.13	11.21	360.00	23	19	Si
2-2	603.94	--	8.53	--	--	-7.16	188.40	11.21	360.00	23	19	Si
3-1	543.42	--	11.28	--	--	-4.27	235.82	11.21	360.00	23	19	Si
3-2	603.42	--	8.52	--	--	-7.15	188.07	11.21	360.00	23	19	Si
4-1	542.91	--	11.26	--	--	-4.26	235.51	11.21	360.00	23	19	Si
4-2	602.91	--	8.50	--	--	-7.13	187.75	11.21	360.00	23	19	Si
5-1	542.39	--	11.25	--	--	-4.26	235.21	11.21	360.00	23	19	Si
5-2	602.39	--	8.49	--	--	-7.12	187.43	11.21	360.00	23	19	Si
6-1	541.87	--	11.23	--	--	-4.25	234.90	11.21	360.00	23	19	Si
6-2	601.87	--	8.47	--	--	-7.11	187.10	11.21	360.00	23	19	Si
7-1	541.40	--	11.22	--	--	-4.25	234.61	11.21	360.00	23	19	Si
7-2	601.40	--	8.46	--	--	-7.10	186.80	11.21	360.00	23	19	Si
8-1	540.90	--	11.20	--	--	-4.24	234.31	11.21	360.00	23	19	Si
8-2	600.90	--	8.44	--	--	-7.09	186.48	11.21	360.00	23	19	Si
9-1	540.39	--	11.14	--	--	-4.21	232.88	11.21	360.00	23	19	Si
9-2	600.39	--	8.38	--	--	-7.03	184.98	11.21	360.00	23	19	Si
10-1	493.03	--	9.94	--	--	-3.76	207.81	11.21	360.00	23	19	Si
10-2	553.03	--	7.17	--	--	-6.02	158.46	11.21	360.00	23	19	Si
11-1	443.05	--	8.86	--	--	-3.35	185.23	11.21	360.00	23	19	Si
11-2	503.05	--	6.08	--	--	-5.10	134.19	11.21	360.00	23	19	Si
12-1	393.06	--	8.01	--	--	-3.63	248.29	11.21	360.00	23	19	Si
12-2	449.44	--	5.53	--	--	-2.50	171.21	11.21	360.00	23	19	Si
13-1	343.07	--	7.41	--	--	-3.35	229.48	11.21	360.00	23	19	Si
13-2	392.03	--	5.53	--	--	-2.50	171.21	11.21	360.00	23	19	Si
14-1	293.09	--	7.03	--	--	-3.19	217.92	11.21	360.00	23	19	Si
14-2	337.05	--	5.53	--	--	-2.50	171.21	11.21	360.00	23	19	Si
15-1	243.10	--	6.89	--	--	-3.12	213.42	11.21	360.00	23	19	Si
15-2	284.73	--	5.53	--	--	-2.50	171.21	11.21	360.00	23	19	Si

Verifica a decompressione o Verifica formazione fessure

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	
1-1	15.00	1.40	--	-0.53	0.00	--	--	2.13	Si
1-2	574.46	--	14.03	--	--	-4.71	0.00	2.13	Si
2-1	15.00	1.40	--	-0.53	0.00	--	--	2.13	Si
2-2	573.94	--	14.01	--	--	-4.71	0.00	2.13	Si
3-1	15.00	1.40	--	-0.53	0.00	--	--	2.13	Si
3-2	573.42	--	13.99	--	--	-4.70	0.00	2.13	Si
4-1	15.00	1.40	--	-0.53	0.00	--	--	2.13	Si
4-2	572.91	--	13.97	--	--	-4.69	0.00	2.13	Si
5-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
5-2	572.39	--	13.96	--	--	-4.69	0.00	2.13	Si
6-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
6-2	571.87	--	13.94	--	--	-4.68	0.00	2.13	Si
7-1	15.00	1.40	--	-0.54	0.00	--	--	2.13	Si
7-2	571.40	--	13.92	--	--	-4.67	0.00	2.13	Si
8-1	15.00	1.39	--	-0.54	0.00	--	--	2.13	Si
8-2	570.90	--	13.90	--	--	-4.67	0.00	2.13	Si
9-1	18.58	1.54	--	-0.59	0.00	--	--	2.13	Si
9-2	570.39	--	13.81	--	--	-4.64	0.00	2.13	Si
10-1	21.21	1.72	--	-0.65	0.00	--	--	2.13	Si
10-2	523.03	--	12.24	--	--	-4.11	0.00	2.13	Si
11-1	21.21	1.51	--	-0.57	0.00	--	--	2.13	Si
11-2	473.05	--	10.80	--	--	-3.63	0.00	2.13	Si
12-1	21.21	1.29	--	-0.49	0.00	--	--	2.13	Si
12-2	423.06	--	9.65	--	--	-3.65	0.00	2.13	Si
13-1	21.21	1.06	--	-0.40	0.00	--	--	2.13	Si
13-2	373.07	--	8.80	--	--	-3.33	0.00	2.13	Si
14-1	21.21	0.81	--	-0.31	0.00	--	--	2.13	Si
14-2	323.09	--	8.24	--	--	-3.12	0.00	2.13	Si
15-1	21.21	0.53	0.18	-0.20	0.00	-0.07	0.00	2.13	Si
15-2	273.10	--	7.98	--	--	-3.02	0.00	2.13	Si

Solaio N.: Copertura 2
Base travetto = 10.00 cm

Criterio di verifica: Solaio in c.a.		
Rck	MPa	30.00
fyk	MPa	450.00
$\varepsilon c0 *10^3$		2
$\varepsilon cu *10^3$		3.5
$\varepsilon fu *10^3$		10
Ef	MPa	2.10E05
Copriferro di calcolo	cm	3.00
Copriferro di disegno	cm	3.00
fcd		0.85
γAcc		1.15
γCls		1.5
Percentuale max acciaio	%	1.8
Fessurazioni		
Verifica a decompressione		No
Verifica formazione fessure		Si
Verifica aperture fessure	MPa	No
Tensioni ammissibili di esercizio		
Verifica Combinazione Rara		Si
Tensione ammissibile σCls	MPa	14.94
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione QP		Si
Tensione ammissibile σCls	MPa	11.21
Tensione ammissibile σAcciaio	MPa	360.00
Verifica Combinazione Freq.		No
Coeffcienti di omogeneizzazione		
Acciaio - Cls compresso		15
Cls teso - Cls compresso		0.5

TRAVETTO N.: 1

CAMPATA N.: 1

Luce Netta L 250.00 cm
Altezza solaio H 25.00 cm
Altezza soletta s 4.00 cm
Tipo Gettato in Opera
Fascia piena a sinistra 30.00 cm
Fascia piena a destra 30.00 cm

Xcn	Mi	Ms	T	Mrs	Mri	Vres	Afs	Afi	Fascia	Ver
cm	kN*m	kN*m	kN	kN*m	kN*m	kN				
0.00	-0.00	1.65	7.94	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si
125.00	3.31	0.00	0.00	0.57	19.66	15.41		3Ø10		Si
250.00	-0.00	1.65	7.94	20.26	20.26	56.76	3Ø10	3Ø10	FP	Si

Verifiche di Deformabilità
Combinazioni di tipo: Rara

T-C	Tipo	Comb	ridE	L	C	Coeff.	famm	f	CS
				cm			cm	cm	
1-1	A	8	1.00	280.00	0.50	250.0	1.12	-0.01	82
1-1	A	9	1.00	280.00	0.50	250.0	1.12	-0.01	82
1-1	A	10	1.00	280.00	0.50	250.0	1.12	-0.01	82
1-1	A	11	1.00	280.00	0.50	250.0	1.12	-0.01	82
1-1	A	12	1.00	280.00	0.50	250.0	1.12	-0.01	82
1-1	A	7	1.00	280.00	0.50	250.0	1.12	-0.01	82

Proprietà geometriche delle sezioni delle campate

T-C	x1	x2	Lt	Afs	Afi	B	H	Bs	Hs
	cm	cm	cm	cmq	cmq	cm	cm	cm	cm
1-1	-0.00	15.00	15.00	--	--	--	--	--	--
1-1	15.00	45.00	30.00	2.36	2.36	50.00	25.00	--	--
1-1	45.00	68.46	23.46	2.36	2.36	10.00	21.00	50.00	4.00
1-1	68.46	115.00	46.53	1.57	2.36	10.00	21.00	50.00	4.00
1-1	115.00	211.53	96.53	0.00	2.36	10.00	21.00	50.00	4.00
1-1	211.53	235.00	23.46	1.57	2.36	10.00	21.00	50.00	4.00
1-1	235.00	265.00	30.00	2.36	2.36	50.00	25.00	--	--
1-1	265.00	280.00	15.00	--	--	--	--	--	--

Proprietà di inerzia delle sezioni delle campate

T-C	x1	x2	Lt	Mrfs	Mrfi	EJ1i	EJ2i	EJ1s	EJ2s
	cm	cm	cm	kN*m	kN*m	kN*cm^4	kN*cm^4	kN*cm^4	kN*cm^4
1-1	-0.00	15.00	15.00	Tratto infinitamente rigido					
1-1	15.00	45.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	45.00	68.46	23.46	8.04	4.29	8.59E07	1.92E07	8.59E07	1.54E07
1-1	68.46	115.00	46.53	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	115.00	211.53	96.53	7.70	4.26	8.43E07	1.92E07	8.43E07	1.32E05
1-1	211.53	235.00	23.46	7.93	4.28	8.54E07	1.92E07	8.54E07	1.10E07
1-1	235.00	265.00	30.00	13.90	13.90	2.14E08	1.92E07	2.14E08	1.92E07
1-1	265.00	280.00	15.00	Tratto infinitamente rigido					

Tensioni di esercizio combinazione Rara

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	15.00	--	2.84	--	--	-1.07	59.33	14.94	360.00	7	7	Si

Tensioni di esercizio combinazione QP

T-C	Xt	M+	M-	σc+	σf+	σc-	σf-	σca	σfa	Cb+	Cb-.	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	MPa			
1-1	15.00	--	2.84	--	--	-1.07	59.33	11.21	360.00	19	19	Si

Verifica a decompressione o Verifica formazione fessure

T-C	Xt	M+	M-	σc+	σct+	σc-	σct-	σcta	Ver.
	cm	kN*m	kN*m	MPa	MPa	MPa	MPa	MPa	
1-1	15.00	--	2.84	--	--	-1.07	0.00	2.13	Si

Il Progettista